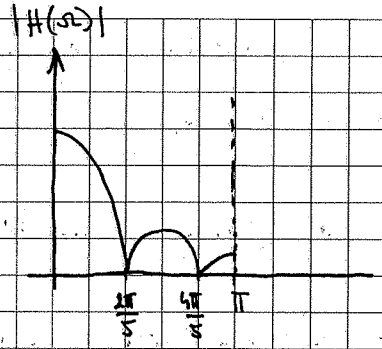
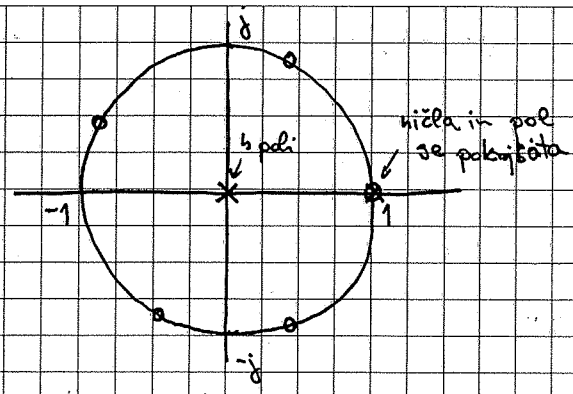


(3) 74B

74.

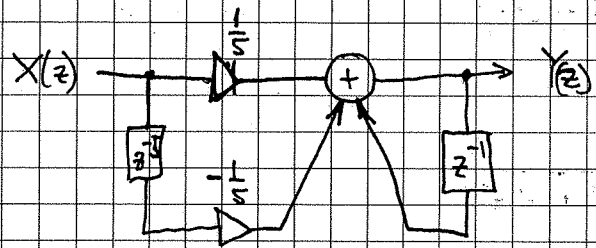


$$\frac{Y(z)}{X(z)} = \frac{1}{5} \frac{1-z^{-5}}{1-z^{-1}}$$

$$Y(z) (1-z^{-1}) = \frac{1}{5} X(z) (1-z^{-5})$$

$$Y(z) - Y(z) z^{-1} = \frac{1}{5} X(z) - \frac{1}{5} X(z) z^{-5}$$

$$Y(z) = \frac{1}{5} X(z) - \frac{1}{5} X(z) z^{-5} + Y(z) z^{-1}$$



18.4.2013

Narišite generator kosinusnega in sinusnega signala z normirano
krožno frekvenco Ω_1

$$x[n] = \cos(\Omega_1 n) \quad \dots \text{KOSINUS}$$

$$h[n] = a^n \cdot \cos(\Omega_1 n) \cdot u[n] \quad \dots \text{KOSINUS}$$

$$H(z) = \sum_{n=0}^{\infty} a^n \cdot \cos(\Omega_1 n) z^{-n} = \quad \cos \psi = \frac{1}{2} (e^{j\psi} + e^{-j\psi})$$

$$= \frac{1}{2} \left[\sum_{n=0}^{\infty} a^n \cdot e^{j\Omega_1 n} z^{-n} + \sum_{n=0}^{\infty} a^n \cdot e^{-j\Omega_1 n} z^{-n} \right] =$$

$$H(z) = \frac{1}{2} \left[\frac{1 - (ae^{j\Omega_1} z^{-1})^{\infty}}{1 - ae^{j\Omega_1} z^{-1}} + \frac{1 - (ae^{-j\Omega_1} z^{-1})^{\infty}}{1 - ae^{-j\Omega_1} z^{-1}} \right] =$$

$$= \frac{1}{2} \frac{1 - ae^{-j\Omega_1} z^{-1} + 1 - ae^{j\Omega_1} z^{-1}}{(1 - ae^{j\Omega_1} z^{-1})(1 - ae^{-j\Omega_1} z^{-1})} =$$

$$= \frac{1}{2} \frac{2 - az^{-1}(e^{-j\Omega_1} + e^{j\Omega_1})}{1 - ae^{j\Omega_1} z^{-1} - ae^{-j\Omega_1} z^{-1} + a^2 z^{-2}}$$

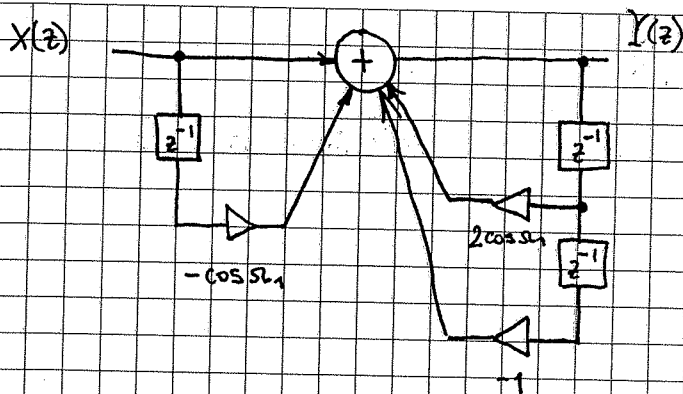
$$H(z) = \frac{1}{2} \frac{z - 2 \cos \Omega_1 \cdot az^{-1}}{1 - 2 \cos \Omega_1 \cdot az^{-1} + a^2 z^{-2}} \cdot \frac{1 \cdot z^2}{1 \cdot z^2} = \frac{Y(z)}{X(z)}$$

$$H(z) = \frac{z^2 - z \cos \Omega_1 \cdot a}{z^2 - 2 \cos \Omega_1 \cdot za + a^2}$$

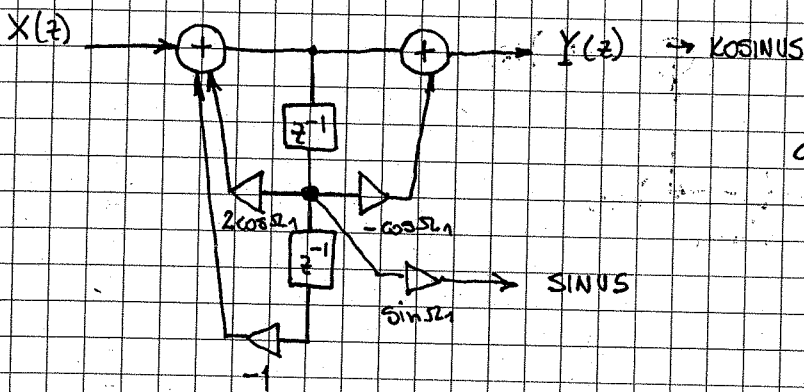
$$Y(z) (1 - 2 \cos \Omega_1 a z^{-1} + a^2 z^{-2}) = X(z) (1 - \cos \Omega_1 a z^{-1})$$

$$Y(z) = X(z) - a \cos \Omega_1 X(z) z^{-1} + 2a \cos \Omega_1 Y(z) z^{-1} - a^2 Y(z) z^{-2}$$

$$\text{če je } a=1: Y(z) = X(z) - \cos \Omega_1 X(z) z^{-1} + 2 \cos \Omega_1 Y(z) z^{-1} - Y(z) z^{-2}$$



direktna str. I.



direktna str. II.

$$h[n] = a^n \cdot \sin(\Omega_1 n) u[n] \dots \text{sinus}$$

$$\sin \theta = \frac{1}{2j} (e^{j\theta} - e^{-j\theta})$$

$$H(z) = \frac{1}{2j} \left(\sum_{n=0}^{\infty} a^n e^{j\Omega_1 n} z^{-n} - \sum_{n=0}^{\infty} a^n e^{-j\Omega_1 n} z^{-n} \right) =$$

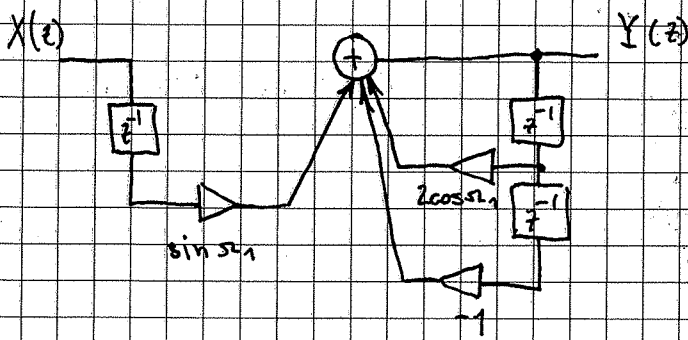
$$= \frac{1}{2j} \left(\frac{1}{1 - a e^{j\Omega_1} z^{-1}} - \frac{1}{1 - a e^{-j\Omega_1} z^{-1}} \right) = \frac{1}{2j} \frac{1 - a e^{-j\Omega_1} z^{-1} - 1 + a e^{j\Omega_1} z^{-1}}{1 - a z^{-1} (2 \cos \Omega_1) + a^2 z^{-2}}$$

$$= \frac{1}{2j} \frac{a z^{-1} (2j \sin \Omega_1)}{1 - 2a \cos \Omega_1 z^{-1} + a^2 z^{-2}} = \frac{a z^{-1} \sin \Omega_1}{1 - 2a \cos \Omega_1 z^{-1} + a^2 z^{-2}}$$

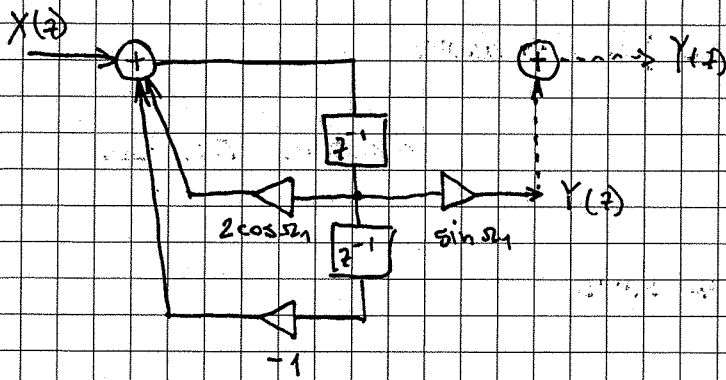
$$Y(z) = a \sin \Omega_1 X(z) z^{-1} + 2a \cos \Omega_1 Y(z) z^{-1} - a^2 Y(z) z^{-2}$$

za $a=1$:

$$Y(z) = \sin \Omega_1 X(z) z^{-1} + 2 \cos \Omega_1 Y(z) z^{-1} - Y(z) z^{-2}$$

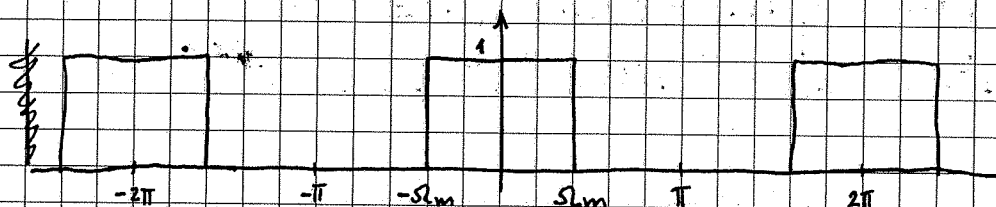


direktna str. I.



18. Naloga

Izračunajte koeficiente nizkega FIR sira 8. reda $h[n]$ z
mejno normirano krožno frekvenco $\Omega_m = \frac{\pi}{4}$.



$H(\omega)$ namo

IDFT

$$h[n] = \frac{1}{2\pi} \int_{-\pi}^{\pi} H(\omega) e^{+j\omega n} d\omega \quad \dots \text{inv. Fourier transf.}$$

$$h[n] = \frac{1}{2\pi} \int_{-\Omega_m}^{\Omega_m} e^{+j\omega n} d\omega = \frac{1}{2\pi} \left[\frac{e^{+j\omega n}}{jn} \right]_{-\Omega_m}^{\Omega_m}$$

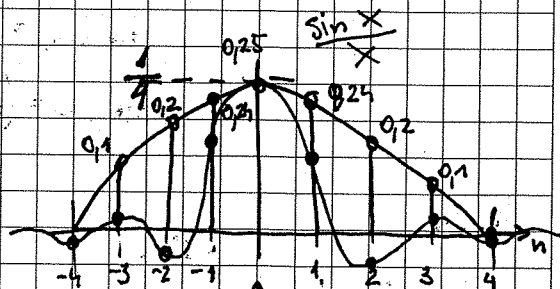
$$= \frac{1}{j2\pi n} \left(e^{j\Omega_m n} - e^{-j\Omega_m n} \right) =$$

$$h[n] = \frac{\sin(\Omega_m n)}{j\pi n}$$

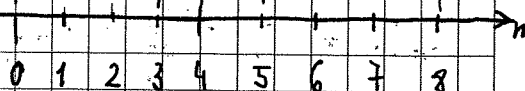
$$h[n] = \frac{\Omega_m}{\pi} \frac{\sin(\Omega_m n)}{\Omega_m n}$$

$$h[n] = \frac{\pi}{4\pi} \frac{\sin\left(\frac{\pi n}{4}\right)}{\frac{\pi n}{4}}$$

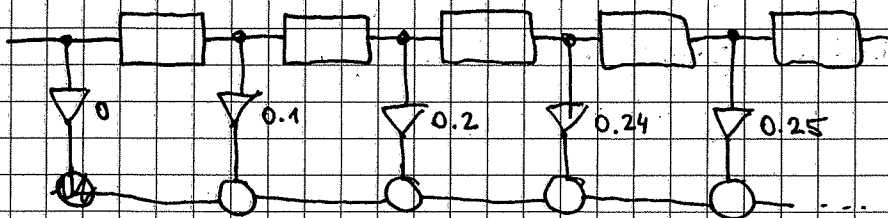
$$h[n] = \{0, 0.1, 0.2, 0.25, 0.24, 0.2, 0.1, 0\}$$



ker je 8. reda - 9 koeficient

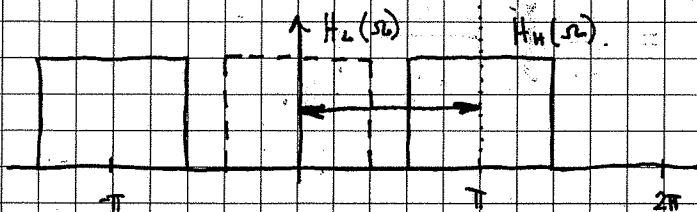


Shema:



19. NALOGA

Izračunajte koeficiente visokega FIR sita 8. reda $h_v[n]$ z mejno normalizirano krožno frekvenco $\omega_m = \frac{4\pi}{5}$. Za izhodisce uporabite koeficiente nizkega sita $h_n[n] = \frac{\omega_m}{\pi} \frac{\sin(\omega_m n)}{\omega_m n}$.



$$H_H(\omega) = H_L(\omega - \pi)$$

$$H_H^*(\omega) = H_L(\omega + \pi)$$

$$H_H(\omega) = (H_L(\omega - \pi) + H_L(\omega + \pi)) / 2$$

delimo z 2, ker
dobimo dvojni spekter
zaradi obeh premikov

$$h_v[n]$$

$$h_v^-[n] = h_n[n] e^{-j\pi n}$$

$$h_v^+[n] = h_n[n] e^{j\pi n}$$

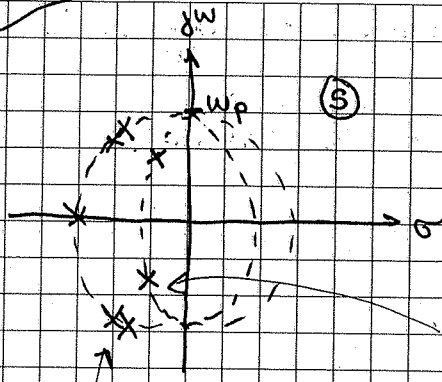
$$h_v[n] = \frac{h_n[n]}{2} \cdot (e^{-j\pi n} + e^{j\pi n}) = \frac{h_n[n]}{2} \cdot 2 \cos(\pi n)$$

$$h_v[n] = \frac{1}{4} \frac{\sin \frac{n\pi}{5}}{\frac{n\pi}{5}} \cdot \cos \pi n \quad \dots \text{za podatke iz prejsne naloge}$$

$$h_v[n] = \frac{1}{5} \frac{\sin \frac{n\pi}{5}}{\frac{n\pi}{5}} \cos \pi n \quad \dots \text{za podatke iz te naloge}$$

112 filteri:

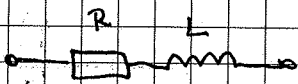
9.5.2013



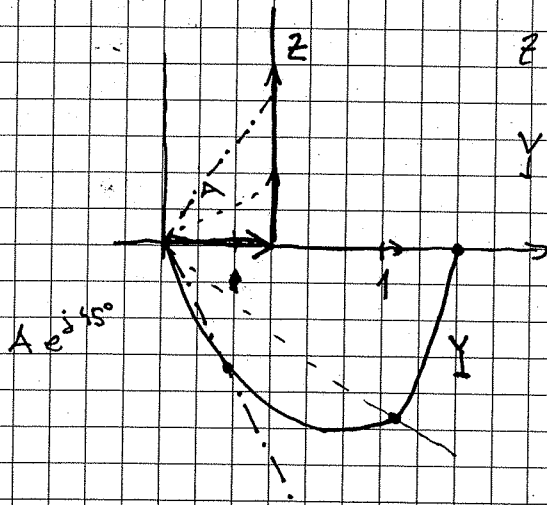
ω_p ... programna frez

Chebisev filter 2. reda (elipsa)

Butterworthov filter 2. reda (kroznica)
3. reda



INVERTIRANJE



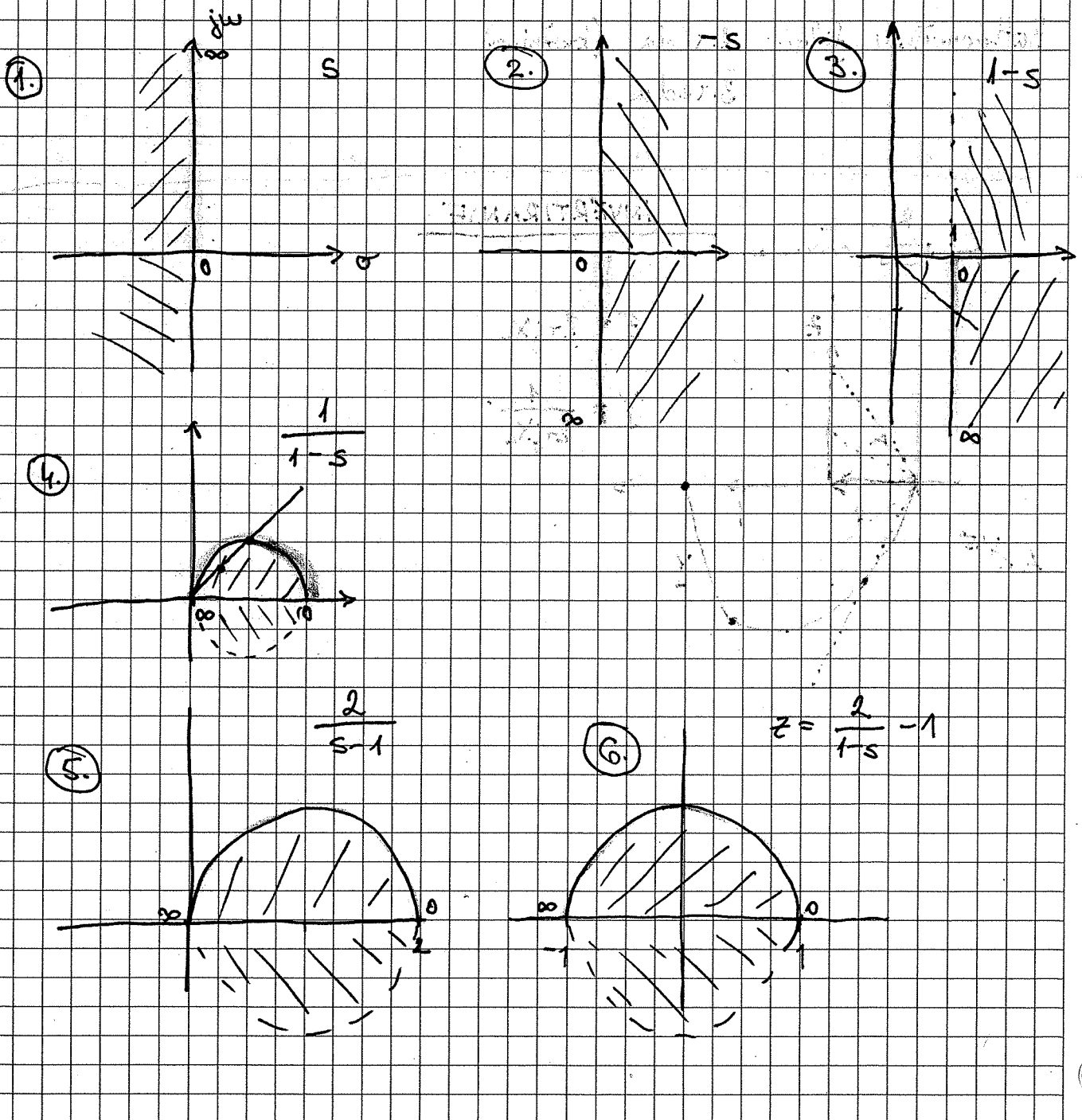
$$Z = R + jX_L$$

$$Y = \frac{1}{R + jX_L}$$

2 Invertiranjem pokažite kako bi linearna transformacija

$$z = \frac{1+s}{1-s} \text{ preslika } s \text{ ravnino u } z \text{ ravnino}$$

$$z = \frac{1+s}{1-s} = \frac{-(1-s)+2}{1-s} = \frac{2}{1-s} - 1$$



13 formule $z(s)$ izrazimo $S(z)$

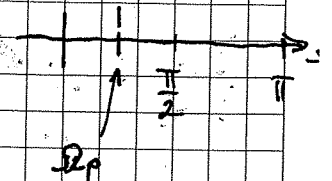
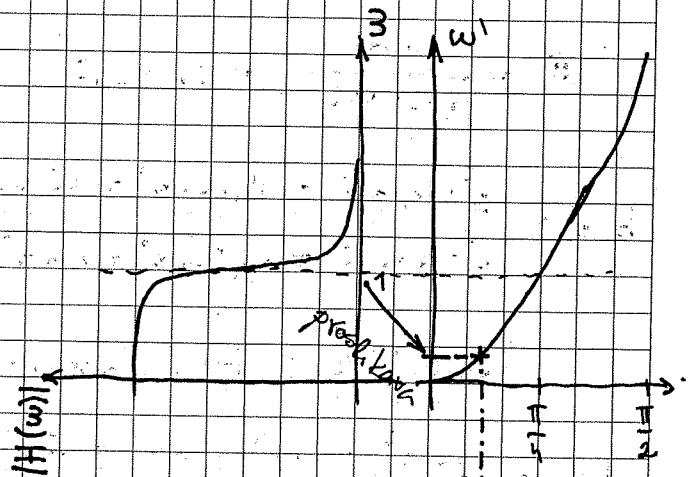
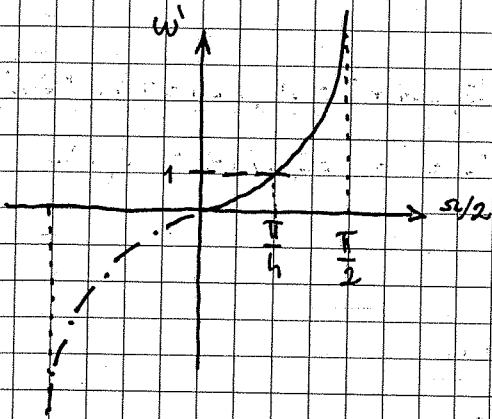
$$S = 1 - \frac{z}{z+1} = \frac{z+1-z}{z+1} = \frac{z-1}{z+1}$$

$$z = e^{j\omega}$$

$$S = j\omega'$$

$$j\omega' = \frac{e^{j\frac{\omega'}{2}} - 1}{e^{j\frac{\omega'}{2}} + 1} = \frac{e^{j\frac{\omega'}{2}} (e^{j\frac{\omega'}{2}} - e^{-j\frac{\omega'}{2}})}{e^{j\frac{\omega'}{2}} (e^{j\frac{\omega'}{2}} + e^{-j\frac{\omega'}{2}})} = \frac{j \sin \frac{\omega'}{2}}{\cos \frac{\omega'}{2}}$$

$$\omega' = \tan \frac{\omega}{2}$$



$$\omega' = \frac{\omega}{\omega_N}$$

$$\omega_p' = \frac{\omega_p}{\omega_N} = \tan \frac{\omega_p}{2}$$

$$\frac{1}{\omega_N} = \tan \frac{\omega_p}{2}$$

$$\omega_N = \frac{1}{\tan \frac{\omega_p}{2}}$$

p_{s1}, p_{s2} $S = \frac{B}{W_N} \leftarrow$ mali s

$$z = \frac{1+s}{1-s} = \frac{z}{1-s} + 1$$

(pazi izrazimo na kalkulator)

bo. velikost filtra

$$p_{z1} = \frac{1 + \frac{p_{s1}}{\omega_N}}{1 - \frac{p_{s2}}{\omega_N}}$$

$$p_{z2} = \frac{1 + \frac{p_{s2}}{\omega_N}}{1 - \frac{p_{s2}}{\omega_N}}$$

$$H(z) = b_0 \frac{(z+1)(z+1)}{(z-p_{z1})(z-p_{z2})}$$

Akta $b_0 = \frac{1}{|H(e^{j\omega})|}$

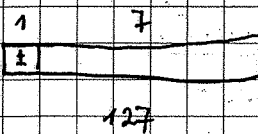
16.5.2013

24. naloga

LT1 sistem ima podano sistemsko funkcijo:

$$H(z) = \frac{z^5 - 2,5247147 z^4 + 1,573690 z^3 + 1,5736901 z^2 - 2,5247147 z + 1}{z^5 - 7,4135352 z^4 + 7,890889 z^3 - 7,1347574 z^2 + 3,259790 z - 0,6016686}$$

