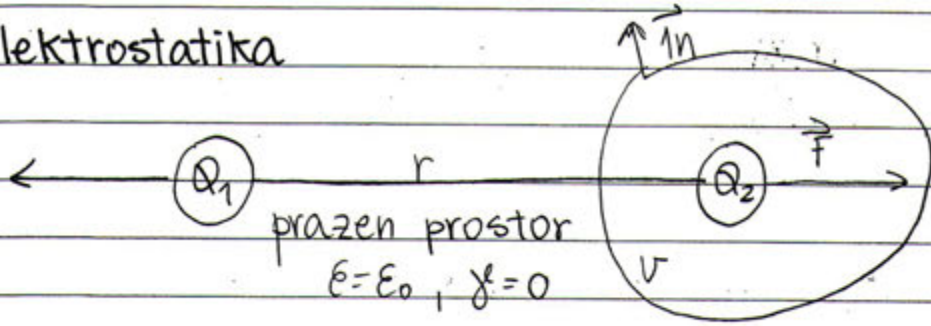


Elektrostatika



enak predznak
→ sila odbojna

sila:
$$\vec{F} = \vec{F}_{odbojna} = \frac{1}{4\pi\epsilon_0} \frac{Q_1 Q_2}{r^2} \quad [N]$$

sila normirana na enoto elektrine:

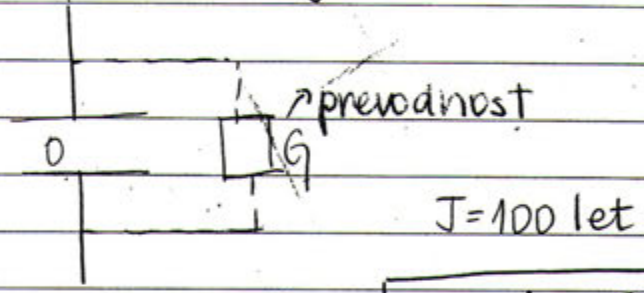
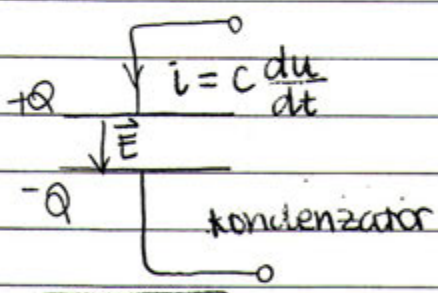
$$\frac{\vec{F}}{Q_1} = \vec{F}_{odbojna} \frac{1}{Q_1} = \vec{E}_2 = \text{vektor el. poljske jakosti} \quad [N/C] = [V/m]$$

vektor električnega pretoka:
$$\vec{D}_2 = \epsilon_0 \vec{E}_2 \quad [As/Vm] [V/m] = [As/m^2] = [C/m^2]$$

Gaussov zakon
$$Q_2 = \oint_A \vec{D} \cdot \vec{n} \cdot dA = \int_V \rho \, dv \quad [As] = [C]$$

napetost:
$$U = \pm \int \vec{E} \cdot d\vec{s}$$

odvisno tako postavimo meje



$$Q = C \cdot U \quad \text{el. energija kondenzatorja} \quad W_e = \frac{1}{2} C U^2$$

SNDR: dielektričnost: $\epsilon \neq \epsilon_0 \quad \epsilon = \epsilon_r \epsilon_0 \quad \epsilon_0 = 8.85 \cdot 10^{-12} \frac{As}{Vm} \quad [As/Vm] = [F/m]$

električna prevodnost: $\gamma \neq 0 \quad [S]$

gostota prevodniškega toka:
$$\vec{J} = \gamma \cdot \vec{E} \quad [A/m^2]$$

prevodniški električni tok:
$$I = \int_A \vec{J} \cdot \vec{n} \, dA$$

$$I = G \cdot U = \frac{U}{R}$$

elektrika se pretvarja v toploto
moč ki se troši na upor:



$$P = I^2 R = \frac{U^2}{R} = U^2 G$$

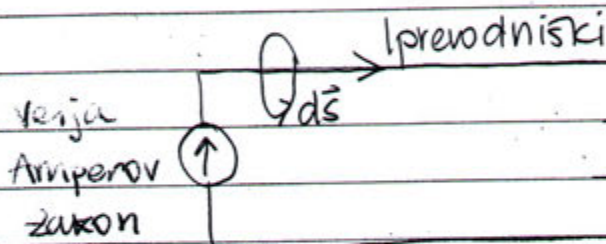
$$[W] = [VA]$$

Magnetostatika: \vec{H} (mag. poljska jakost) → računski pripomoček
Magnetna poljska jakost

$$\oint_S \vec{H} \cdot d\vec{s} = \left[\text{celotni} + \text{prevodniški (konduktivni)} + \text{konvektivni} + \frac{dQ}{dt} \right] \cdot \text{el. veličina}$$