Koeficiente zapišite z osmimi bitmi.



množimo ulomek z tako številko, da bo najvišji koeficient enak 127

$$\textcircled{1} = \frac{127}{7,890889} = 16,0945$$

množimo $H(z) \cdot \textcircled{1}$

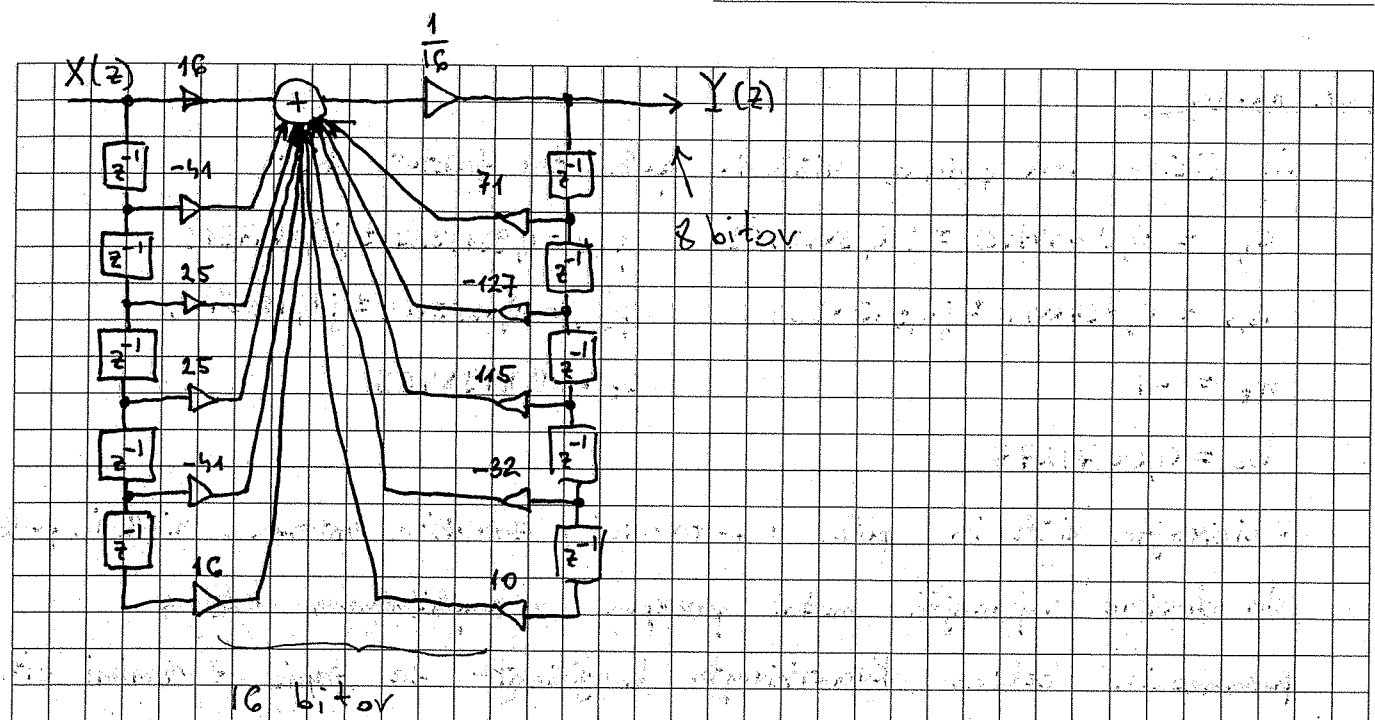
$$H(z) = \frac{z^5 \cdot 16,0945 - 40,634 z^4 + 25,327 z^3 + 25,327 z^2 - 40,634 z + 16,0945}{z^5 \cdot 16,0945 - 71,033 z^4 + 127 z^3 - 114,83 z^2 + 32,464 z - 9,683}$$

sedaj vse cifre zaokrožimo

$$H(z) = \frac{16 z^5 - 41 z^4 + 25 z^3 + 25 z^2 - 41 z + 16}{16 z^5 - 71 z^4 + 127 z^3 - 115 z^2 + 32 z - 10}$$

$$\frac{Y(z)}{X(z)} = \frac{16 z^5 - 41 z^4 + 25 z^3 + 25 z^2 - 41 z + 16}{16 z^5 - 71 z^4 + 127 z^3 - 115 z^2 + 32 z - 10}$$

$$16 Y(z) = 16 X(z) - 41 X(z) z^{-1} + 25 X(z) z^{-2} + 25 X(z) z^{-3} - 41 X(z) z^{-4} + 16 X(z) z^{-5} + 71 Y(z) z^{-1} - 127 Y(z) z^{-2} + 115 Y(z) z^{-3} - 32 Y(z) z^{-4} + 10 Y(z) z^{-5}$$



24. naloga

LTI sistem ima podane ničle in pole ter faktor b_0 :

$$n_{1,2} = 0,9244760 \pm j0,3812603$$

$$p_{1,2} = 0,9343337 \pm j0,2647313$$

$$n_{3,4} = 0,8378914 \pm j0,5458527$$

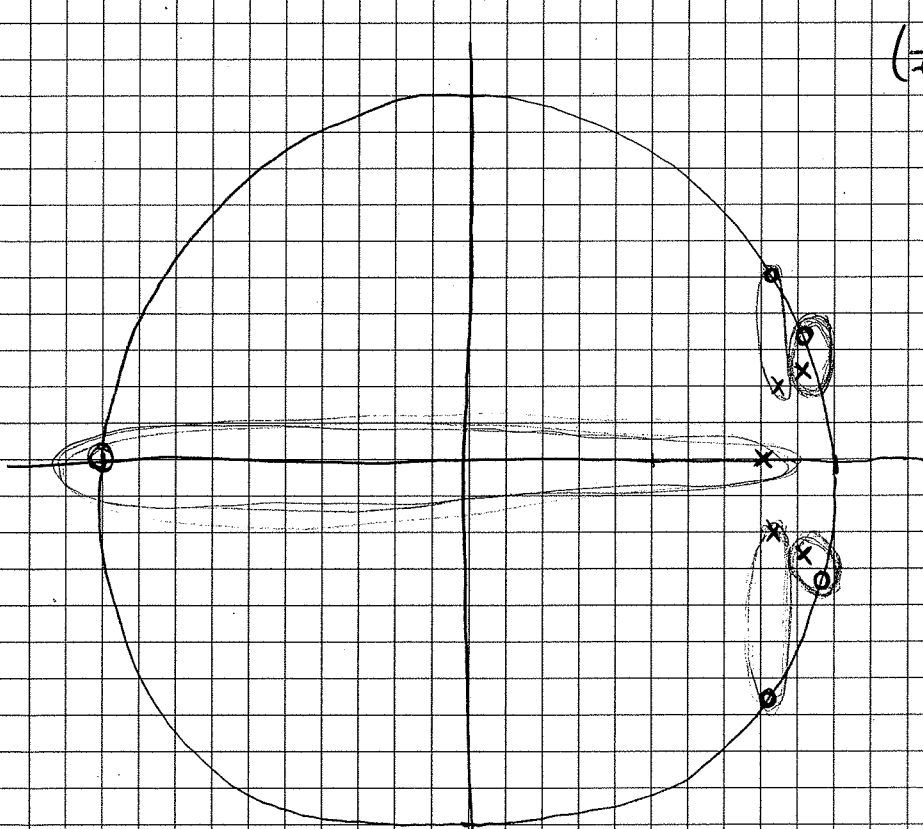
$$p_{3,4} = 0,8655104 \pm j0,1836447$$

$$n_5 = -1$$

$$p_5 = 0,8198469$$

$$b_0 = 0,0071273$$

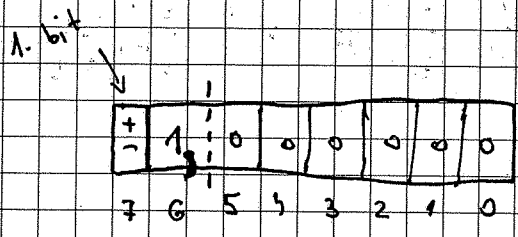
Skicirajte ničle in pole v z -ravnini, združite ustrezne ničle in pole, da dobimo najmanjši možni prevezan v amplitudnem odzivu posameznih celic. Kvantizirajte koeficiente za zapis z osmimi biti.



$$\begin{aligned}(z - a - jb)(z - a + jb) &= \\ &= z^2 - 2az + (a^2 + b^2)\end{aligned}$$

Naredimo 2 sistema drugega reda in 1 sistem prvega reda

$$H(z) = b_0 \frac{(z-n_1)(z-n_2)}{(z-p_1)(z-p_2)} = \frac{z^2 - \overbrace{(n_1+n_2)}^{\text{vedno } < 2} z + \overbrace{n_1 n_2}^{\leq 1}}{z^2 - \overbrace{(p_1+p_2)}^{\text{vedno } < 2} z + \overbrace{p_1 p_2}^{\leq 1}}$$



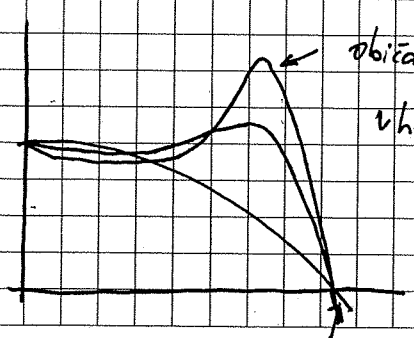
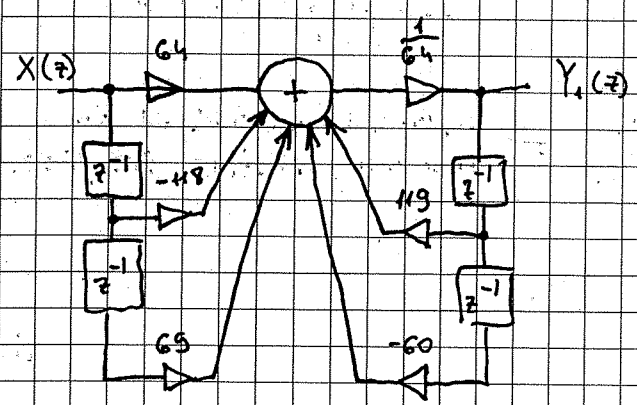
če imamo dvojno ničlo, jo realiziramo kot Z sistema prvega reda

$$H_1(z) = \frac{z^2 - 1,848952 \cdot z + 1}{z^2 - 1,8626674 \cdot z + 0,937465}$$

$$= \frac{64 - 118,3 z^{-1} + 64 z^{-2}}{64 - 119,2 z^{-1} + 59,3 z^{-2}}$$

vse množimo z 64 in z z⁻²

$$64 Y_1(z) = 64 X_1(z) - 118 X_1(z) z^{-1} + 64 X_1(z) z^{-2} + 119 Y_1(z) z^{-1} - 60 Y_1(z) z^{-2}$$



običajno se da bo pred vhod v sistema ki ima največjo špic

1. red

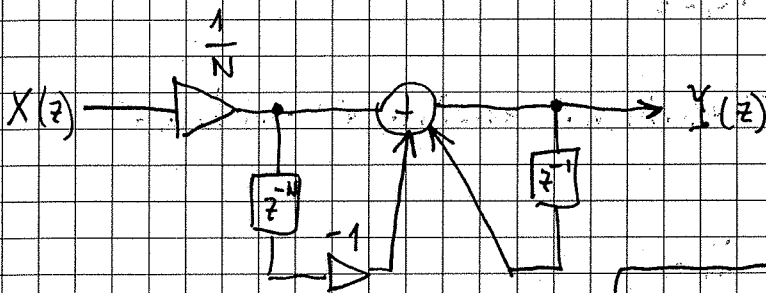
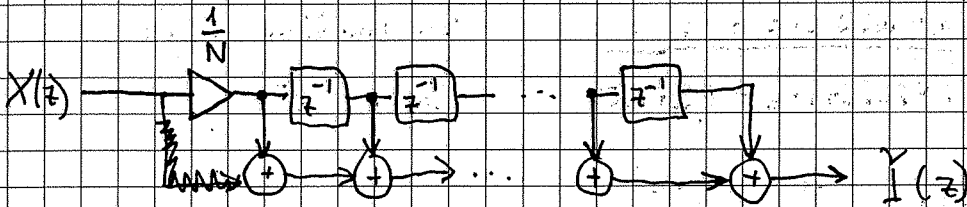
23.5.2013

POVPREČEVALNIK - da odstranimo enosmerno komponento

N

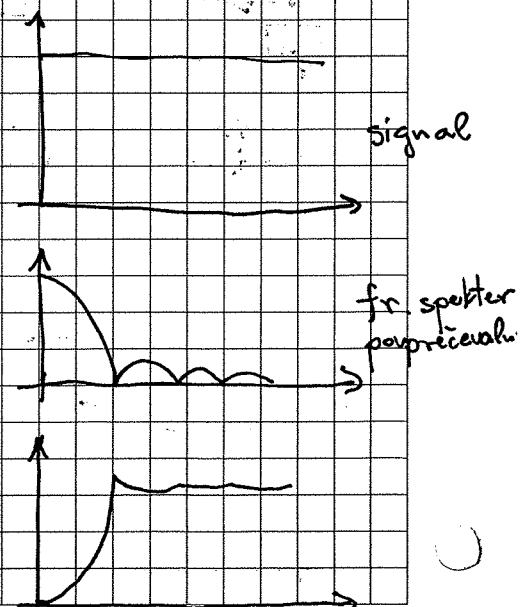
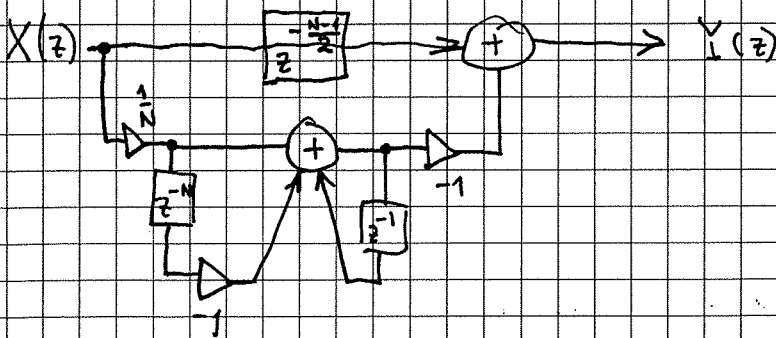
$$H(z) = \frac{1}{N} \sum_{n=0}^{N-1} z^{-n} = \frac{1}{N} \frac{1 - z^{-N}}{1 - z^{-1}} = \frac{1}{N} \frac{z^N - 1}{z^N - z^{N-1}} = \frac{1}{N} \frac{z^N - 1}{z^{N-1}(z-1)}$$

$$Y(z) = \frac{1}{N} (X(z) - X(z)z^{-N}) + Y(z)z^{-1}$$



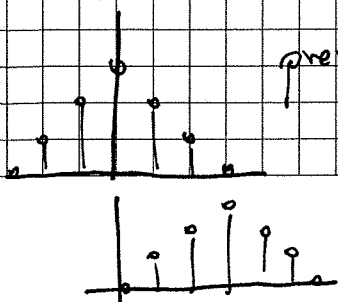
... povprečevalnik

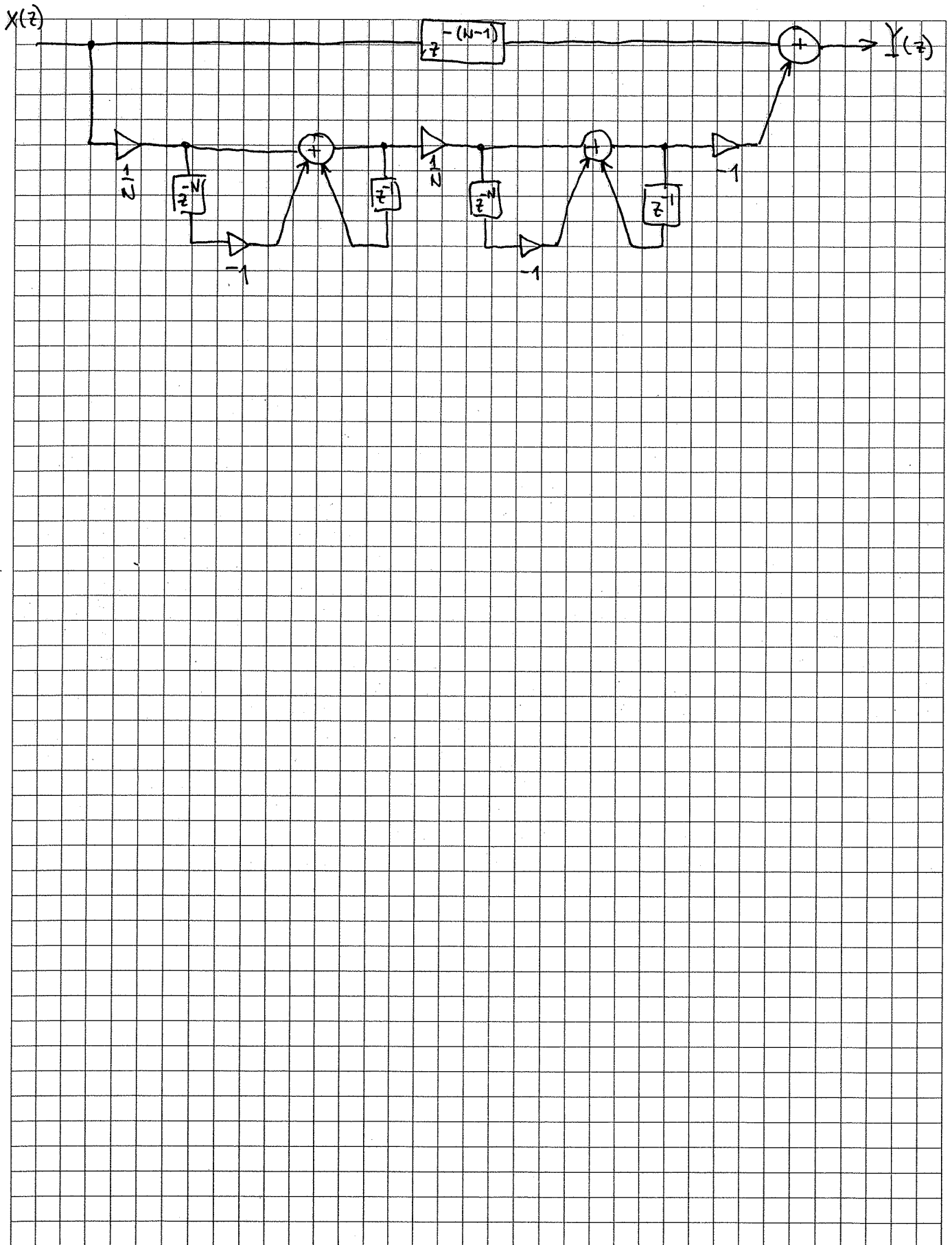
$\frac{N-1}{2} \equiv$ SIGNAL JE ZAMAKNJEJ ZA POLOVICO DOŽINE FIR filtra



premaknemo za $\frac{N-1}{2}$

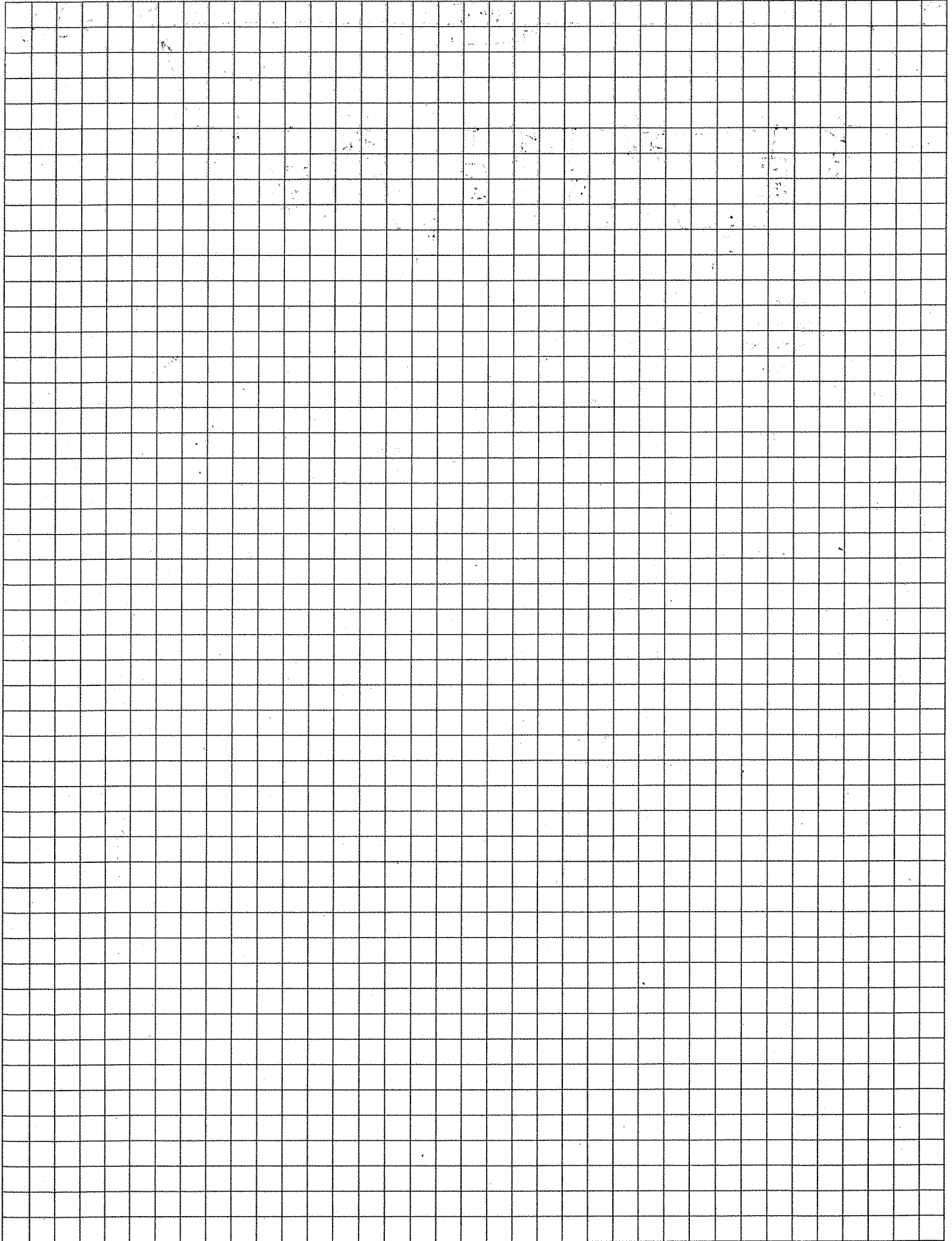
zato zamaknemo tudi člen v filtra





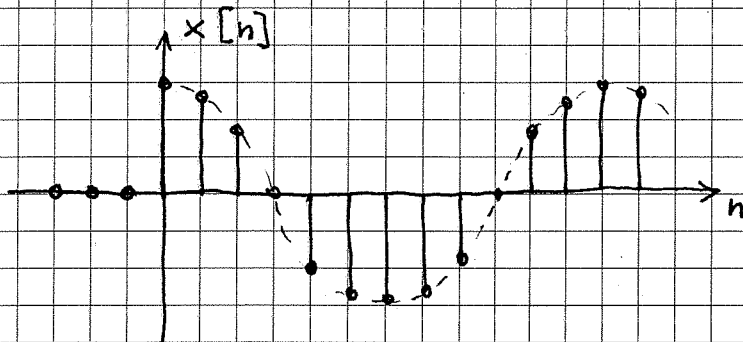
DSS 2.60

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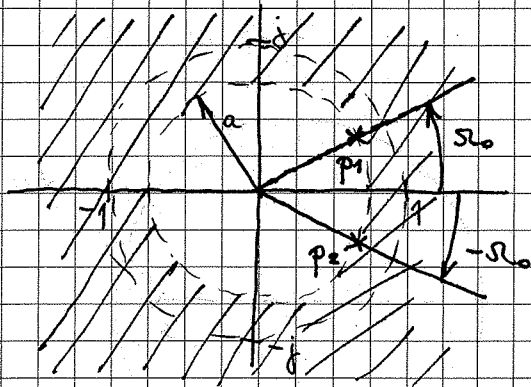


4. Dušeni kosinusni signal

$$x[n] = (a^n \cos(\Omega_0 n)) \cdot u[n]$$



$$\longleftrightarrow \frac{z(z - a \cos \Omega_0)}{z^2 - 2a \cos \Omega_0 z + a^2}$$



območje konvergence

5. Dušeni sinusni signal

$$x[n] = (a^n \sin \Omega_0 n) u[n] \longleftrightarrow \frac{z \cdot a \sin \Omega_0}{z^2 - 2a \cos \Omega_0 z + a^2}$$

$$|z| > |a|$$

ZGLED PRAVILA O ODVAJANJU (stran 25-2)

$$X(z) \leftrightarrow x[n]$$

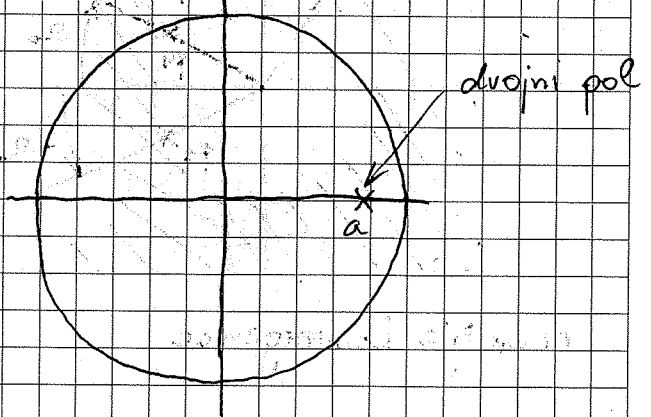
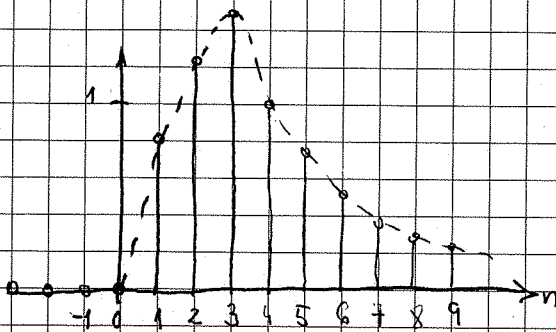
$$-z \frac{dX(z)}{dz} \leftrightarrow nx[n]$$

$$x[n] = a^n \cdot u[n] \quad |a| < 1$$

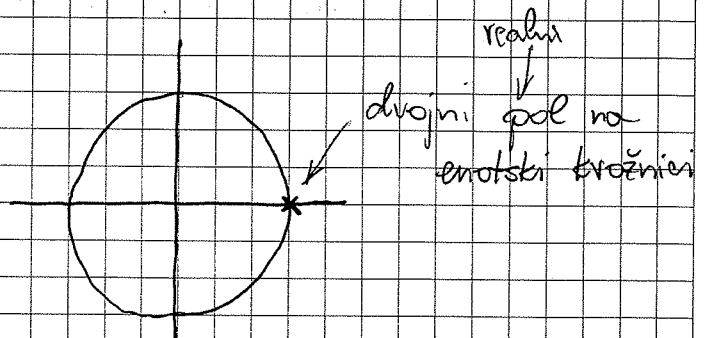
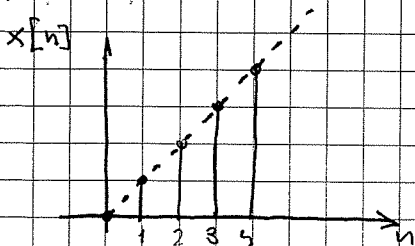
$$X(z) = \frac{1}{1-az^{-1}} = \frac{z}{z-a}$$

$$-z \frac{dX(z)}{dz} = -z \frac{z-a-z}{(z-a)^2} = \frac{az}{(z-a)^2} \leftrightarrow (n a^n) u[n]$$

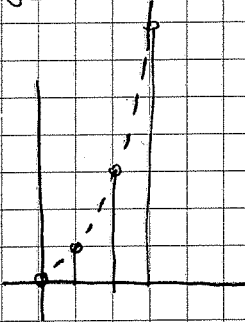
graf za $a = 0.8$



če je $a = 1$, potem:



če je $a > 1$

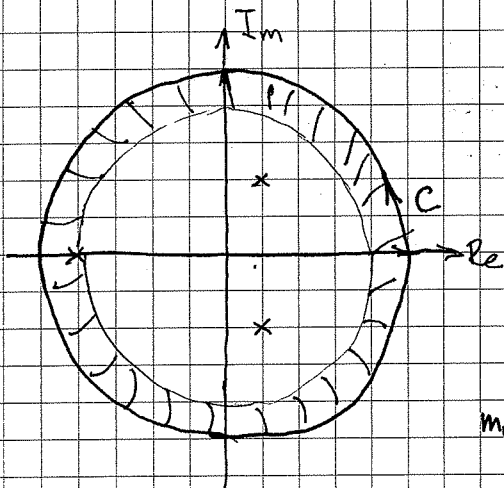


dvajni pol izven območja konvergence

5.5.5. INVERZNA Z - TRANSFORMACIJA

$$x[n] = \frac{1}{2\pi j} \oint_C x(z) z^{n-1} dz$$

C ... sklenjena krivulja v ROC in okrožna izhodišče v pozitivnem smislu



$$X[n] = \sum_{i=1}^M \operatorname{Res}_{z=p_i} [x(z) \cdot z^{n-1}]$$

$$\operatorname{Res}_{z=p_i} [x(z) z^{n-1}] = \lim_{z \rightarrow p_i} \left[\frac{1}{(m_i-1)!} \frac{d^{(m_i-1)}}{dz^{(m_i-1)}} (z-p_i)^{m_i} x(z) \right]$$

m_i j red pola p_i

za $m_i = 1$: $\operatorname{Res}_{z=p_i} [x(z) z^{n-1}] = \lim_{z \rightarrow p_i} [(z-p_i) x(z) z^{n-1}]$

$m_i = 2$: $\operatorname{Res}_{z=p_i} [x(z) z^{n-1}] = \lim_{z \rightarrow p_i} \left[\frac{d}{dz} \left((z-p_i)^2 \cdot x(z) z^{n-1} \right) \right]$

Zgled:

$$X(z) = \frac{z}{z-a} \quad \text{ROC} \quad |z| > |a|$$

$$X[n] = \text{Res}_{z=a} \left[\frac{z}{z-a} z^{n-1} \right] = \lim_{z \rightarrow a} \left(\cancel{(z-a)} \frac{z}{\cancel{(z-a)}} z^{n-1} \right)$$

Konvergenca zahteva, da velja $n \geq 0$

$$X[n] = a^n \quad \text{za } n \geq 0$$
$$\emptyset \quad \text{za } n < 0$$

Zgled: uporaba tabele z-transformacij

$$X(z) = \frac{3 \cdot z}{(z-0,6)(z+0,5)} \quad \text{ROC} \quad |z| > 0,6 \quad \dots \text{ desnostranski signal}$$

$$X(z) = \frac{A}{z-0,6} + \frac{B}{z+0,5} = \frac{Az+0,5A+Bz-0,6B}{(z-0,6)(z+0,5)}$$

$$A+B=3$$

$$0,5A-0,6B=0$$

$$A=3-B = \frac{18}{11}$$

$$2,2B=3$$

$$B = \frac{3}{2,2} = \frac{15}{11}$$

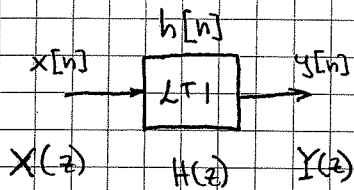
$$X(z) = \frac{11}{11} \frac{1}{z-0,6} + \frac{15}{11} \frac{1}{z+0,5}$$

↓ ZT

$$X[n] = \frac{18}{11} \cdot 0,6^{n-1} \cdot u[n-1] + \frac{15}{11} \cdot 0,5^{n-1} \cdot u[n-1]$$

5.6. SISTEMSKA FUNKCIJA $H(z)$

5.6.1. DEFINICIJA SISTEMSKE FUNKCIJE



$$y[n] = x[n] * h[n]$$

↑ ZT

$$Y(z) = X(z) \cdot H(z)$$

1. $H(z)$ je z-transform impulznega odziva "mrtvega" sistema
zakasnilni elementi so 0 za $n \leq 0$

$$H(z) = \sum_{n=0}^{\infty} \{h[n]\} z^{-n}$$

$$2. H(z) = \frac{Y(z)}{X(z)}$$

5.6.2. DOLOČANJE $H(z)$

1. Iz poznanega impulznega odziva

$$H(z) = \sum_{n=-\infty}^{\infty} h[n] z^{-n}$$

za kausalne odzive $H(z) = \sum_{n=0}^{\infty} h[n] \cdot z^{-n}$

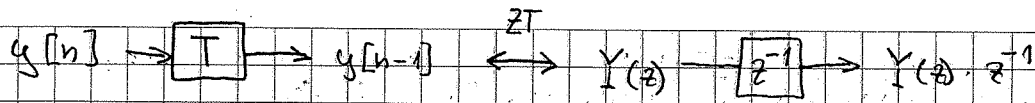
2. Iz bločne sheme v z-prostoru

- sestevalniki in množilniki ostanejo nespremenjeni
- zakasnilni elementi se spremenijo v množilnike

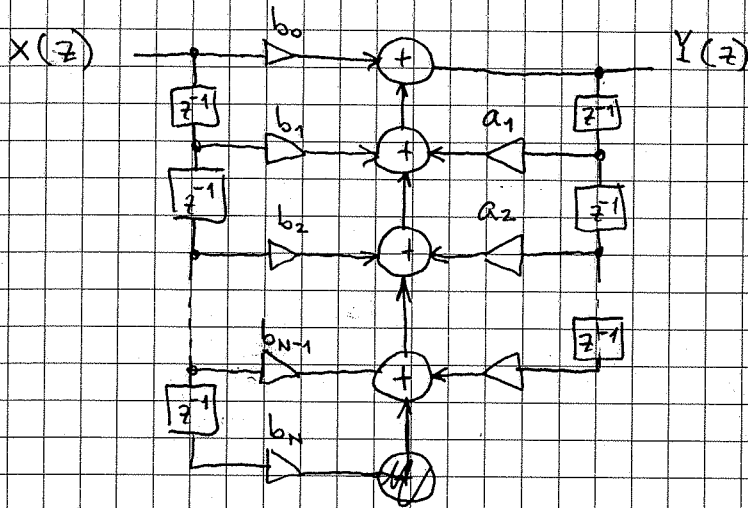
$$y[n-m] \longleftrightarrow z^{-m} Y(z)$$

Alta®

18.4.2013



Direktna struktura I v z-prostoru



3. Z transformacija diferencne enačbe

$$y[n] = \sum_{i=0}^N b_i x[n-i] + \sum_{j=1}^M a_j y[n-j]$$

z transf

$$Y(z) = \sum_{i=0}^N b_i X(z) z^{-i} + \sum_{j=1}^M a_j Y(z) z^{-j}$$

$$\frac{Y(z)}{X(z)} = H(z) = \frac{\sum_{i=0}^N b_i z^{-i}}{\sum_{j=0}^M a_j z^{-j}}$$

5.6.3. POLI IN NIČE SISTEMSKÉ FUNKCIJE

$$H(z) = \frac{z^N}{z^M} \cdot z^{M-N} = \frac{\sum_{i=0}^N b_i z^{N-i}}{z^M - \sum_{j=1}^M a_j z^{M-j}} \cdot z^{M-N}$$

$$H(z) = b_0 \frac{z^N + \frac{b_1}{b_0} z^{N-1} + \frac{b_2}{b_0} z^{N-2} + \dots + \frac{b_N}{b_0}}{z^M - a_1 z^{M-1} - a_2 z^{M-2} - \dots - a_M} \cdot z^{M-N}$$

Niče polinoma v števcu ($N(z)$) so ničle sistemske funkcije

$$z_i \quad ; \quad i = 1, 2, \dots, N$$

$$H(z_i) = 0$$

Poli so ničle polinoma v imenovalcu ($D(z)$)

$$p_j \quad ; \quad j = 1, 2, \dots, M$$

$$|H(p_j)| \rightarrow \infty$$

$$H(z) = b_0 \frac{(z-z_1)(z-z_2)\dots(z-z_N)}{(z-p_1)(z-p_2)\dots(z-p_M)} z^{M-N}$$

ničle in poli določajo $H(z)$ do multiplikativne

konstante natančno

5.6.4. VPLIV LEGE POLOV IN NIČEL $H(z)$ NA

LASTNOSTI SISTEMA

① STABILNOST

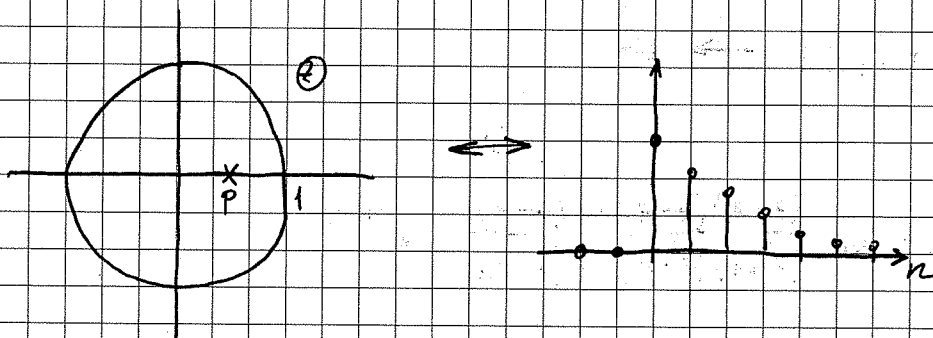
Sistem je stabilen, če so vsi poli v notranjosti enotske krožnice

$$|p_j| < 1 \quad \text{za} \quad j = 1, \dots, M$$

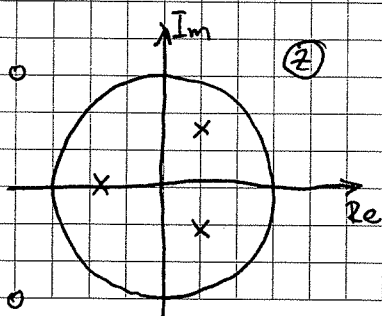
Je potreben in zadosten pogoj.

$$H(z) = \sum_{j=1}^M \frac{A_j \cdot z}{z - p_j} \quad \longleftrightarrow \quad h[n] = \sum_{j=1}^M A_j \cdot p_j^n \cdot u[n]$$

razbijemo na vsoto delnih ulomkov



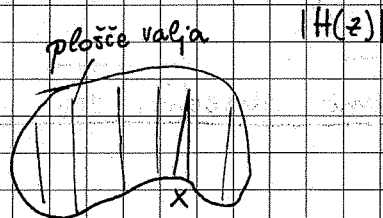
Ničle ne vplivajo na stabilnost - ležijo lahko kjerkoli



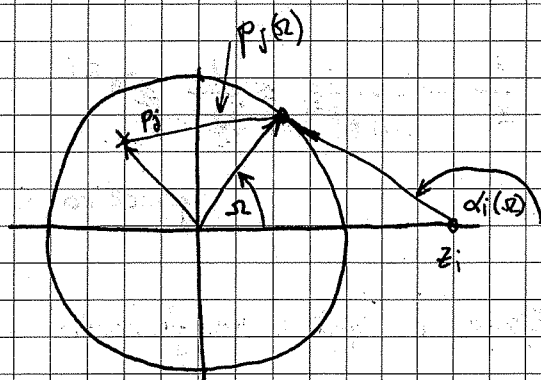
② POLI IN NULE DO KONSTANTE b_0 NATAČNO DOKOČAJO
 FREKVENČNI ODZIV $H(\omega)$

$$H(z) = \frac{\prod_{i=1}^N (z-z_i)}{\prod_{j=1}^M (z-p_j)} \cdot z^{M-N} \quad \prod \dots \text{produkt}$$

$$H(\omega) = H(z) \Big|_{z=e^{j\omega}} = b_0 \frac{\prod_{i=1}^N (e^{j\omega} - z_i)}{\prod_{j=1}^M (e^{j\omega} - p_j)} \cdot e^{j\omega(M-N)}$$



poli v bližini enotske krožnice povečujejo odziv



$$e^{j\omega} - z_i = z_i(\omega) = |z_i(\omega)| e^{j\alpha_i(\omega)}$$

$$e^{j\omega} - p_j = p_j(\omega) = |p_j(\omega)| e^{j\beta_j(\omega)}$$

$$H(\omega) = b_0 \frac{\prod_{i=1}^N z_i(\omega)}{\prod_{j=1}^M p_j(\omega)} e^{j\omega(M-N)}$$

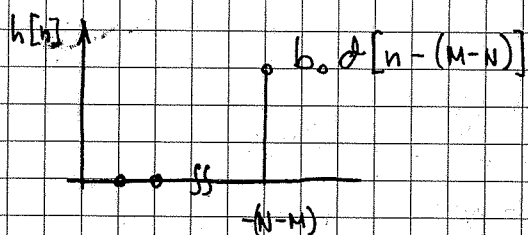
$$H(\omega) = |H(\omega)| e^{j\phi_H(\omega)}$$

$$|H(\omega)| = |b_0| \frac{|z_1(\omega)| |z_2(\omega)| \dots |z_N(\omega)|}{|p_1(\omega)| |p_2(\omega)| \dots |p_M(\omega)|}$$

$$\phi_H(\omega) = \sum_{i=1}^N \alpha_i(\omega) - \sum_{j=1}^M \beta_j(\omega) + \omega(M-N) \pm k\pi \quad k = \begin{cases} 0 & ; b_0 > 0 \\ 1 & ; b_0 < 0 \end{cases}$$

Poli in ničle v izhodšču ne vpliva na amplitudo, ampak le na fazo.

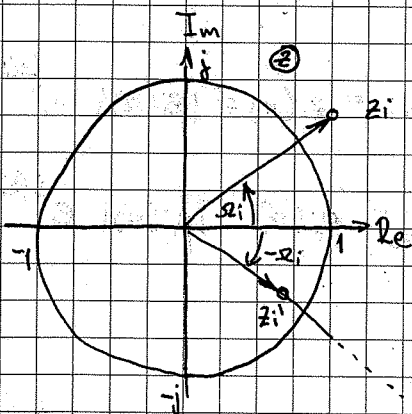
M-N odloča o začetku $h[n]$



$$H(z) = \frac{b_0 z^N}{z^M} z^{M-N} = (b_0 z^{N-M} + (b_1 + b_0 a_1) z^{N-M-1}) z^{M-N}$$

Nemogoče narediti več ničel kot polov (kavzalnost)

3. PRESLIKAVA ("ZRCALJENJE") NIČEL



$$z_i' = \frac{1}{z_i} = \frac{1}{|z_i| e^{j\phi_i}} = \frac{1}{|z_i|} e^{-j\phi_i}$$

preslikava

Zrcaljenje ne vpliva na frekvenčni potek

$$H(z) = H_1(z) \cdot H_2(z) \quad ; \quad H_2(z) = (z - z_i)(z - z_i^*)$$

$$H'(z) = H_1(z) \cdot H_2'(z) \quad ; \quad H_2'(z) = (z - \frac{1}{z_i})(z - \frac{1}{z_i^*})$$

$$H_2'(z) = \frac{z}{z_i} (z_i - \frac{1}{z}) \cdot \frac{z}{z_i^*} (z_i^* - \frac{1}{z}) = \frac{z^2}{|z_i|^2} (z^{-1} - z_i)(z^{-1} - z_i^*)$$

$$H_2'(\omega) = H_2'(z) \Big|_{z=e^{j\omega}} = \frac{e^{j2\omega}}{|z_i|^2} (e^{-j\omega} - z_i)(e^{-j\omega} - z_i^*) = \frac{e^{j2\omega}}{|z_i|^2} H_2(-\omega)$$

$$|H_z'(s)| = \frac{1}{|z_i|^2} |H(-s)| = \frac{1}{|z_i|^2} |H(s)|$$

soda funkcija

amplituda drugačna

potek je isti

$$\phi_z'(s) = 2s - \phi_z(s)$$

fazni potek je drugačen

Za realno ničlo dobimo: $|H_z'(s)| = \frac{1}{|z_i|}$

$$\phi_z'(s) = \pi + s - \alpha_i(s)$$

Sistemi z minimalno fazo imajo vse ničle znotraj enotskega kroga.

Sistemi z maksimalno fazo imajo vse ničle zunaj enotskega kroga.