$$\left[\frac{Vs}{m^2} / \frac{Vs}{Am} \right] = [A/m]$$

poljski tok
sprememba elektrine
na enoto časa



$\frac{dQ}{dt}$ količina elektrine
se povečuje

Gostota mag. pretoka $\vec{B} = \mu_0 \vec{H}$ $\vec{B} = \mu \vec{H}$ $[T] = \frac{Vs}{m^2}$

prazen prostor

snov. $\mu = \mu_r \mu_0$

$$\mu_0 = 4\pi \cdot 10^{-7} \frac{Vs}{Am} \quad \left[\frac{Vs}{Am} \right] = [T/m]$$



Faraday-er zakon

$$U_i = - \frac{d\Phi}{dt} = - \frac{d}{dt} \int_A \vec{B} \cdot \vec{n} \cdot dA$$

inducirana
napetost: U_i

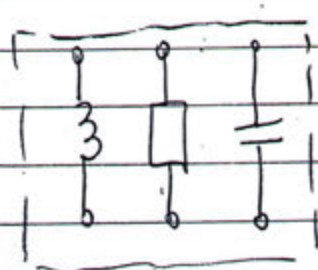
mag. pretok: $\Phi = \int_A \vec{B} \cdot \vec{n} \cdot dA$ $[Wb] = Vs = Tm^2$



induktivnost:

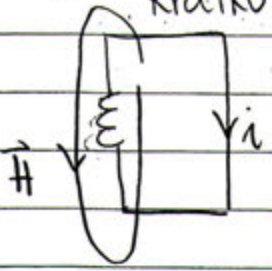
$$U = L \frac{di}{dt}$$

$$W_m = \frac{1}{2} I^2 L$$



Tuljava in kondenzator lahko hranita energija. Kondenzator hrani energijo, če ga odklopimo, tuljava pa če je 0-D ⇒ nič dimenzij kratko sklenjena. Pri kond. lahko to traja "več časa" (100 let), pri tuljavi pa manj časa (1ms, teden-če prevodnik)

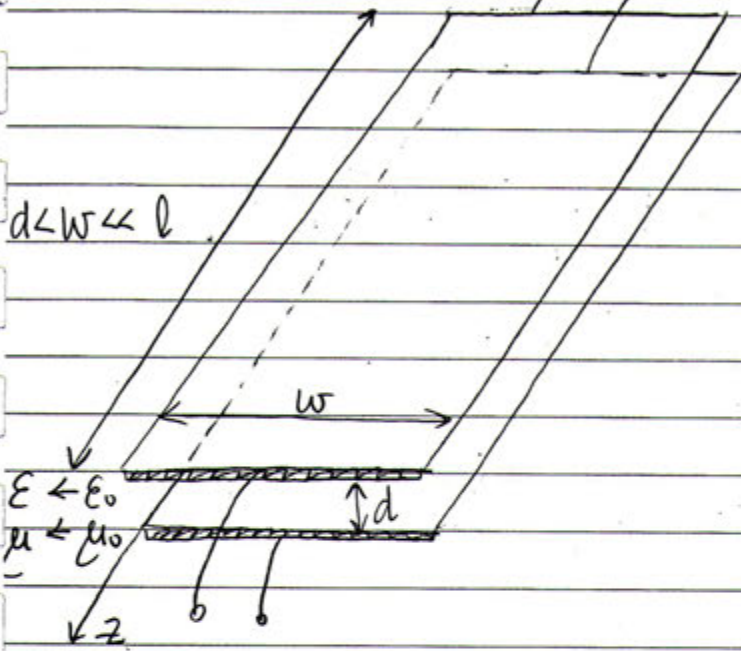
mišna nit
energija, če je
kratko sklenjena



$J_p = 1 \text{ teden}$ $J = 1 \text{ ms}$
na tem upori se troši moč
zgubja se energija