Ničle na krožnici so same sebi imune - jih nemoremo preslikati

min. faza \rightarrow ničle bližje polov \rightarrow manjša faza

4. FAZNI SUKALNIK (ALL-PASS FILTER (network))

$$|H(\omega)| = \text{konstanta} = 1 \quad \text{za} \quad -\pi < \omega < \pi$$

↑
običajno

1. Vsi poli ležijo znotraj enotske krožnice

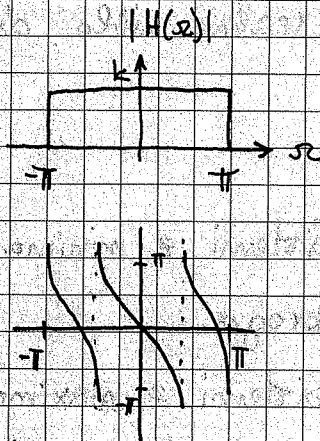
$$|p_j| < 1 \quad j = 1, \dots, M$$

2. Vsak pol je uporjen z ničlo zunaj enotskega kroga

$$z_j = \frac{1}{p_j^*} \quad j = 1, \dots, M$$

za $|H(\omega)| = 1$ moramo izbrati

$$|b_0| = \prod_{j=1}^M |p_j|$$



$$H(z) = \prod_{j=1}^{M/2} \frac{(z - \frac{1}{p_j})(z - \frac{1}{p_j^*})}{(z - p_j)(z - p_j^*)} = \prod_{j=1}^{M/2} H_j(z)$$

$$H_j(\omega) = \frac{(e^{j\omega} - \frac{1}{p_j})(e^{j\omega} - \frac{1}{p_j^*})}{(e^{j\omega} - p_j)(e^{j\omega} - p_j^*)} = \frac{e^{j2\omega} (p_j - e^{-j\omega}) e^{j\omega} (p_j^* - e^{-j\omega})}{p_j (e^{j\omega} - p_j) \cdot p_j^* (e^{j\omega} - p_j^*)} =$$

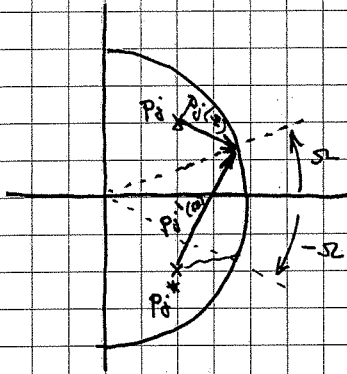
$$= \frac{e^{j2\omega} (e^{-j\omega} - p_j^*)(e^{-j\omega} - p_j)}{|p_j|^2 (e^{j\omega} - p_j)(e^{j\omega} - p_j^*)}$$

$$e^{j\omega} - p_j = p_j(\omega) = |p_j(\omega)| e^{j\beta_j(\omega)}$$

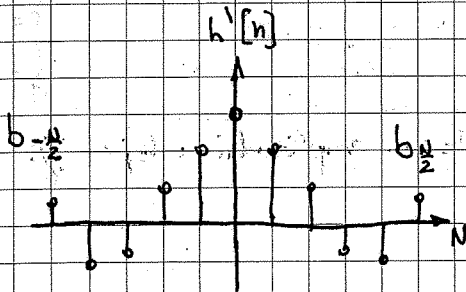
$$e^{-j\omega} - p_j^* = p_j^*(\omega) = |p_j^*(\omega)| e^{-j\beta_j^*(\omega)}$$

$$H_f(\omega) = \frac{e^{j2\omega}}{|p_i|^2} \frac{|p_i| e^{-j\beta_i(\omega)}}{|p_i| e^{j\beta_i(\omega)}} \frac{|p_i'(\omega)| e^{-j\beta_i'(\omega)}}{|p_i'(\omega)| e^{j\beta_i'(\omega)}} =$$

$$= \frac{1}{|p_i|^2} e^{j(2\omega - 2\beta_i(\omega) - 2\beta_i'(\omega))}$$

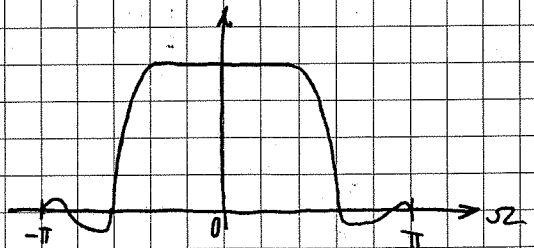


5) SISTEMI Z LINEARNO FAZO

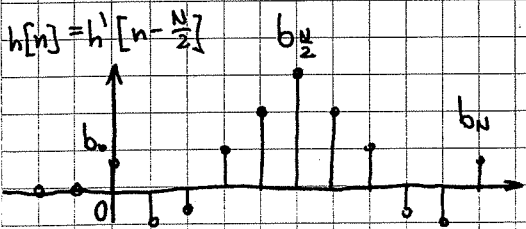


←→
SIMETRIJA

$$H'(\omega) = A(\omega)$$

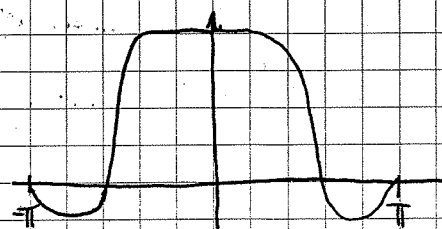


ZAKASNIHO

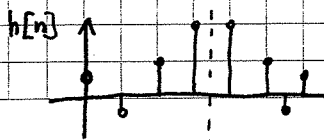


←→
SIMETRIJA

$$H(\omega) = A(\omega) e^{-j\omega \frac{N}{2}}$$



sistem lahko tudi nima enakega



$$|H_0(\omega)| \quad H_0(\omega) = e^{-j\omega \frac{N}{2}}$$

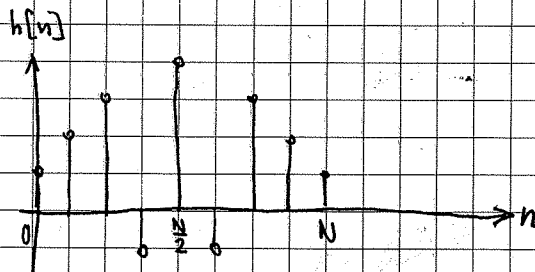
$$\phi_{H_0}(\omega) \quad \phi_{H_0}(\omega) = -\omega \frac{N}{2}$$

22.4.2013

Tip 1 : Simetrični koeficienti $b_i = b_{N-i}$

$N = \text{sod}$ - ostaja centralni impulz $b_{\frac{N}{2}}$

$$H(\Omega) = \sum_{n=0}^N b_n e^{-j\Omega n}$$



$$H(\Omega) = \sum_{n=0}^{\frac{N}{2}-1} b_n e^{-j\Omega n} + b_{\frac{N}{2}} e^{-j\frac{N}{2}\Omega} + \sum_{n=\frac{N}{2}+1}^N b_n e^{-j\Omega n}$$

$$= e^{-j\frac{N}{2}\Omega} \left[b_{\frac{N}{2}} + \sum_{n=0}^{\frac{N}{2}-1} b_n e^{j(\frac{N}{2}-n)\Omega} + \sum_{n=\frac{N}{2}+1}^N b_n e^{+j(\frac{N}{2}-n)\Omega} \right] =$$

$$= e^{-j\frac{N}{2}\Omega} \cdot A(\Omega) \quad \dots \text{amplitudni odziv (je realn)}$$

$$\left. \begin{array}{l} \frac{N}{2} - n = k \quad n = \frac{N}{2} - k \\ k(n=0) = \frac{N}{2} \quad \dots \text{sp. meja} \\ k(n=\frac{N}{2}-1) = 1 \quad \dots \text{zg. meja} \end{array} \right\} \begin{array}{l} \text{substitucija za} \\ \text{prvo vsoto} \end{array}$$

$$\left. \begin{array}{l} \frac{N}{2} - n = -k \quad n = \frac{N}{2} + k \\ k(n=\frac{N}{2}+1) = 1 \quad \text{sp. meja} \\ k(n=N) = \frac{N}{2} \quad \text{zg. meja} \end{array} \right\} \begin{array}{l} \text{substitucija za} \\ \text{drugo vsoto} \end{array}$$

$$A(\omega) = b_{\frac{N}{2}} + \sum_{k=0}^{\frac{N}{2}-1} b_{\frac{N}{2}-k} e^{jk\omega} + \sum_{k=1}^{\frac{N}{2}} b_{\frac{N}{2}+k} e^{-jk\omega}$$

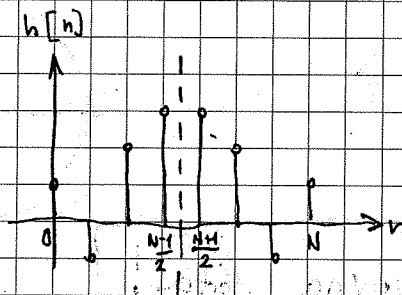
$$= b_{\frac{N}{2}} + \sum_{k=1}^{\frac{N}{2}} b_{\frac{N}{2}-k} (e^{jk\omega} + e^{-jk\omega}) = b_{\frac{N}{2}} + 2 \sum_{k=1}^{\frac{N}{2}} b_{\frac{N}{2}-k} \cdot \cos k\omega$$

odziv amplitudnega dela

Tip 1 je privržen za nizka sira.

Tip 2: Simetrični koeficienti $b_i = b_{N-i}$

$N = \text{lih}$



$$H(\omega) = \sum_{n=0}^N b_n e^{-j\omega n} = e^{-j\frac{N}{2}\omega} \sum_{n=0}^{\frac{N-1}{2}} b_n e^{j(\frac{N}{2}-n)\omega} + e^{-j\frac{N}{2}\omega} \sum_{n=\frac{N+1}{2}}^N b_n e^{j(\frac{N}{2}-n)\omega}$$

substituciji

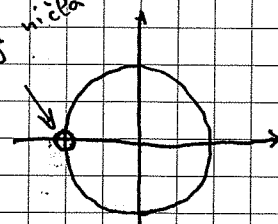
$$\frac{N}{2} - n = k + \frac{1}{2}$$

$$\frac{N}{2} - n = -k - \frac{1}{2}$$

$$A(\omega) = \sum_{k=0}^{\frac{N-1}{2}} b_{\frac{N-1}{2}-k} e^{j(\frac{1}{2}+k)\omega} + \sum_{k=0}^{\frac{N-1}{2}} b_{\frac{N-1}{2}+k} e^{-j(\frac{1}{2}+k)\omega}$$

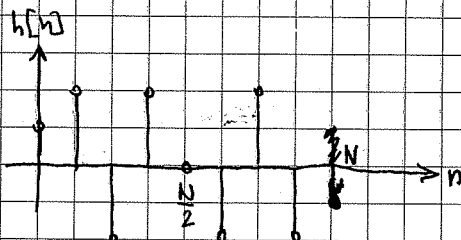
$$A(\omega) = 2 \cdot \sum_{k=0}^{\frac{N-1}{2}} b_{\frac{N-1}{2}-k} \cdot \cos\left(\left(\frac{1}{2}+k\right)\omega\right)$$

vedno 8 ničla tu (obrezna ničla)

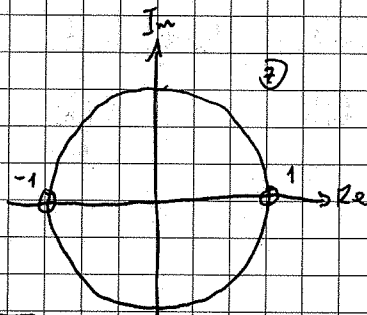
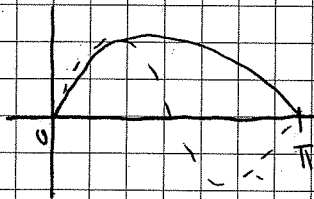


Tip 3: Antisimetrični koeficienti $b_i = -b_{N-i}$

$N = \text{sod}$



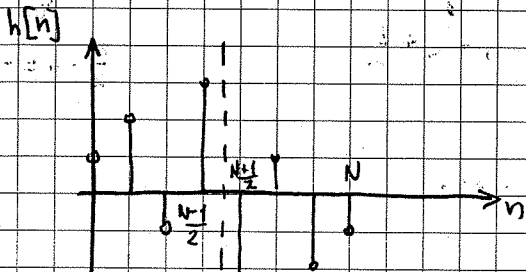
$$A(\omega) = 2 \cdot \sum_{k=1}^{\frac{N}{2}} b_{\frac{N}{2}-k} \sin(k\omega)$$



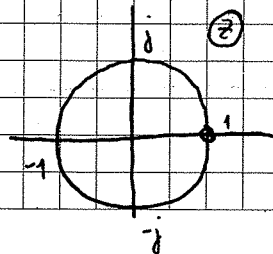
Vežja za pasovna sita!

Tip 4: Antisimetrični koeficienti $b_i = -b_{N-i}$

$N = \text{li}$



$$A(\omega) = 2 \cdot \sum_{k=0}^{\frac{N-1}{2}} b_{\frac{N-1}{2}-k} \sin\left(\left(\frac{1}{2}+k\right)\omega\right)$$



$$H(z) = b_0 + b_1 z^{-1} + b_2 z^{-2} + \dots + b_2 z^{-(N-2)} + b_1 z^{-(N-1)} + b_0 z^{-N}$$

ničle sistemske funkcije

$$b_0 + b_1 \left(\frac{1}{z}\right) + b_2 \left(\frac{1}{z}\right)^2 + \dots + b_2 \left(\frac{1}{z}\right)^{N-2} + b_1 \left(\frac{1}{z}\right)^{N-1} + b_0 \left(\frac{1}{z}\right)^N = 0 \quad | \cdot z^N$$

$$b_0 z^N + b_1 z^{N-1} + b_2 z^{N-2} + \dots + b_2 z^2 + b_1 z + b_0 = 0$$

ničle nastopajo recipročno z_i je ničla $\Rightarrow \frac{1}{z_i}$ je tudi ničla $H(z)$

Vsi poli so v izhodišču (FIR odziv)

Ničle pa nastopajo v recipročnih parih, razen pri ± 1 .

Možne lege ničel:

a.) par na realni osi: $z = a$ in $z = \frac{1}{a}$

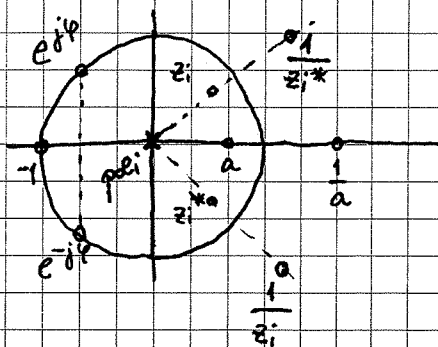
b.) kompleksno konjugiran par na enotski krožnici

$$z = e^{j\varphi} \quad \text{in} \quad z = e^{-j\varphi}$$

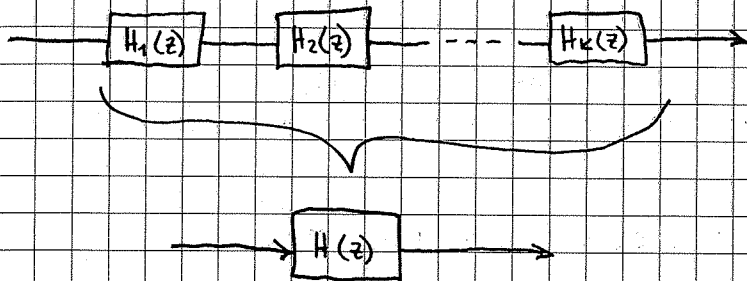
c.) kompleksno konjugiran par izven krožnice (štiri kompl. ničle)

$$|z| \neq 1$$

$$z_i, z_i^* \quad ; \quad \frac{1}{z_i}, \frac{1}{z_i^*}$$



⑥. KASKADNA VEZAVA SISTEMOV



$$H(z) = H_1(z) \cdot H_2(z) \cdot \dots \cdot H_k(z)$$

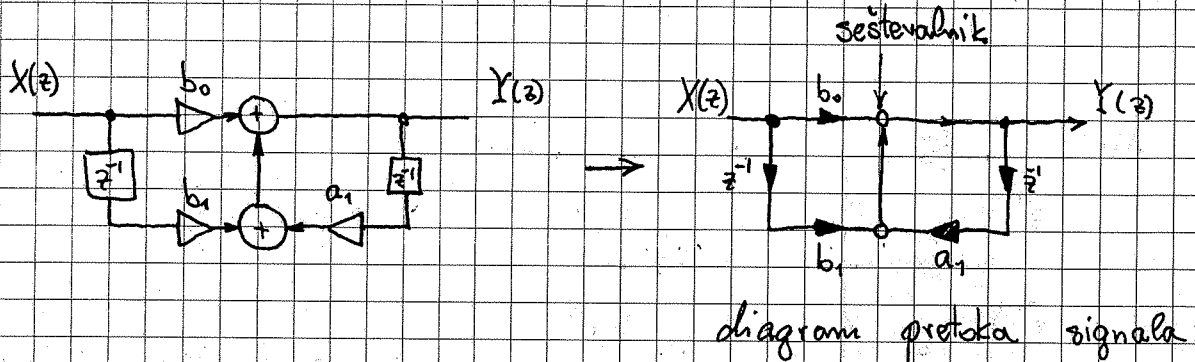
⑦. Vzorčni sistemi imajo število polov večje, večjemu enako število ničel

$$M \cong N$$

6. DISKRETNİ FILTRI

6.1. BLOČNA SCHEMA IN DIAGRAM PRETOKA SIGNALOV

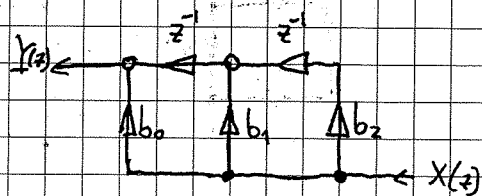
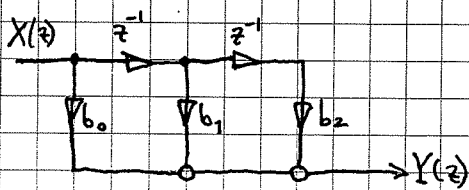
(signal flow graph)



6.1.1. TRANSPOZICIJA DIAGRAMA PRETOKA

- obrnemo smeri pretoka v vseh vejah
- razvejišče spremenimo v seštevalnik
- seštevalniki postanejo razvejišča
- položaj sponke vhodnega in izhodnega se zamenjata

FIR filter : $Y(z) = b_0 + b_1 z^{-1} + b_2 z^{-2}$

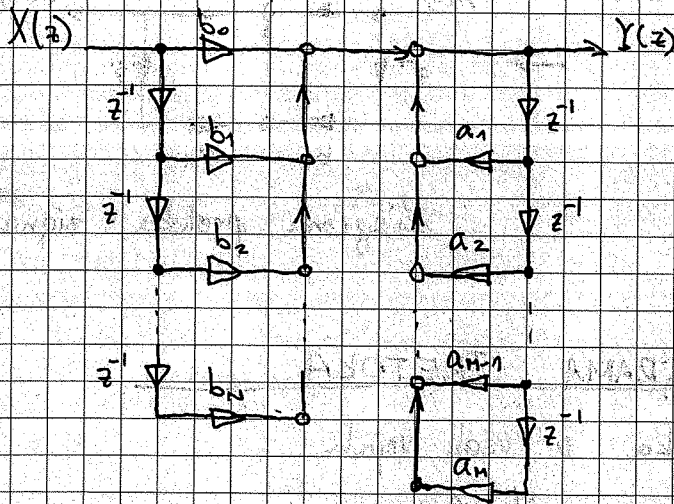


$$Y(z) = b_0 X(z) + z^{-1} (b_1 X(z) + z^{-1} b_2 X(z))$$

6.2. STRUKTURE DISKRETNIH FILTROK

6.2.1. DIREKTA STRUKTURA I in I.

$$Y(z) = \sum_{i=0}^N b_i \cdot z^{-i} X(z) + \sum_{j=1}^M a_j \cdot z^{-j} \cdot Y(z)$$

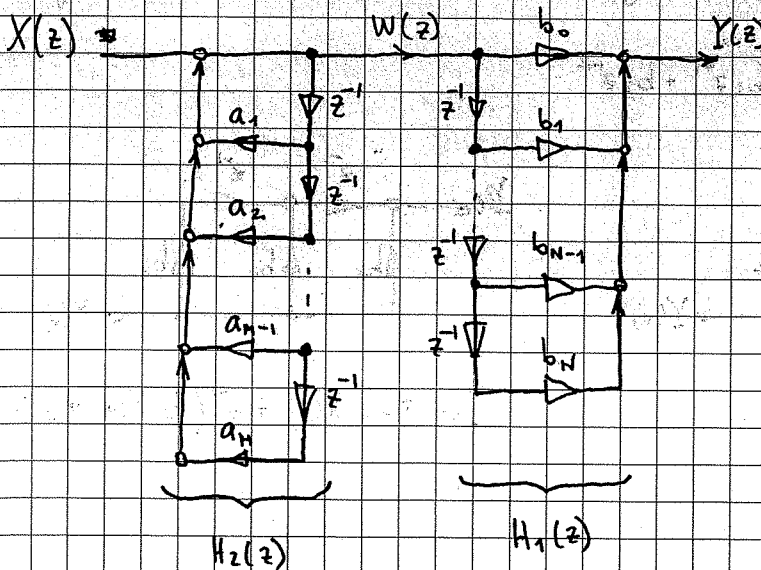


$$H(z) = \frac{N(z)}{D(z)}$$

$$H_1(z) = \sum_{i=0}^N b_i z^{-i} = N(z)$$

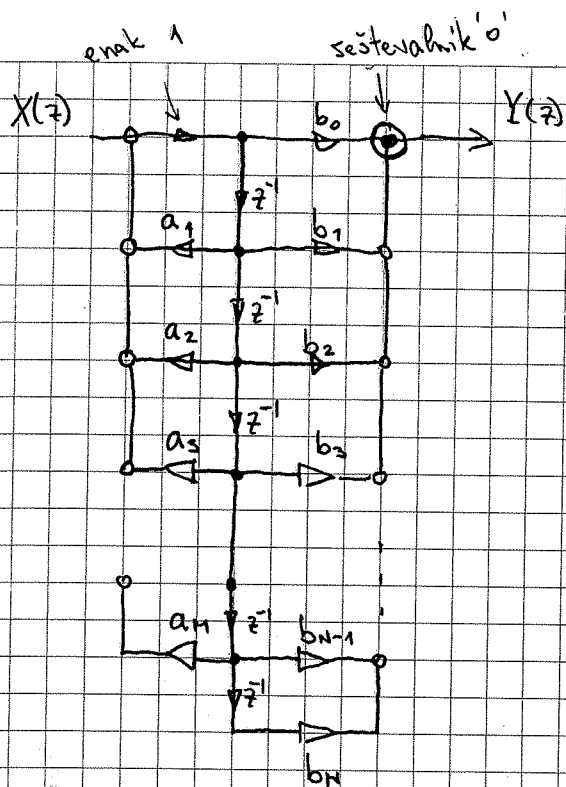
$$H_2(z) = \frac{1}{1 - \sum_{j=1}^M a_j z^{-j}}$$

$$H(z) = H_1(z) \cdot H_2(z) = H_2(z) \cdot H_1(z)$$



$$W(z) = H_2(z) \cdot X(z)$$

$$Y(z) = H_1(z) \cdot W(z)$$



direktna struktura II.
(kanonična oblika)
[porabi najmanj elementov za realizacijo]

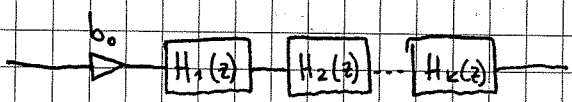
$$W[n] = x[n] + \sum_{j=1}^M a_j w[n-j]$$

$$y[n] = \sum_{j=0}^N b_j w[n-j]$$

w... spremenljivka sistema

6.2.2. KASKADNA VEZANA

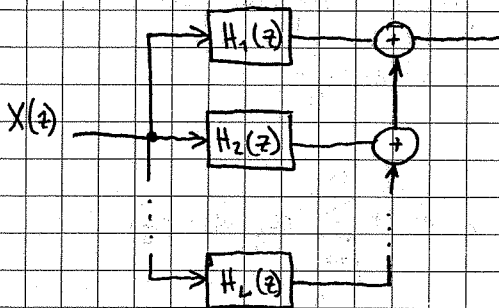
uporabljamo jo za IIR filtre
kaskado celic prvega in drugega reda



$$H(z) = b_0 \prod_{i=1}^k H_i(z)$$

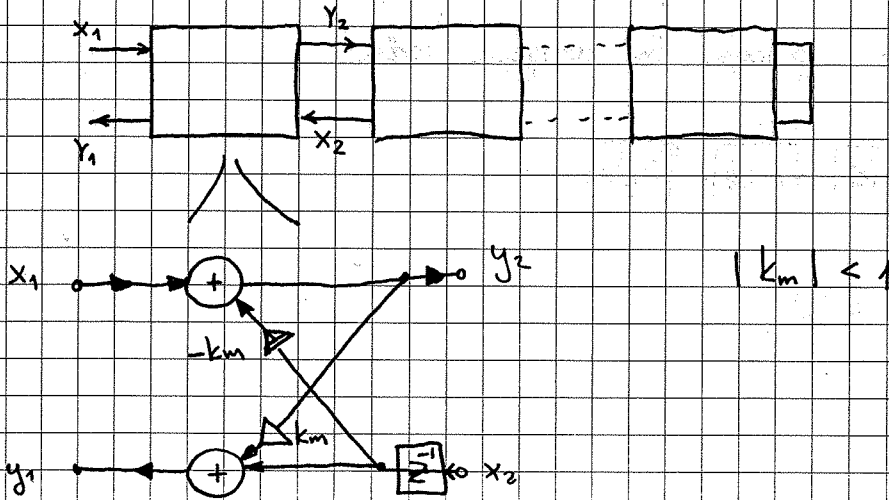
6.2.3. VZPOREDNA VEZAVA

$$H(z) = \sum_{i=1}^L \frac{b_{0i} + b_{1i} z^{-1}}{1 - a_{1i} z^{-1} + a_{2i} z^{-2}}$$

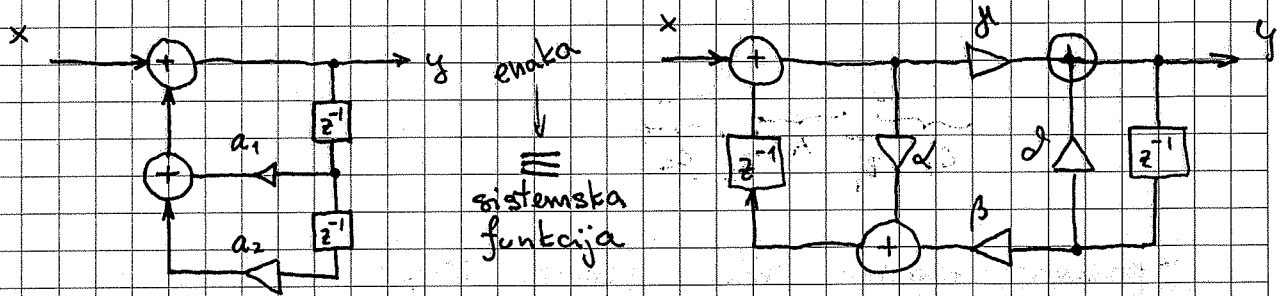


6.2.4. DRUGE STRUKTURE

Lestričasti filter - lattice filter
realizacija FIR in IIR filtrov



Sklopljena struktura 2. reda (coupled form)

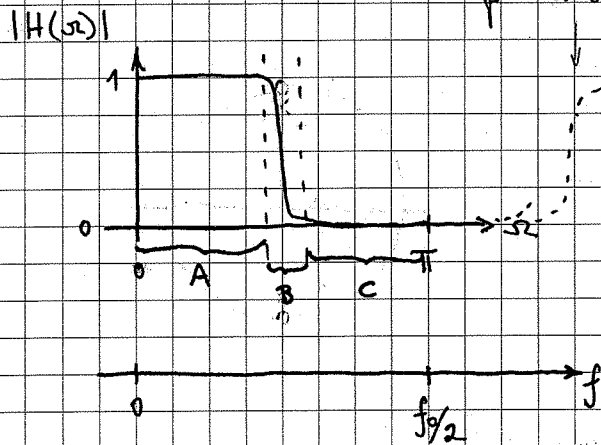


enaka
≡
sistemsko
funkcija

več možnosti
preglednejša lega polov

G.2.5. ZNAČILNIKI PREDSTAVNIKI DISKRETNIH FILTROV

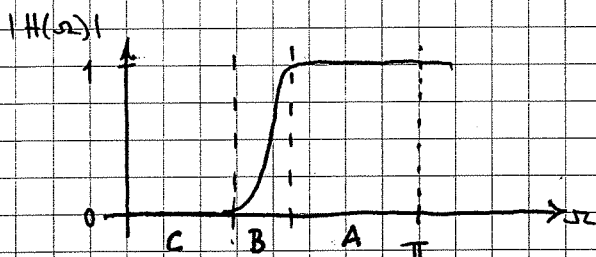
- nizko sito



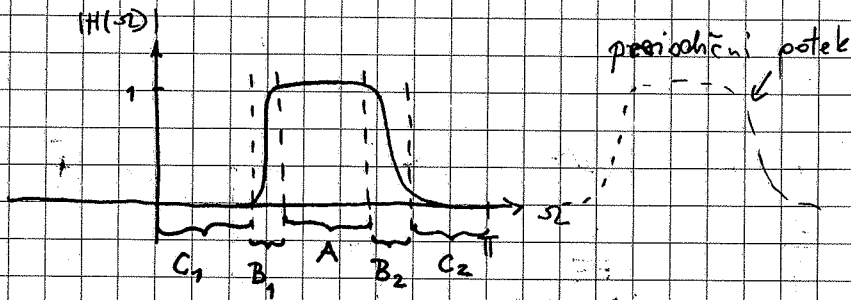
periodično ponavljanje

- A... prepustni pas
- B... prehodni pas
- C... zaporni pas

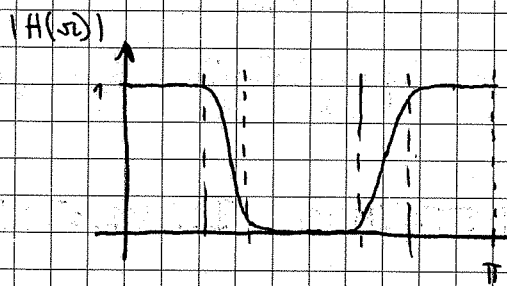
- visoko sito



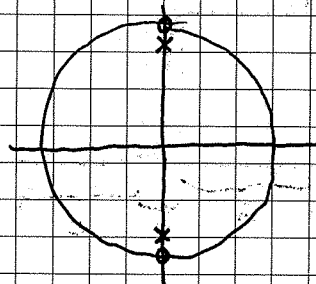
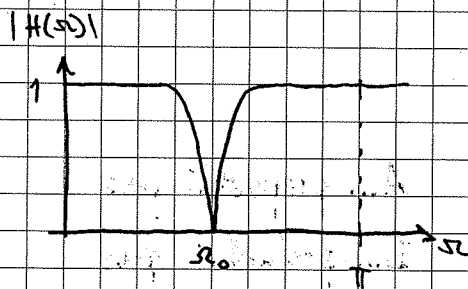
- pasovno prepustno sito (band pass)



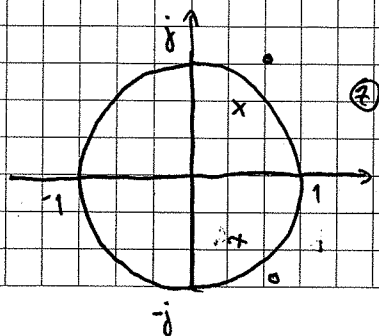
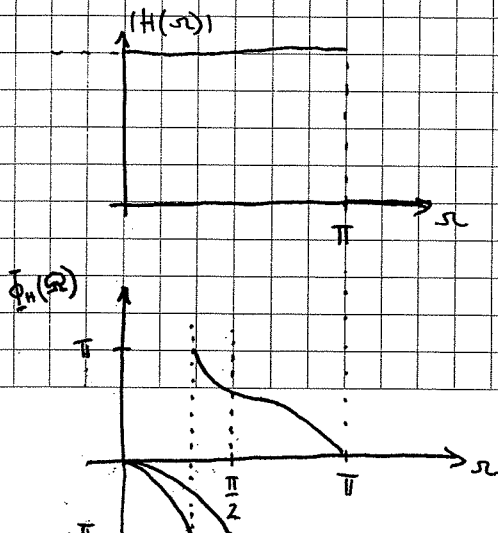
- pasovno zaporno sito (band stop)



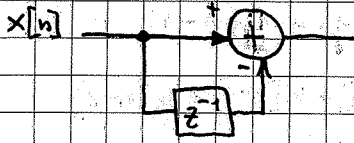
- zavlačno sito (notch filter)



- fazni sukalniik (all pass filter)

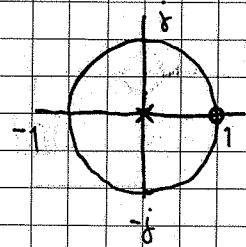


- diferenciator



$$y[n] = x[n] - x[n-1]$$

$$H(z) = 1 - z^{-1} = \frac{z-1}{z}$$

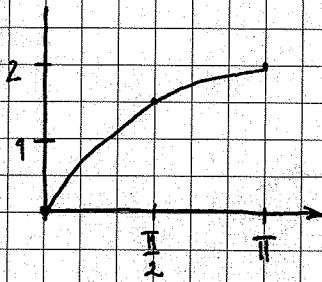


$$H(\omega) = 2j \sin \frac{\omega}{2} e^{-j\frac{\omega}{2}}$$

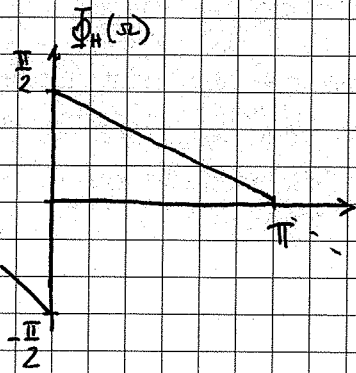
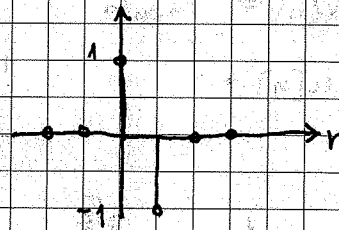
zvezni diferenciator : $y(t) = \frac{dx(t)}{dt}$

$$H(\omega) = j\omega$$

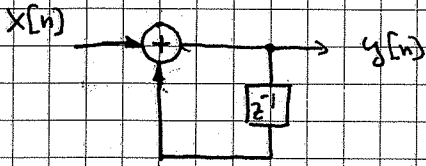
$|H(\omega)|$



$h[n]$



- diskretni sumator (akumulator)

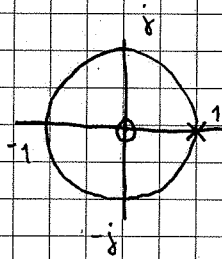


$$y[n] = x[n] + y[n-1]$$

$$= x[n] + x[n-1] + y[n-2]$$

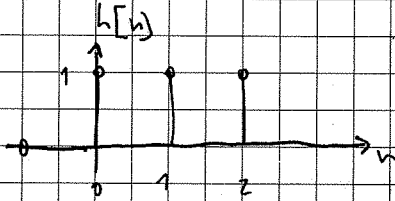
$$y[n] = \sum_{i=-\infty}^n x[i]$$

$$H(z) = \frac{z}{z-1}$$

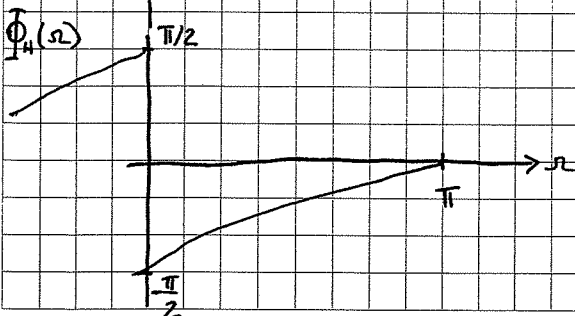
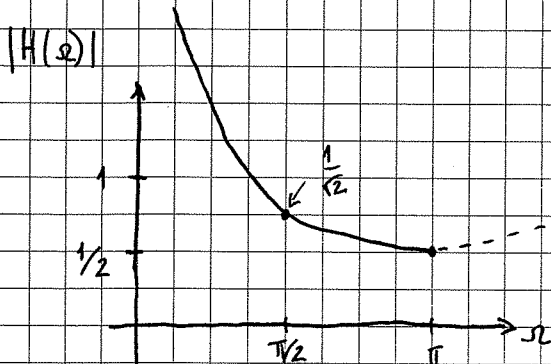


ce dajmo $x[n] = \text{impuls}$

$$h[n] = u[n]$$



$$H(\omega) = \frac{1}{2j \sin \frac{\omega}{2}} e^{j \frac{\omega}{2}}$$



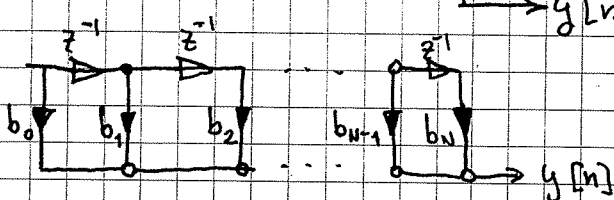
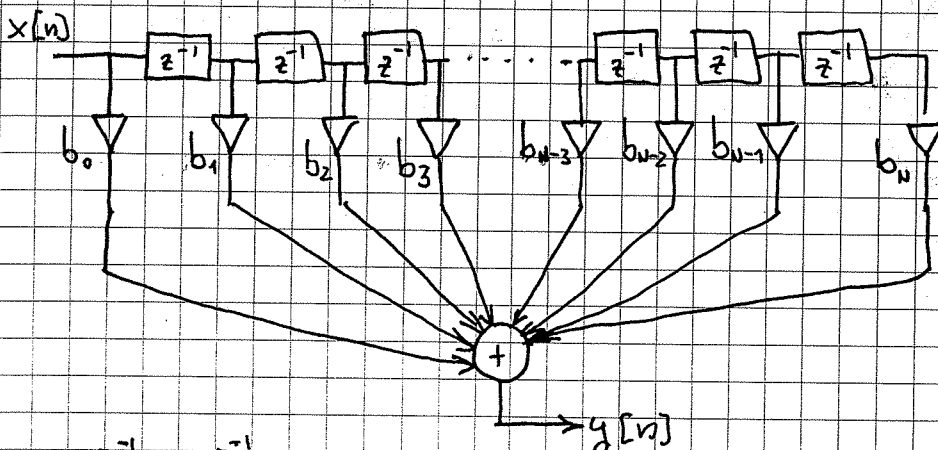
6.3. NAČRTOVANJE FIR FILTROV

6.3.1. LASTNOSTI

- imajo končen odziv, so vedno stabilni
- dolžina odziva je enaka številu koeficientov, ki je $N+1$: b_0, b_1, \dots, b_N
- poli ležijo v izhodišču z ravnine, in ne vplivajo na potek frekvenčnega odziva, frekvenčni potek je določen z ničlami
- imajo lahko linearno fazo
- primerni za adaptivne izvedbe
 - ↳ zadeva se prilagaja na signal

6.3.2. STRUKTURE

a) transferzalni filter (kanonična oblika)



$$H(z) = \sum_{i=0}^N b_i z^{-i} = \frac{\sum_{i=0}^N b_i z^{N-i}}{z^N}$$

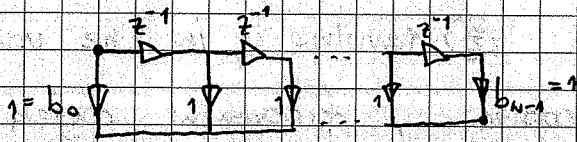
Alta $h[n] = \sum_{i=0}^N b_i \cdot \delta[n-i]$

b) rekurzivna izvedba.

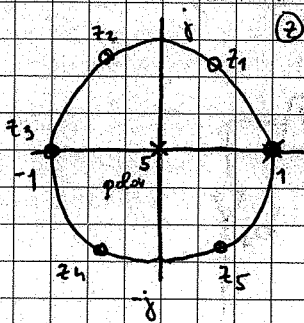
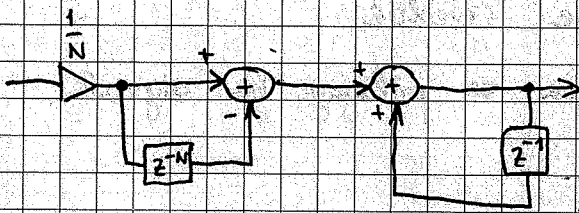
filter za tekoče povprečje (moving average filter)

$$H(z) = \frac{1}{N} \sum_{l=0}^{N-1} z^{-l} = \frac{1}{N} (1 + z^{-1} + z^{-2} + \dots + z^{-(N-1)}) =$$

$$= \frac{1}{N} \frac{1 - z^{-N}}{1 - z^{-1}} = \frac{1}{N} \frac{z^N - 1}{z^{N-1}(z-1)}$$



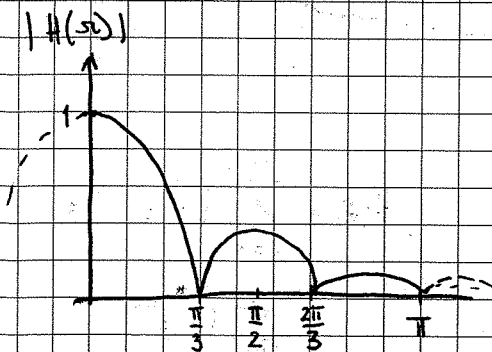
$$H(z) = \frac{1}{N} (1 - z^{-N}) \cdot \frac{1}{1 - z^{-1}}$$



$$z^N = 1 = e^{j2k\pi}$$

$$z_k = e^{j\frac{2k\pi}{N}} \quad ; k=1, \dots, N$$

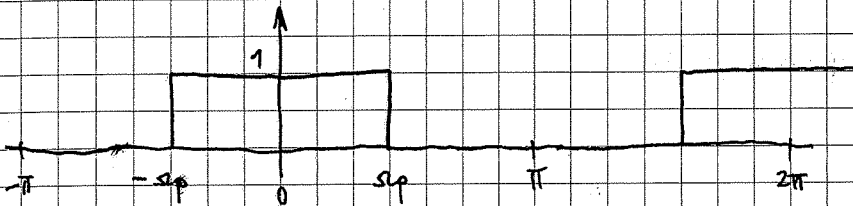
$$N=6$$



6.3.3 NACRTOVANJE FIR FILTROV Z OKNENJEM

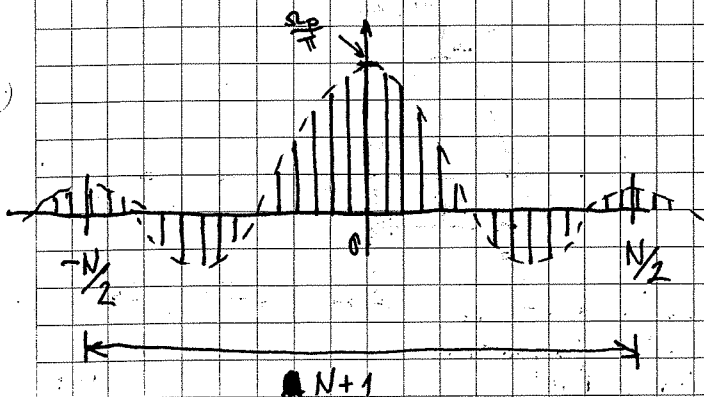
Idealno nizko sito :

$$H(\omega) = \begin{cases} 1 & \text{za } |\omega| < \omega_p \\ 0 & \text{drugod} \end{cases} \quad \begin{array}{l} \text{za osnovno periodo} \\ -\pi < \omega < \pi \end{array}$$



$$h[n] = \frac{1}{2\pi} \int_{-\pi}^{\pi} H(\omega) \cdot e^{j\omega n} d\omega = \frac{1}{2\pi} \int_{-\omega_p}^{\omega_p} e^{j\omega n} d\omega = \frac{\sin(\omega_p \cdot n)}{\pi \cdot n}$$

$$h[0] = \lim_{n \rightarrow 0} \frac{\sin(\omega_p \cdot n)}{\pi \cdot n} = \frac{\omega_p}{\pi}$$



$$h[n] = \begin{cases} \frac{\sin(\omega_p (n - \frac{N}{2}))}{\pi (n - \frac{N}{2})} & \text{za } 0 \leq n \leq N \\ 0 & \text{drugod} \end{cases}$$

impulzni odziv ni
periodičen ;
frekvenčni je periodičen

13. 5. 2013

Rezultate predstavimo z množenjem s pravokotnim oknom.

$$w[n] = \begin{cases} 1 & \text{za } |n| \leq \frac{N}{2} \\ 0 & \text{drugače} \end{cases}$$

$$h[n] = h_i[n] \cdot w[n] \leftarrow \text{okenska funkcija}$$

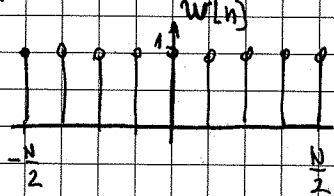
↑
idealni impulzni odziv

↑
TDFT
↓

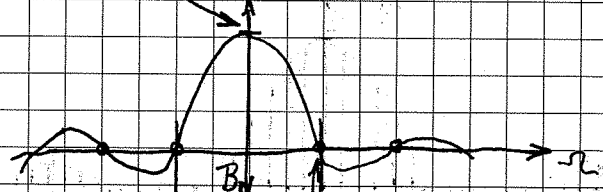
$$H(\Omega) = \frac{1}{2\pi} H_i(\Omega) * W(\Omega) = \frac{1}{2\pi} \int_{-\frac{\pi}{2}}^{\frac{\pi}{2}} H_i(\Omega - \lambda) \cdot W(\lambda) d\lambda$$

$$W(\Omega) = \sum_{n=-\frac{N}{2}}^{\frac{N}{2}} e^{-j\Omega n} = \frac{\sin\left(\frac{N+1}{2}\Omega\right)}{\sin\left(\frac{\Omega}{2}\right)}$$

pravokotno okno



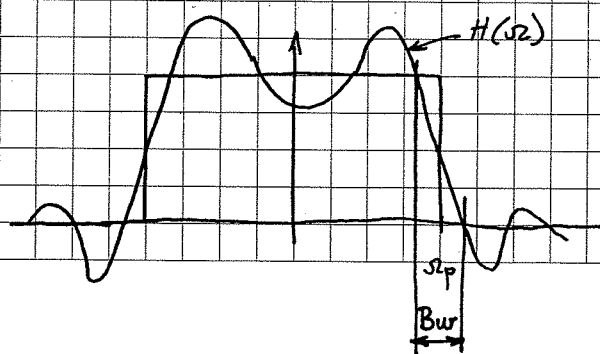
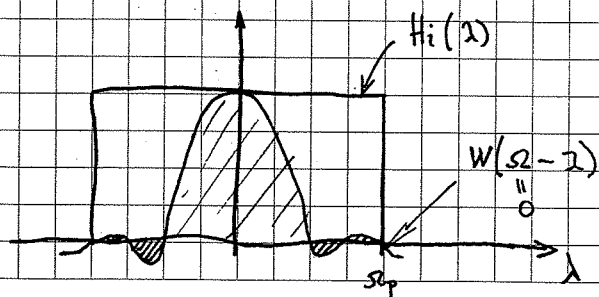
$N+1$ $W(\Omega)$



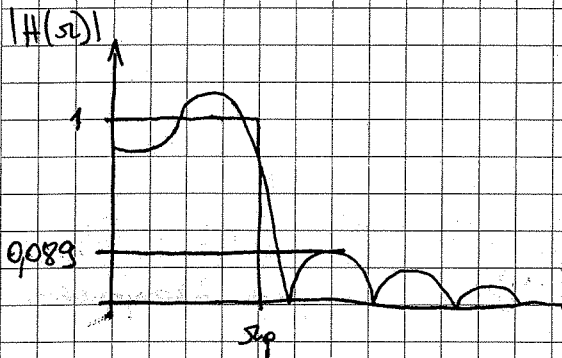
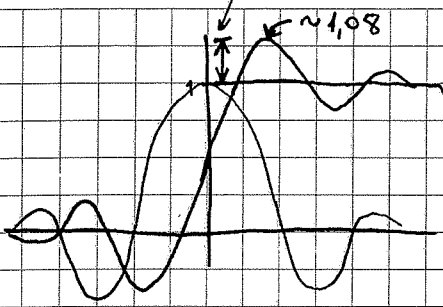
razdalja med tema ničloma je pasovna širina B_N

ničla: $\pi = \frac{N+1}{2}\Omega \Rightarrow \Omega = \frac{2\pi}{N+1}$

$$B_{BW} = \frac{4\pi}{N+1}$$



prezpon (Gibbsov fenomen)



dušenje : $20 \log(0,089) = -20,96$
 $\approx -21 \text{ dB}$

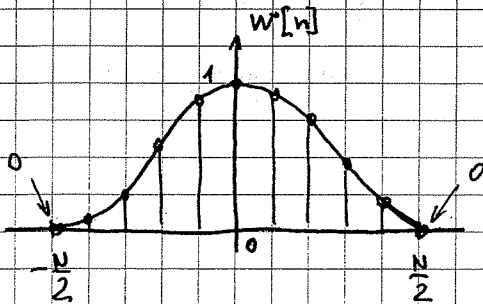
Zaradi tega raje namesto trdih oken uporabimo mehka okna

KOSINUSNA OKNA

$$w[n] = \begin{cases} a_0 + a_1 \cdot \cos\left(\frac{2\pi}{N} \cdot n\right) & \text{za } |n| \leq \frac{N}{2} \\ 0 & \text{za } |n| > \frac{N}{2} \end{cases}$$

von Hannovo okno :

$a_0 = a_1 = 0,5$



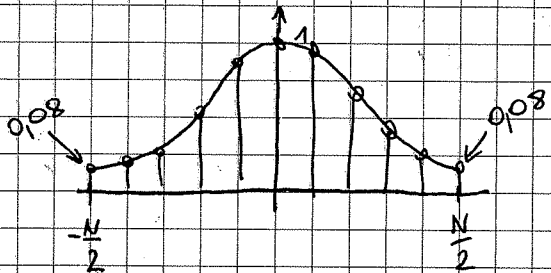
$B_{wr} = \frac{8\pi}{N}$

dušenje stranskega stopa 43,9 dB

Hammingovo okno:

$$a_0 = 0,54$$

$$a_1 = 0,46$$



$$B_w = \frac{8\pi}{N}$$

dušenje 54,4 dB

Blackmanovo okno:

$$0,42 + 0,5 \cos\left(\frac{2\pi}{N} \cdot n\right) + 0,08 \cos\left(\frac{4\pi}{N} \cdot n\right)$$

... ima 3 komponente

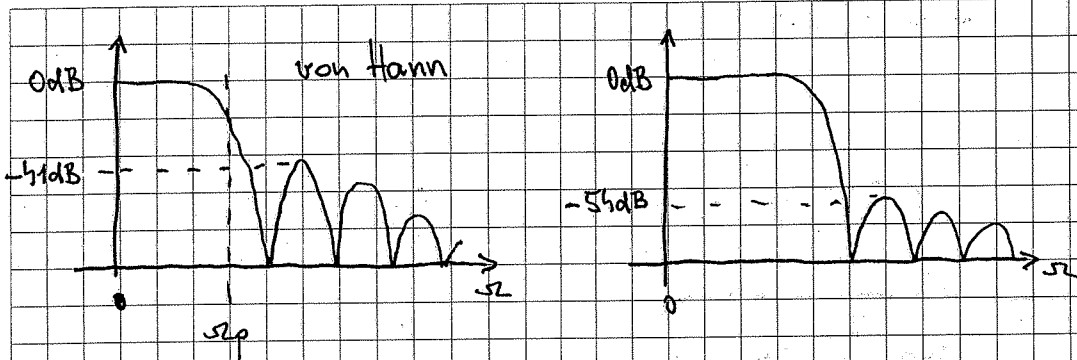
$$B_w = \frac{5,56\pi}{N}$$

dušenje 75,3 dB

Kaiserjevo, Gaussovo, Čebiševovo, ...

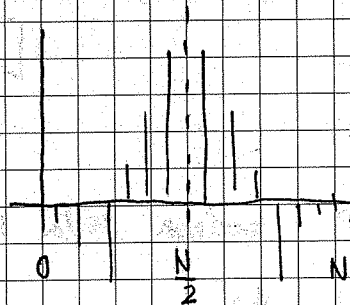
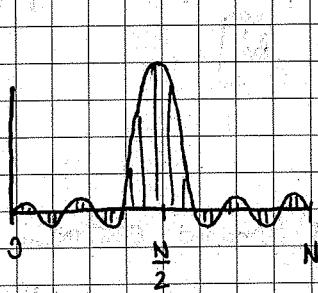
Bistveni pravili pri načrtovanju z okenstevimi funkcijami

- 1) Izbiha okna vpliva na minimalno slabljenje v zaporu, večje slabljenje razširi prehodno področje.
- 2) Dolžina okna oža centralni snop $W(f)$, z dolžino lahko vplivamo na širino prehodnega področja.



Zaradi simetrije odziva imajo ti filtri LINEARNO FAZO!

(Tip 1)



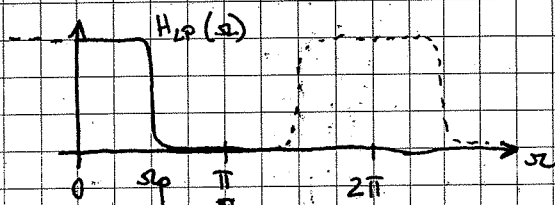
(Tip 2)

tudi ima lin. fazo

6.3.4. FREKVENČNE TRANSFORMACIJE FIR SIT

LP prototip prestavimo po frekvenci za doseganje drugih vrst filtrov

a.) HP - visoko sito

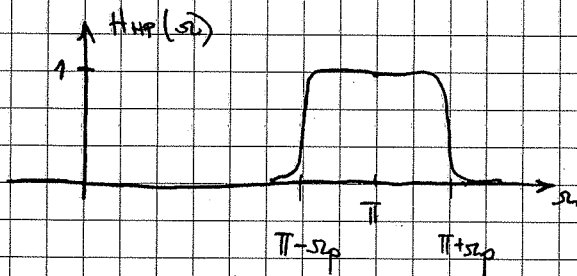


$$h_{HP}[n] = b_n$$

Množenje z $e^{j\pi n}$ premakne spekter za $\pm \pi$ (TDFT)

$$e^{j\pi n} = (e^{j\pi})^n = (-1)^n \dots \text{izmenični signal}$$

$$h[n] e^{j\pi n} \leftrightarrow H(\omega - \pi)$$

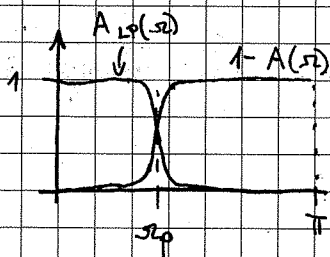
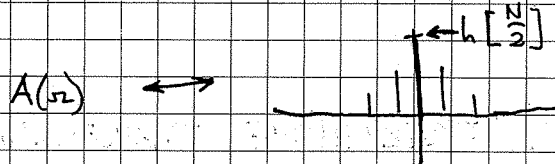


$$h_{HP}[n] = (-1)^n \cdot h_{LP}[n] = (-1)^n \cdot b_m$$

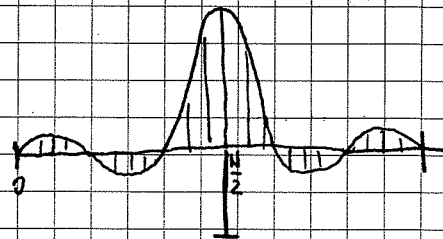
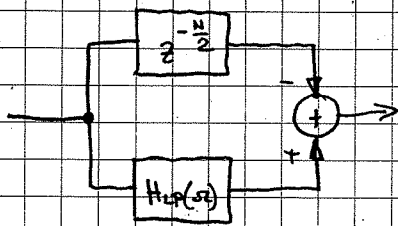
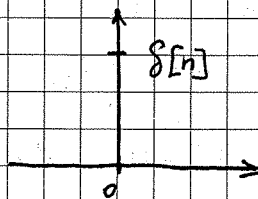
Transformacija deluje za lih in sod tip (Tip1 in Tip2).
[lih in sodi N]

Za FIR LP sodlega reda N (N = sod) (imamo centralni koef.)

$$H_{LP} = A(\omega) e^{-j\frac{N}{2}\omega}$$



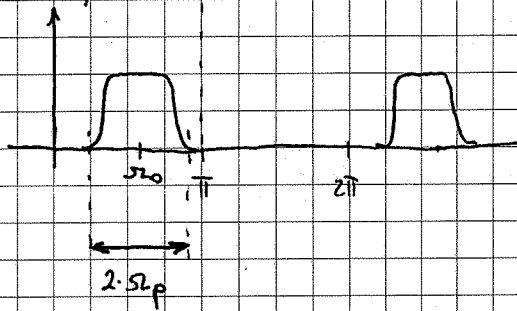
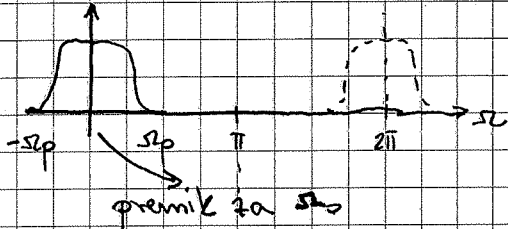
1 ↔



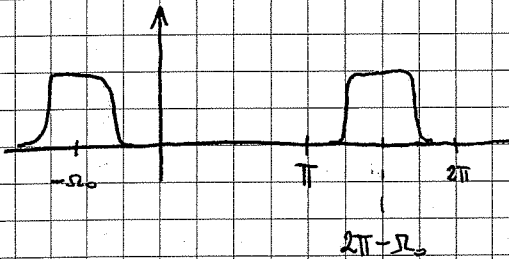
$$H_{HP}(\omega) \leftrightarrow h_{HP}[n] = h_{LP}[n] - \delta\left[\frac{N}{2}\right]$$

$$h_{LP}\left[\frac{N}{2}\right] = b_m - 1$$

b) BP - pasamo sito



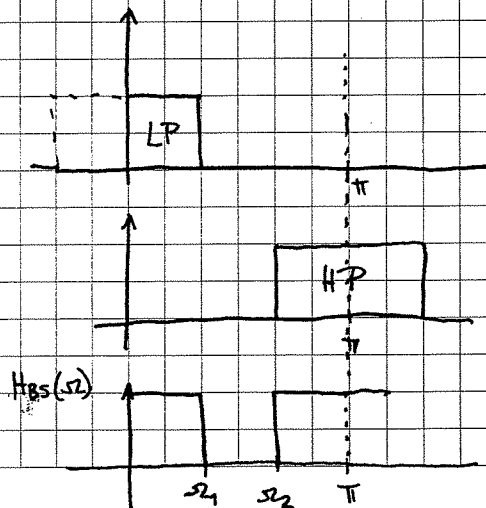
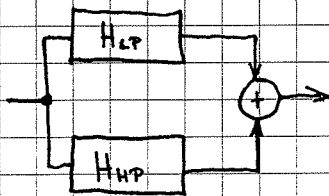
$$h[n] e^{j\omega_0 n}$$



$$h[n] e^{-j\omega_0 n}$$

$$h_{BP}[n] = h[n] (e^{j\omega_0 n} + e^{-j\omega_0 n}) = h[n] \cdot 2 \cos(\omega_0 n)$$

c) BS - pasamo zaposno sito

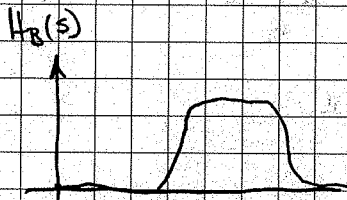
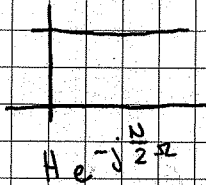
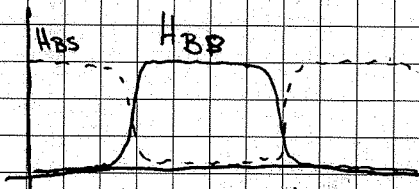


$$H(z) = H_L(z) + H_H(z) = \sum_{i=0}^N b_{LPi} z^{-i} + \sum_{i=0}^N b_{HPi} z^{-i}$$

$$H_{BS}(z) = \sum_{i=0}^N (b_{LPi} + b_{HPi}) z^{-i}$$

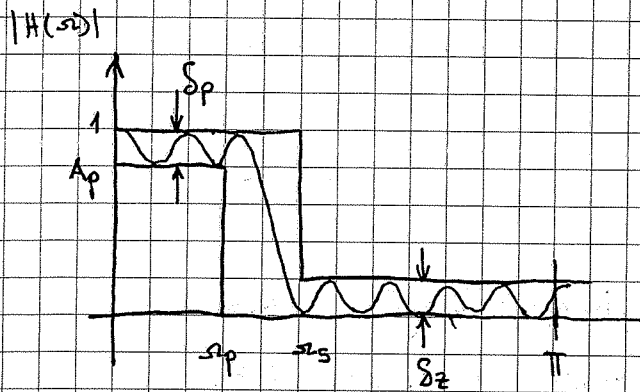
Pogoj je da morata biti filtra istega reda (tip-a)

Za sodi red N lahko uporabimo odštevanje



$$H_{BS} = e^{-j \frac{N}{2} \omega} \cdot A_{BP}(\omega)$$

6.3.5. NACRTOVANJE FIR SIT Z ENAKOMERNO VALOVITOSTJO



Parks in McClellan postopek

potrebujemo: N, δ_p, δ_s , razmerje $\frac{\delta_p}{\delta_s}$

$$A_p [\text{dB}] : \delta_p = 1 - 10^{\frac{A_p}{20}}$$

$$A_s [\text{dB}] : \delta_s = 10^{\frac{A_s}{20}}$$

6.4. NAČRTOVANJE IIR FILTROV

6.4.1. LASTNOSTI

- imajo rekurzivno strukturo
- so potencialno nestabilni
- odziv je neskončen vendar imajo krajše zakasnitve
- nižji red za doseganje zahtevane karakteristike
- večja občutljivost na kvantizacijo koeficientov
- ne moremo doseči linearne faze
- lahko napravimo fazni sukalmik

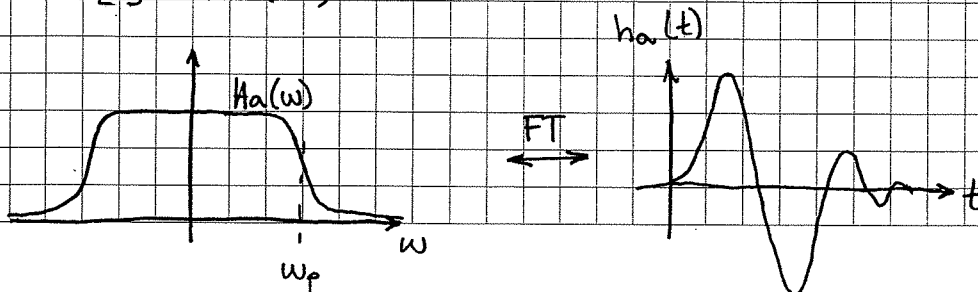
6.4.2. STRUKTURE

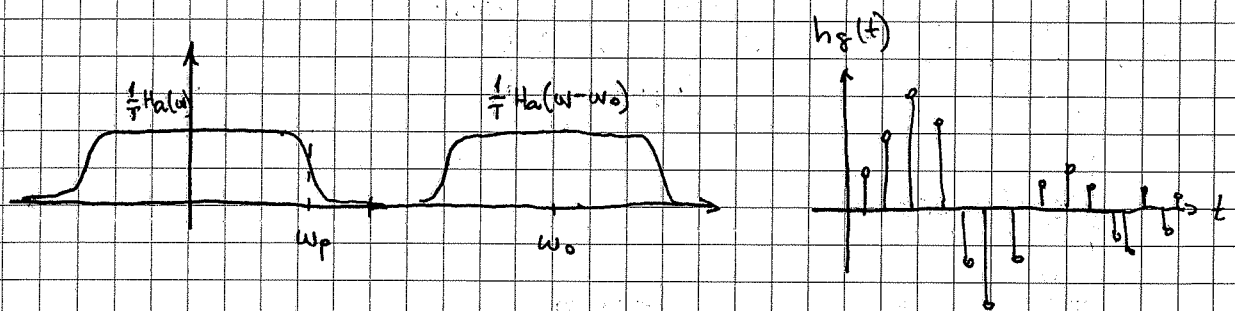
- direktna struktura I. in II.
- kaskadna vezava filtrov 2. reda (tudi 1. red)
2. red - par kompleksnih polov in ničel \rightarrow kontrola stabilnosti
- lestričasta (rešetkasta) struktura
- paralelna struktura (uporablja se zelo redko)

6.4.3. IMPULZNO INVARIANTNA METODA

$h_a(t)$... impulzni odziv analognega prototipa

$$h_w[n] = h_a(nT)$$





$$H(s) = \frac{1}{T} \sum_{k=-\infty}^{\infty} H_a(s - k \cdot \omega_0) = \frac{1}{T} \sum_{k=-\infty}^{\infty} H_a\left(\frac{s - k \cdot 2\pi}{T}\right)$$

Metoda je uporabna za nizka nita, ki imajo 0 polov.

To so Butterworthov in Čebišev I.

(ne sme imeti valovitosti v zapori)

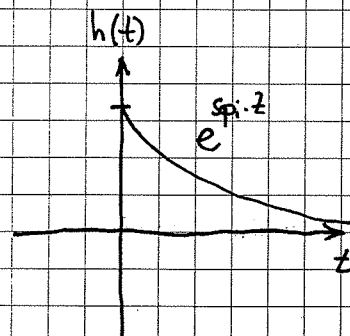
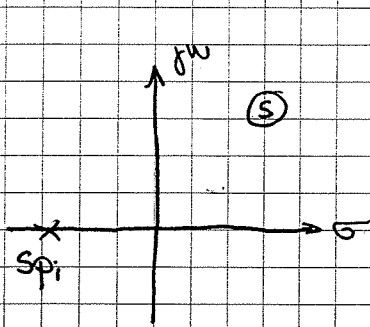
$$H(z) = \sum_{n=0}^{\infty} h_a(nT) z^{-n}$$

ponavadi nimamo, ponavadi imamo $H_a(s)$

$$H_a(s) = \sum_{i=1}^N \frac{C_i}{s - s_{pi}} = b_0 \prod_{i=1}^N \frac{1}{(s - s_{pi})} \quad \dots \text{ničel ni, so samo pol}$$

$$C_i = \operatorname{Res}_{s=s_{pi}} H_a(s)$$

$$h_a(t) = u(t) \sum_{i=1}^N C_i \cdot e^{s_{pi} \cdot t}$$



$$h[n] = h_a(nT) = u[n] \sum_{i=1}^N C_i e^{s_{pi} \cdot T \cdot n}$$

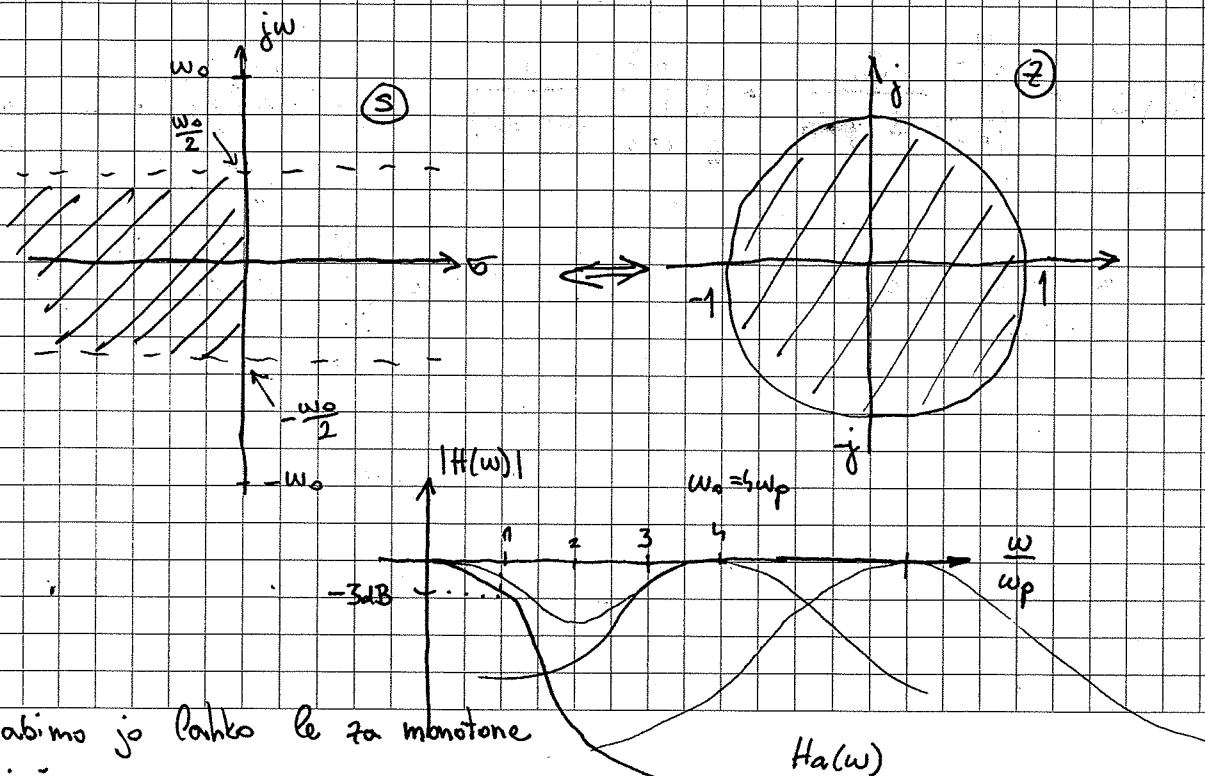
↓ z-transform

$$H(z) = \sum_{i=1}^N C_i \cdot \mathcal{Z} \left\{ u[n] \cdot e^{s_{pi} \cdot T \cdot n} \right\}$$

$$u[n] \cdot e^{s_{pi} \cdot T \cdot n} \xleftrightarrow{z} \frac{1}{1 - e^{s_{pi} T} z^{-1}}$$

$$H(z) = \sum_{i=1}^N \frac{C_i}{1 - (e^{s_{pi} T} z^{-1})}$$

$$z_{pi} = e^{s_{pi} T} \leftarrow T \dots \text{frekvencia vzoröenja}$$



Uporabimo jo lahko le za monotone padajoöe.

lahko samo pada - ne sme naraščati

6.4.4. BILINEARNA TRANSFORMACIJA

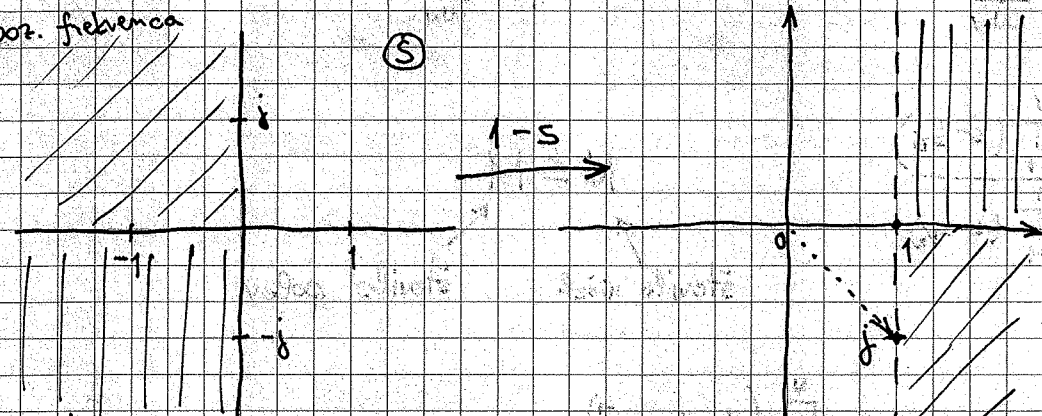
$z = \frac{1+s}{1-s}$ veliki S , predstavlja normirano frekvenco

S je normiran $\frac{\omega}{\omega_n}$

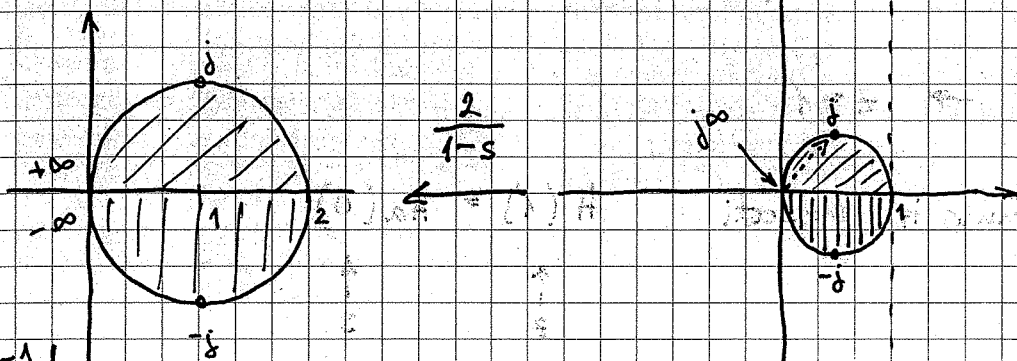
$z = 2 \frac{1}{1-s} - 1$

poz. frekvenca

⑤

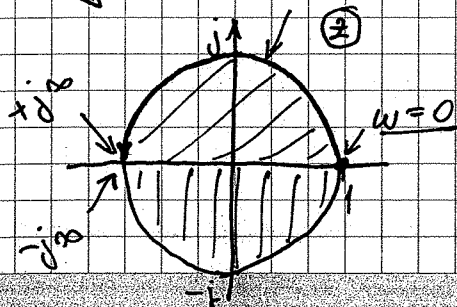


negativna frekvenca



imaginarna os ⑤ ravni

$\frac{z}{1-s} - 1$



$$s = \frac{z-1}{z+1} = \frac{s}{\omega_N}$$

$$s = \omega_N \frac{z-1}{z+1}$$

$$H(z) = H_a\left(\omega_N \frac{z-1}{z+1}\right)$$

$H_a \dots H_{\text{analogna}}$

raje neposredno določimo pole in ničle

$$z_{pi} = \frac{1 + \frac{s_{pi}}{\omega_N}}{1 - \frac{s_{pi}}{\omega_N}}$$

$$z_{zi} = \frac{1 + \frac{s_{zi}}{\omega_N}}{1 - \frac{s_{zi}}{\omega_N}}$$

$$H_a(s) = b_0 \frac{\prod_{i=1}^N (s - s_{zi})}{\prod_{j=1}^M (s - s_{pj})}$$

$$N \leq M$$

↑
število ničel

↑
število polov

$$H(z) = b_0 (1+z^{-1})^{M-N} \frac{\prod_{i=1}^N (1 - z_{zi} z^{-1})}{\prod_{j=1}^M (1 - z_{pj} z^{-1})}$$

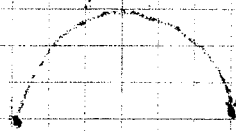
$$s = 0 \rightarrow z = 1$$

b_0 določimo iz enakosti

$$H(1) = H_a(0)$$

↑
 z

↑
 s



Stiskanje frekvenc

$$\omega \in (0, \infty) \rightarrow \Omega \in (0, \pi)$$

$$s = \omega_N \cdot \frac{z-1}{z+1}$$

$$s = j\omega$$

$$z = e^{j\Omega}$$

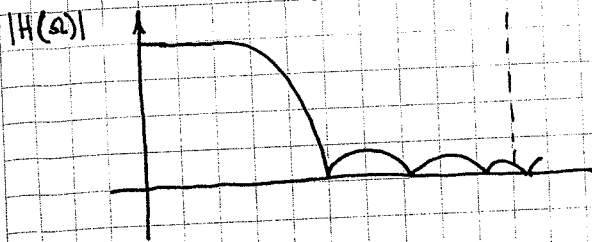
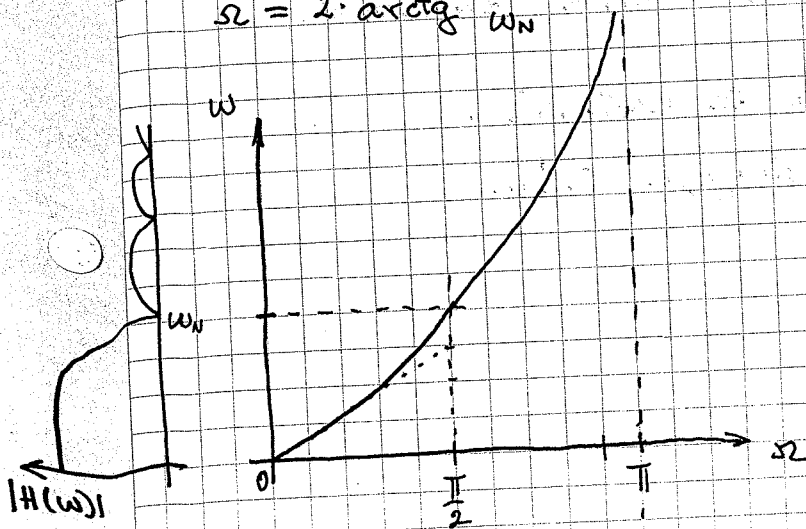
$$j\omega = \omega_N \frac{e^{j\frac{\Omega}{2}} - 1}{e^{j\frac{\Omega}{2}} + 1} = \omega_N \frac{e^{j\frac{\Omega}{2}} - e^{-j\frac{\Omega}{2}}}{e^{j\frac{\Omega}{2}} + e^{-j\frac{\Omega}{2}}}$$

~~$$\frac{e^{j\frac{\Omega}{2}}}{e^{j\frac{\Omega}{2}}}$$~~

~~$$j\omega = j \cdot \omega_N \frac{\sin \frac{\Omega}{2}}{\cos \frac{\Omega}{2}}$$~~

$$\omega = \omega_N \cdot \tan \frac{\Omega}{2}$$

$$\Omega = 2 \cdot \arctan \frac{\omega}{\omega_N}$$



Postopek:

1. Na osnovi $\Omega_p, \Omega_s, A_p, A_s$ določimo analogne ω_p, ω_s .

$$\omega_p = \omega_N \cdot \operatorname{tg}\left(\frac{\Omega_p}{2}\right)$$

$$\omega_s = \omega_N \cdot \operatorname{tg}\left(\frac{\Omega_s}{2}\right)$$

2. Na osnovi ω_p, ω_s in A_p, A_s določimo vrsto in red analognega filtra.

3. Z bilinearno preslikavo določimo pole in ničle v z -ravnini.

$$z_p = \frac{1 + \frac{s_{pi}}{\omega_N}}{1 - \frac{s_{pi}}{\omega_N}}$$

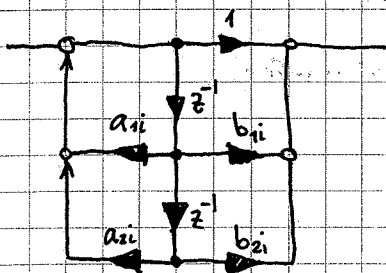
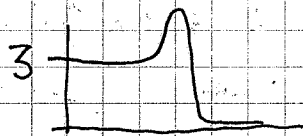
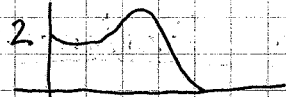
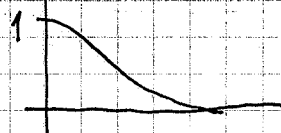
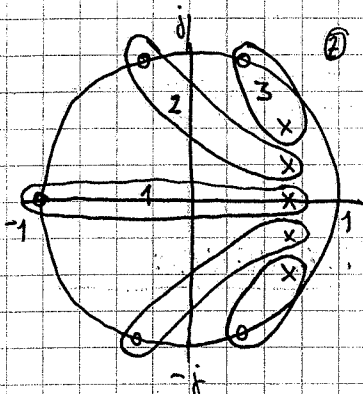
4. Zapišemo $H(z)$.

5. Izračunamo b_0 , da ustreza danim zahtevam.

6. Izberemo ustrezno strukturo za realizacijo.
Običajno kaskada celic drugega reda.

Primer:

//// ... upamitev



$$H_i(z) = \frac{1 + b_{1i} z^{-1} + b_{2i} z^{-2}}{1 - a_{1i} z^{-1} - a_{2i} z^{-2}}$$

z_i, z_i^* in p_i, p_i^* ... konjugirani kompleksni par

$$z_i = |z_i| e^{j\Omega z_i}$$

$$z_i^* = |z_i| e^{-j\Omega z_i}$$

$$p_i = |p_i| e^{j\Omega p_i}$$

$$p_i^* = |p_i| e^{-j\Omega p_i}$$

$$(1 - z_i \cdot z^{-1})(1 - z_i^* \cdot z^{-1}) = 1 - 2 \cdot |z_i| \cdot \cos \Omega z_i \cdot z^{-1} + |z_i|^2 \cdot z^{-2}$$

$$b_{1i} = -2 \cdot |z_i| \cdot \cos \Omega z_i$$

$$a_{1i} = +2 |p_i| \cos \Omega p_i$$

$$b_{2i} = + |z_i|^2$$

$$a_{2i} = - |p_i|^2$$

po absolutni vrednosti vedno < 1

7. SISTEMI Z RAZLIČNIMI VZORČEVALNIMI FREKVENCAMI

(multirate systems)

7.1. RAZLOGI ZA SPREMEMBO VZORČEVALNE FREKVENCE

- prilagajanje med sistemi z različnimi f_s

telefonski govor : 8 kHz (300 + 3400 Hz)

audio signali : 32 kHz - za radio

44,1 kHz - CD (zgoščanka)

48 kHz - DAT (tape-kaseta)

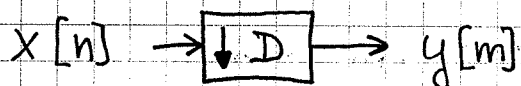
- povečanje učinkovitosti obdelave

(prilagajanje pasovni širini signala)

- zmanjšanje zahtevnosti sit proti prekrivanju pri rekonstrukciji in zajemanju

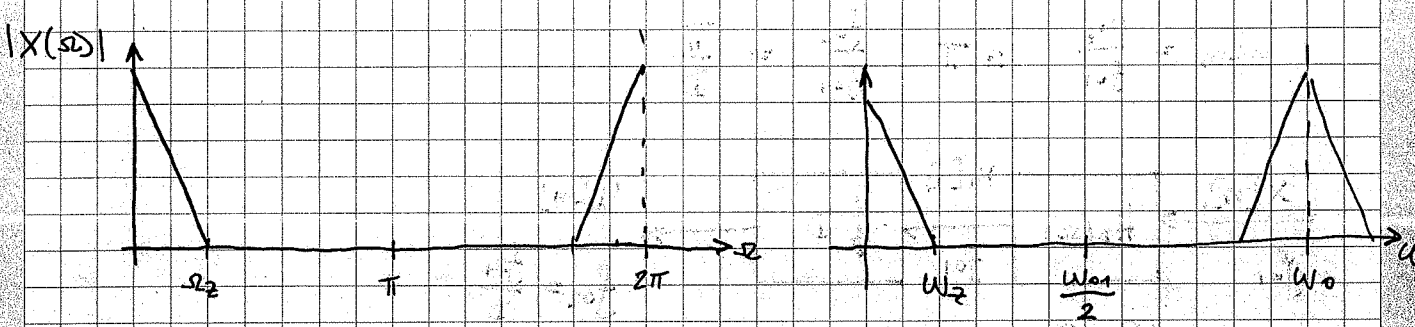
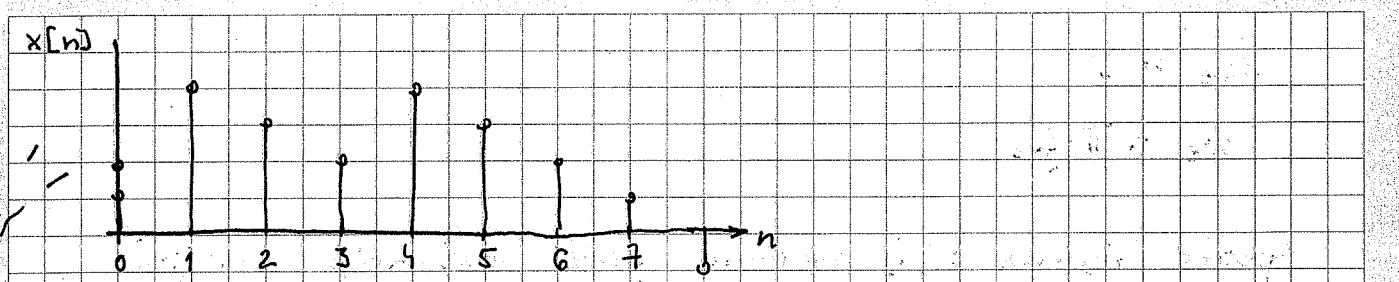
7.2. DECIMACIJA

na D vzorcev spustimo $D-1$ originalnih

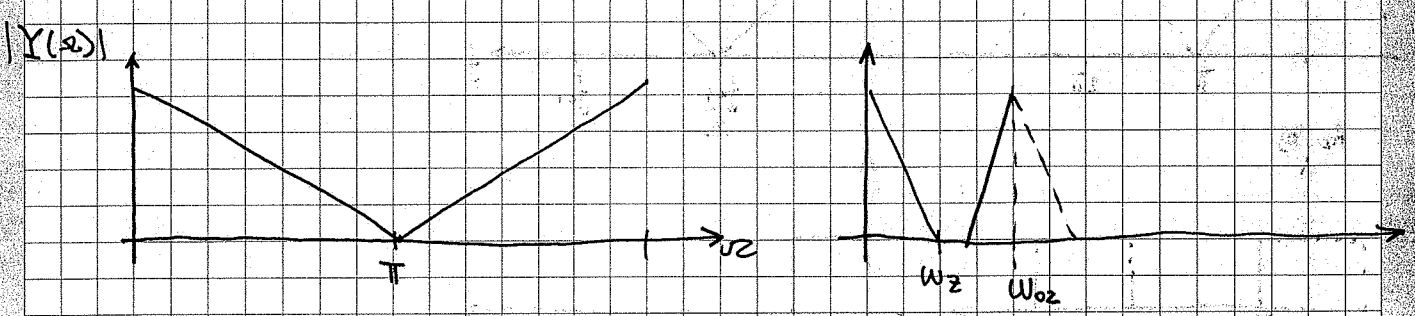
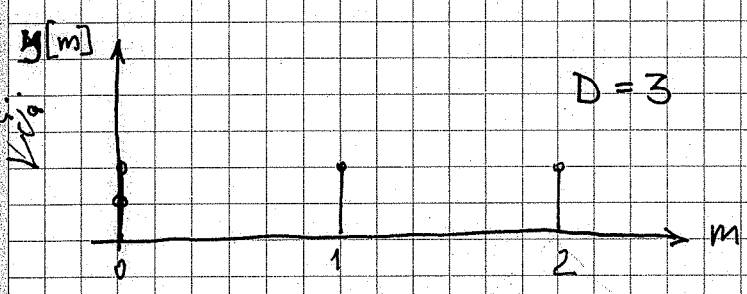


$$f_{s2} = f_{s1} \cdot \frac{1}{D} \geq 2 \cdot f_z$$

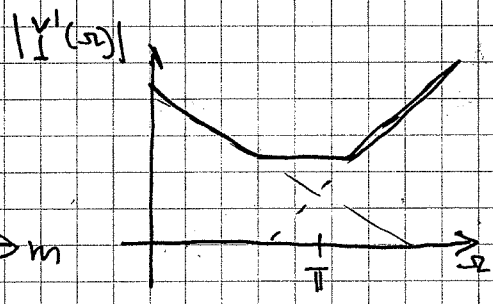
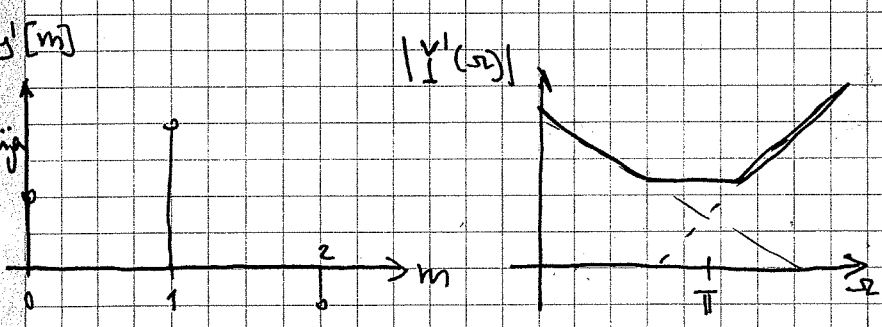
f_z ... mejna frekvenca analognega signala



decimacija



decimacija
D=4



$$\omega_{02} = \frac{\omega_{01}}{3}$$

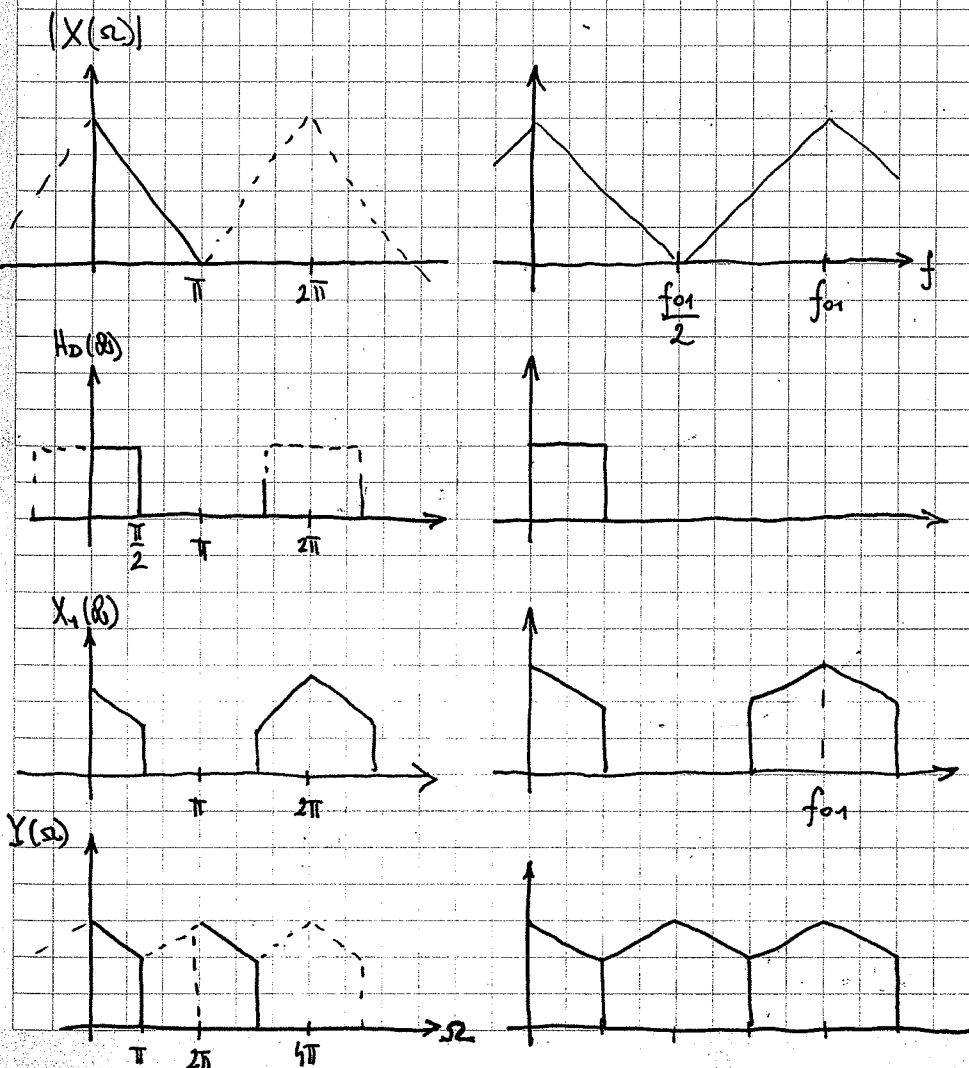
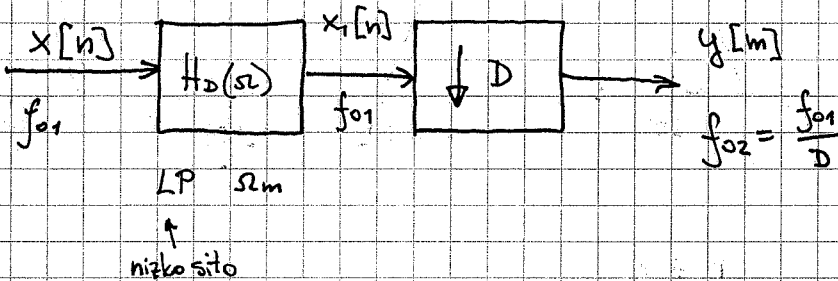
$$\omega_{02}' = \frac{\omega_{01}}{4}$$

$$\Omega_z \leq \pi$$

$$\omega_z < \pi \cdot f_{o2}$$

spekter signala $x[n]$ moramo pred decimacijo omejiti

$$\Omega_m = \frac{\omega_z}{f_{o1}} \leq \pi \cdot \frac{f_{o2}}{f_{o1}} = \frac{\pi}{D}$$

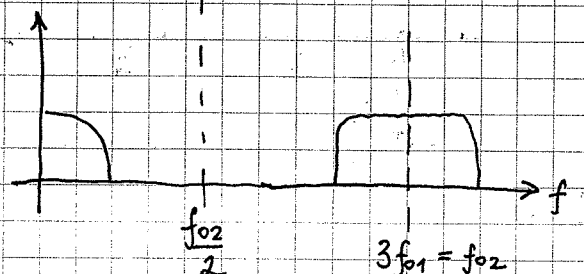
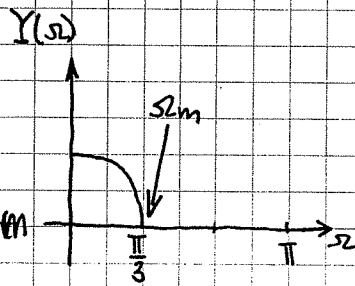
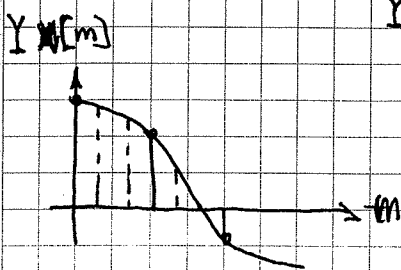
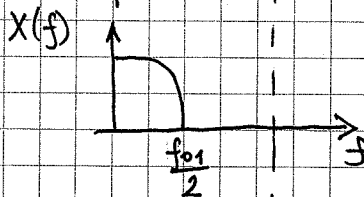
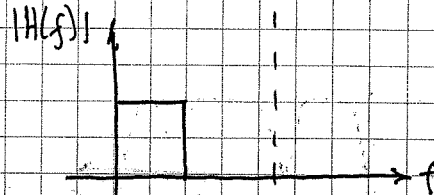
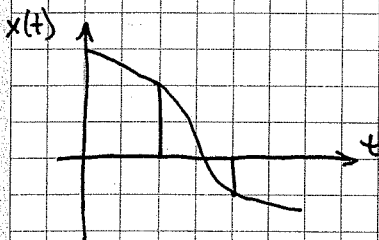
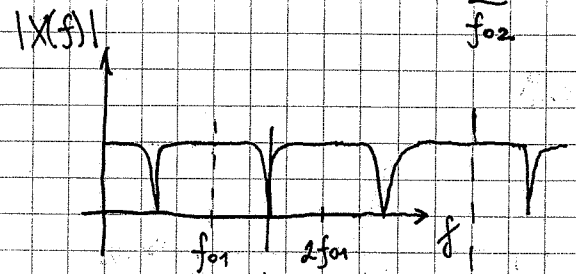
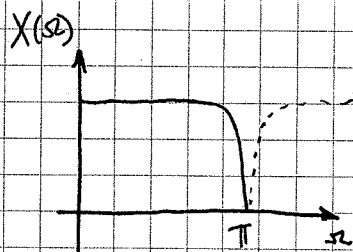
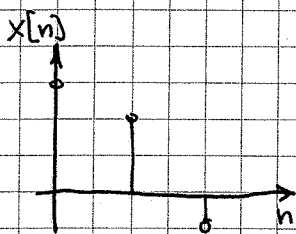
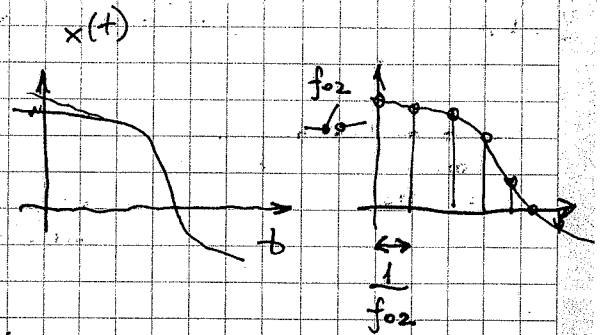
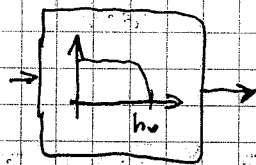
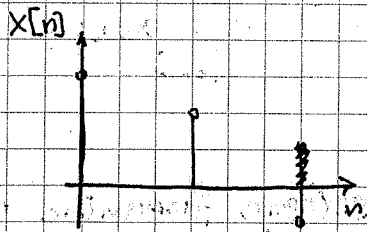


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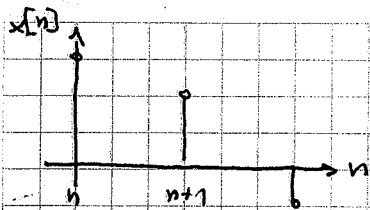
7.3. INTERPOLACIJA

med vzorce klamo I-1 novih vzorcev

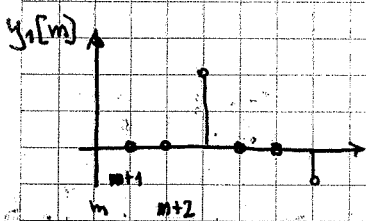
$$I = \frac{f_{02}}{f_{01}}$$



$$\Omega_m = \frac{\omega_2}{f_{02}} = \frac{2\pi \cdot f_{01}}{f_{02} \cdot 2} = \pi \cdot \frac{f_{01}}{f_{02}}$$

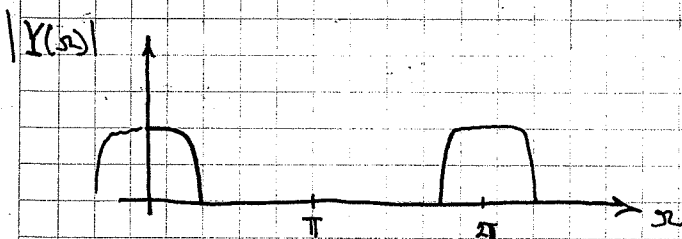
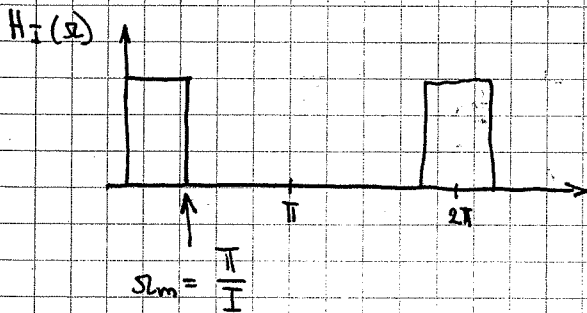
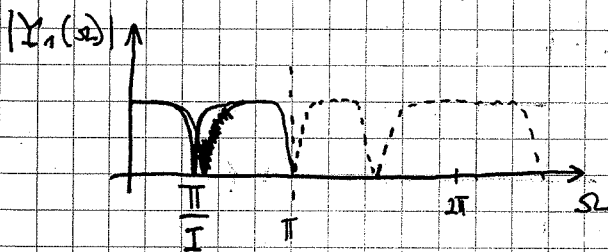
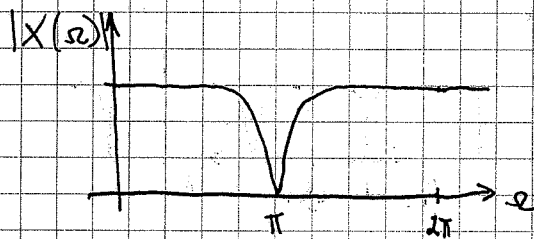


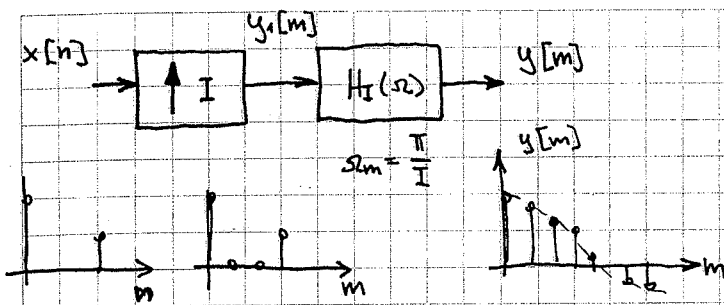
$$y_1[m] = \begin{cases} x[n] & \text{za } m = n \cdot I \\ 0 & \text{za } m \neq n \cdot I \end{cases}$$



$$Y_1(\Omega) = \sum_{m=-\infty}^{\infty} y_1[m] \cdot e^{-j\Omega m} = \sum_{n=-\infty}^{\infty} x[n] \cdot e^{-j\Omega n \cdot I}$$

$$Y_1(\Omega) = X(I \cdot \Omega) \leftarrow \text{skr\u0107enje frekvencijske osi}$$



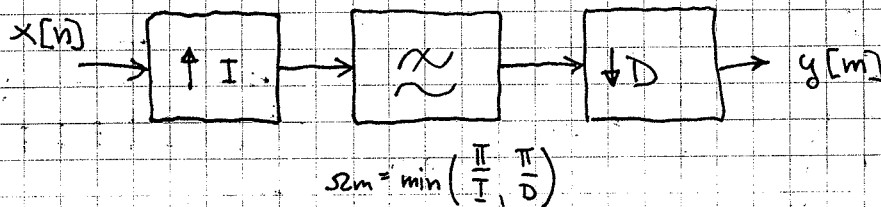
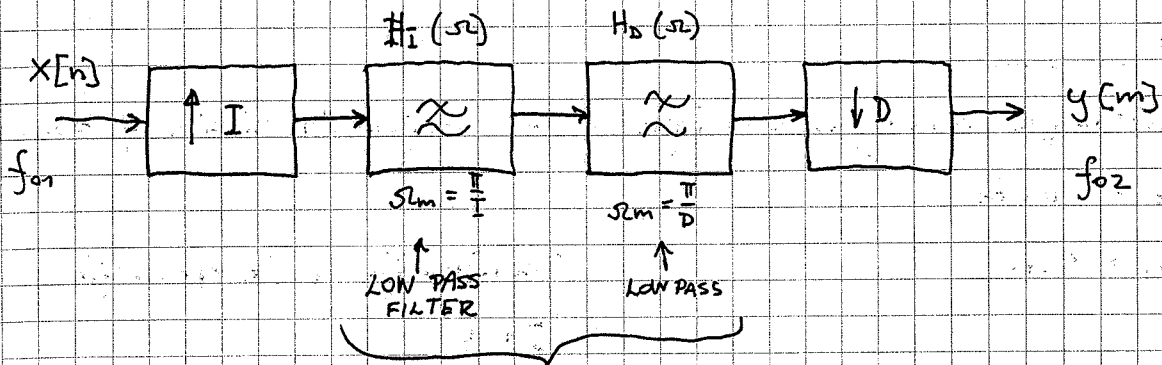


7.4. SPREMEMBA VZORČNE FREKVENCE ZA RACIONALEN FAKTOR

$$\frac{f_{o2}}{f_{o1}} = k = \frac{I}{D}$$

za $k > 1$ je skupno interpolacija
 če $k < 1$ je skupno decimacija

najprej interpoliramo, nato decimiramo



Zgled:

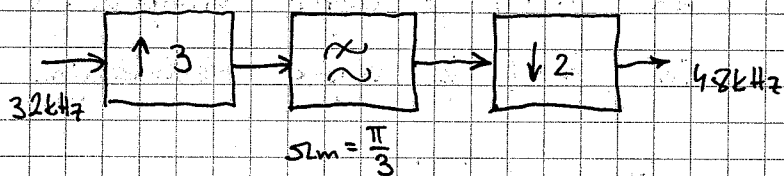
digitalni radio \rightarrow DAT

$$f_{01} = 32 \text{ kHz} \quad \dots \text{ radio}$$

$$f_{02} = 48 \text{ kHz} \quad \dots \text{ DAT}$$

$$f_{02} = f_{01} \cdot \frac{I}{D} \quad \rightarrow \quad \frac{I}{D} = \frac{48 \text{ kHz}}{32 \text{ kHz}} = \frac{3}{2}$$

$$I = 3, \quad D = 2$$

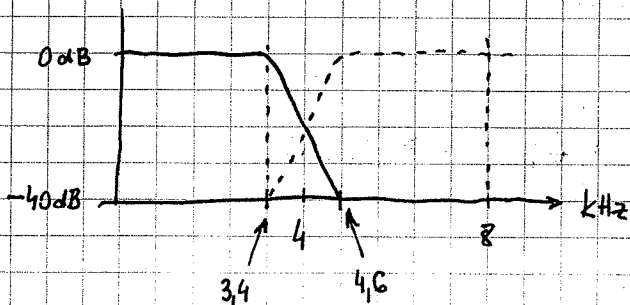


Zgled:

rekonstrukcija analognega signala z enostavnim nizkim filtrom

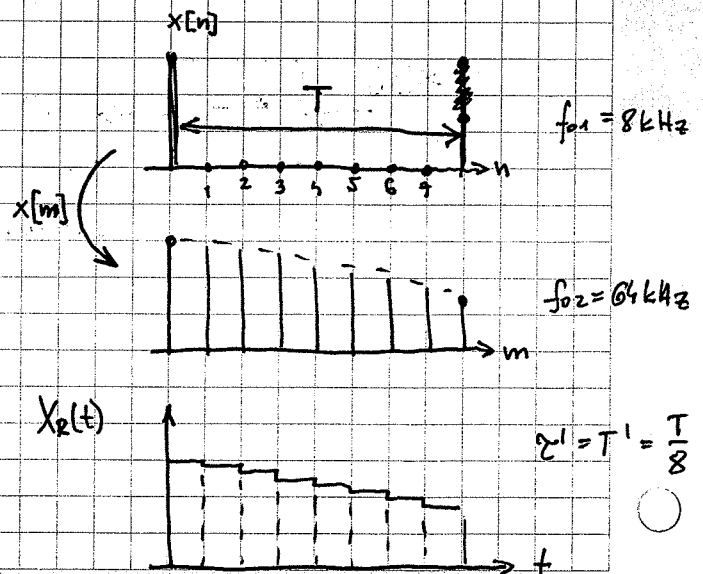
$$f_z = 3400 \text{ Hz}$$

$$f_{01} = 8 \text{ kHz}$$



rekonstrukcija z interpolacijo

$$I = 8$$



$$|X_R(\omega)| = \frac{T'}{T} \left| \frac{\sin \frac{\omega T'}{2}}{\frac{\omega T'}{2}} \right| \sum_{k=-\infty}^{\infty} |X(\omega - k \cdot \omega_{02})|$$

$$T' = \frac{1}{f_{02}} = \frac{1}{2 \cdot I \cdot f_2}$$

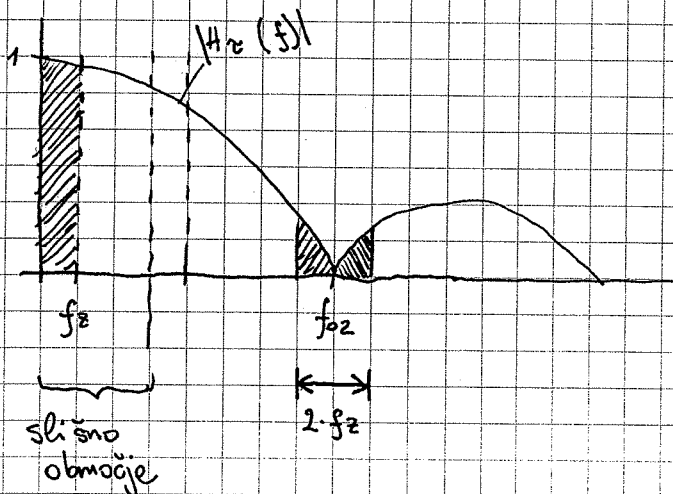
$$|X_R(f)| = \left| \frac{\sin(\pi \cdot T' \cdot f)}{\pi \cdot T' \cdot f} \right| \sum_{k=-\infty}^{\infty} |X(f - k \cdot f_{02})|$$

$k=0$... osnovni pas

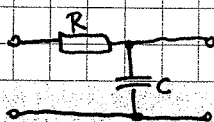
$$|X_R(f)| = \frac{\sin\left(\pi \frac{f}{f_{02}}\right)}{\pi \frac{f}{f_{02}}} \cdot |X(f)|$$

$$f = f_2 \quad |X_R(f_2)| = \frac{\sin \frac{\pi}{16}}{\frac{\pi}{16}} \cdot |X(f_2)| = 0,993 \cdot |X(f_2)|$$

(= -0,5 dB)



$$|H_R(f)|_{f_2 - f_2} = \frac{\sin\left(\pi \frac{f_2 - f_2}{f_{02}}\right)}{\pi \frac{f_2 - f_2}{f_{02}}} = \frac{\sin\left(\pi - \pi \frac{f_2}{f_{02}}\right)}{\pi} = \frac{\sin \pi \frac{f_2}{f_{02}}}{\pi} = \frac{f_2}{f_{02}} = \frac{1}{16}$$



$$|H(f)| = \frac{1}{1 + \left(\frac{f}{f_p}\right)^2}$$

Alta $f_p = \frac{1}{2\pi RC}$

(= -24 dB)

$$-40 \text{ dB} = |H_{LP}(f)| + |H_Z(f)|$$

$$H_{LP}(f_{02}) = -16 \text{ dB} \rightarrow \frac{f_{02}}{f_P} = 6,22$$

$$f_P = \frac{f_{02}}{6,22} = 10 \text{ kHz}$$

$$|H(f)| \Big|_{f=f_Z} = \frac{1}{1 + \left(\frac{4}{10}\right)^2} = 0,88 \quad (= -0,5 \text{ dB})$$

8. VPLIV KVANTIZACIJE SIGNALA IN KOEFICIENTOV NA LASTNOSTI DISKRETNIH SISTEMOV

digitalna izvedba sistemov povzroča dva efekta:

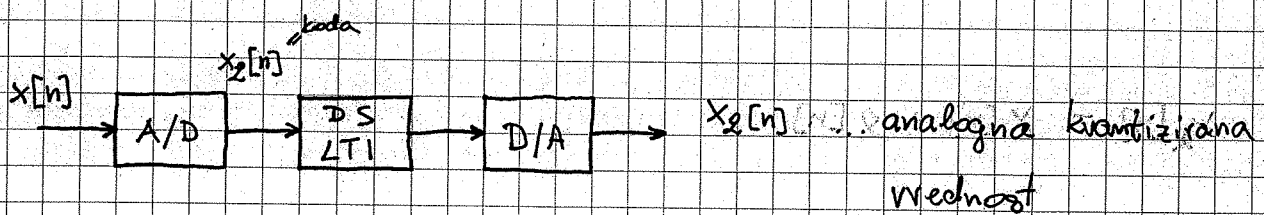
- kvantizacijski šum (napaka)
- odstopanje karakteristike realiziranega sistema ($H(z)$)

Virski za degradacijo so:

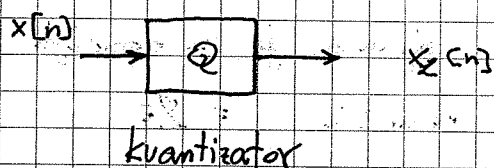
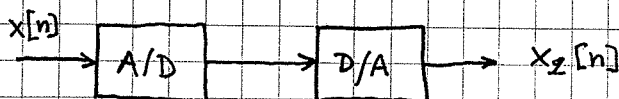
- kvantizacija signala pri A/D pretvorbi
- zaokroževanje delnih rezultatov pri aritmetičnih operacijah

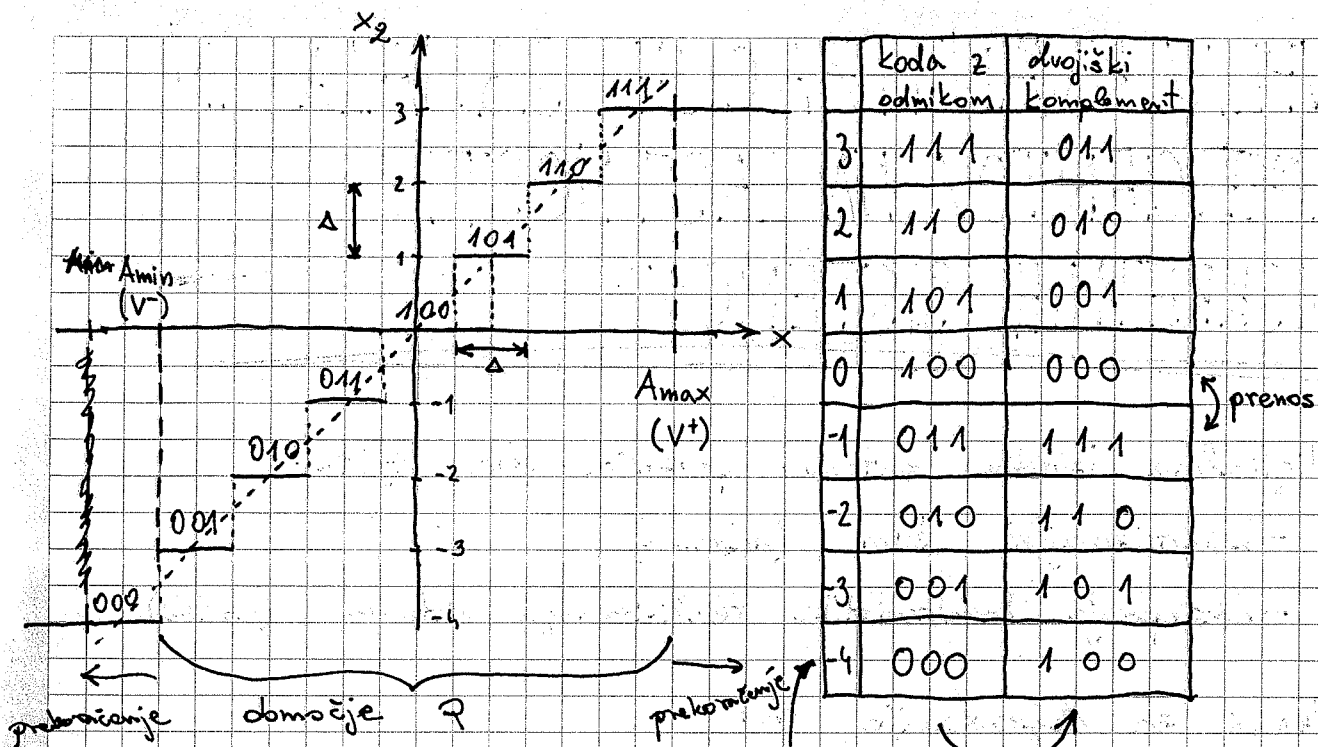
8.1. ANALOGNO DIGITALNA PRETVORBA SIGNALA

8.1.1. KVANTIZACIJA



sistem zamenjamo z idealno identiteto





L - bitov. da 2^L možnih nivojev

$M = 2^L - 1$; ker zavržemo (-4)

za velik L $M \approx 2^L$

$x_2[n] = x[n] + q[n]$

$q[n] = x_2[n] - x[n]$

↑
kvantizacijska napaka oz. šum

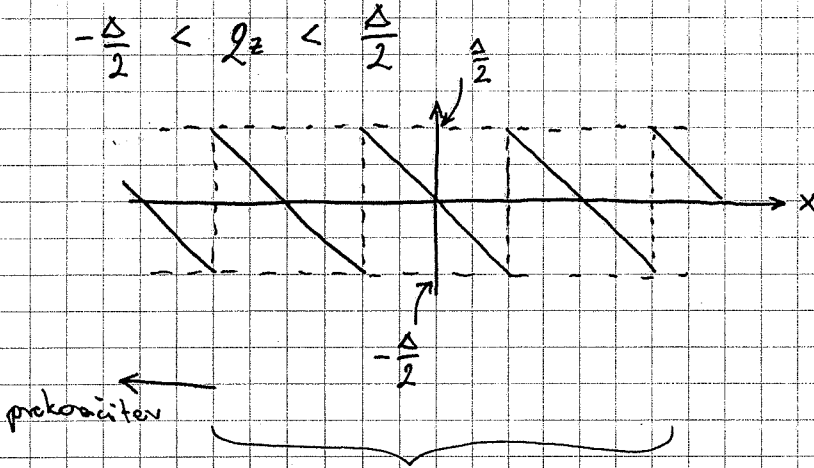
dve vrsti napake:

- ^(granular noise) znato popačenje - amplituda signala je na območju $A_{min} < x < A_{max}$
je znotraj območja $= \Delta$

- ^(overload noise) preokrajšeno popačenje - $x < A_{min}$ ali $x > A_{max}$

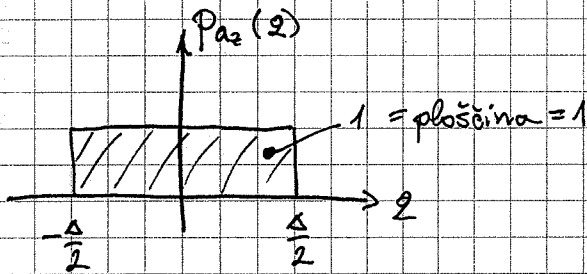
8.1.2. MOČ ZRNATE NAPAKE

$$-\frac{\Delta}{2} < z_2 < \frac{\Delta}{2}$$



porazdelitev gostote verjetnosti za z_2

$$p_{z_2}(z) = \begin{cases} \frac{1}{\Delta} & \text{za } -\frac{\Delta}{2} < z_2 < \frac{\Delta}{2} \\ 0 & \text{drugod} \end{cases}$$



standardna

deviacija

$$\begin{aligned} \sigma_{z_2}^2 &= \overline{z_2^2} = \int_{-\infty}^{\infty} z_2^2 \cdot p_{z_2}(z) dz = \frac{1}{\Delta} \int_{-\frac{\Delta}{2}}^{\frac{\Delta}{2}} z_2^2 \cdot dz = \frac{1}{\Delta} \left. \frac{z_2^3}{3} \right|_{-\frac{\Delta}{2}}^{\frac{\Delta}{2}} = \\ &= \frac{\Delta^2}{12} \end{aligned}$$

$$\overline{z_2^2} = \sigma_{z_2}^2 = N_{z_2} = \frac{\Delta^2}{12}$$