Zgled: TRAKASTI DVONOD

$$l - D = l$$



kapacitivnost na enoto
dolžine

$$C/l = \epsilon \frac{w}{d}$$

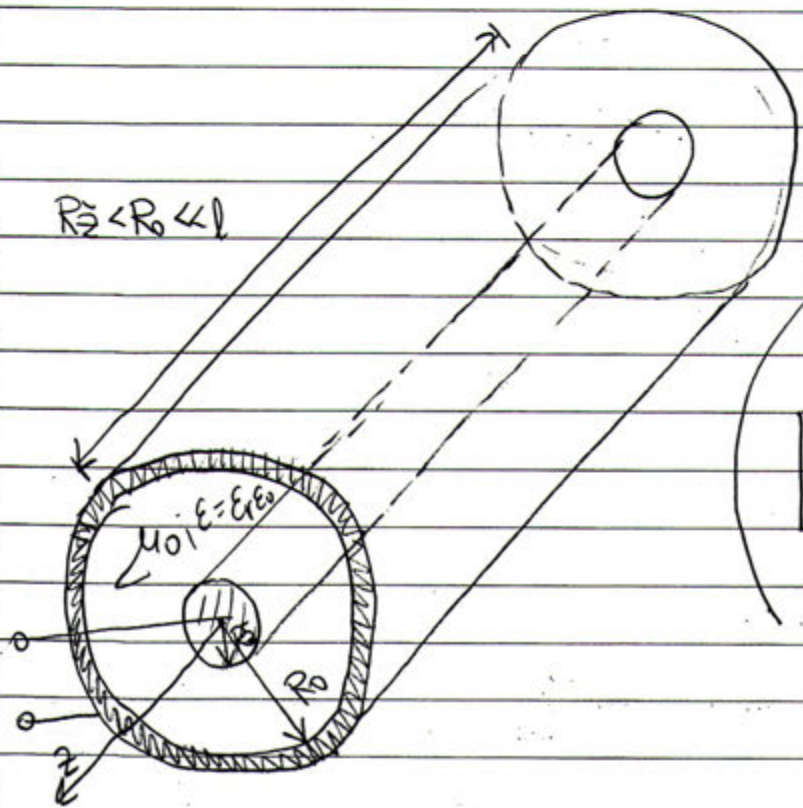
porazdeljene
veličine

$$L/l = \mu \frac{d}{w}$$

induktivnost na enoto dolžine

KOAKSIALNI KABEL

R_z - radij žice ; R_o - radij oklopa



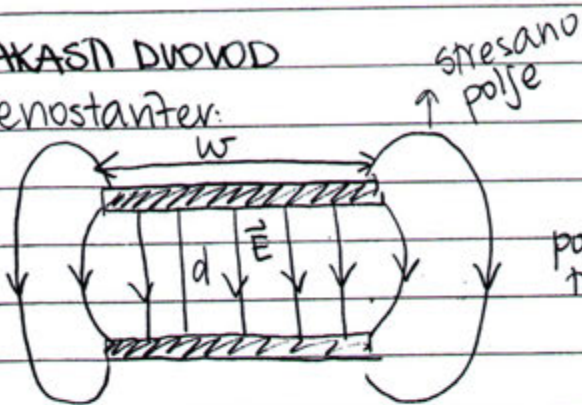
$$C/l = 2\pi\epsilon / \ln \frac{R_o}{R_z}$$

$$L/l = \frac{\mu}{2\pi} \ln \frac{R_o}{R_z}$$

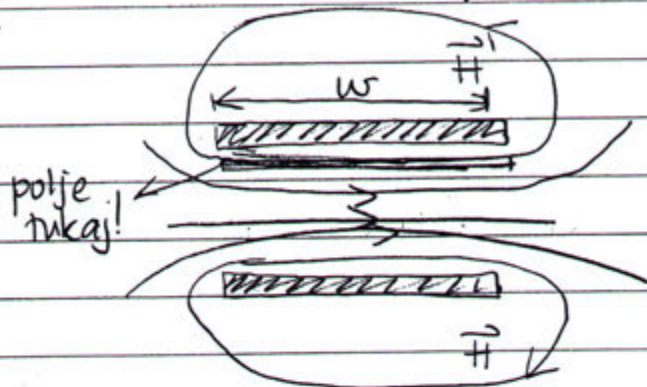
porazdeljene
veličine

TRAKASTI DUVOD

poenostanitev:



$d \ll w \Rightarrow$ mag. polje
skoncetrirano
med ploščama



$d \ll w \Rightarrow$ stresanje zanemarimo

$$C = \epsilon \frac{A}{d} = \epsilon \frac{w \cdot l}{d} = \epsilon \frac{w}{d} \cdot l$$

$$\oint \vec{H} \cdot d\vec{s} = I = |\vec{H}| \cdot w$$

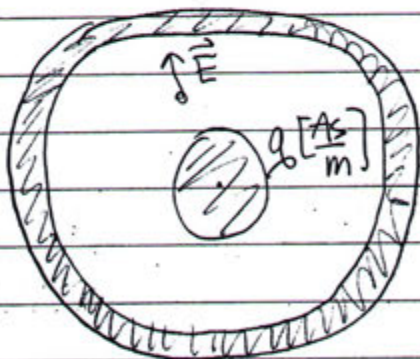
$$|\vec{B}| = \mu \cdot \frac{I}{w} \leftarrow$$

$$\vec{B} = \mu \vec{H}$$

$$\Phi = |\vec{B}| \cdot A = |\vec{B}| \cdot d \cdot l = \mu \frac{I}{w} d \cdot l$$

$$L = \frac{\Phi}{I} = \mu \frac{d}{w} \cdot l$$

KOAKSIALNI KABEL

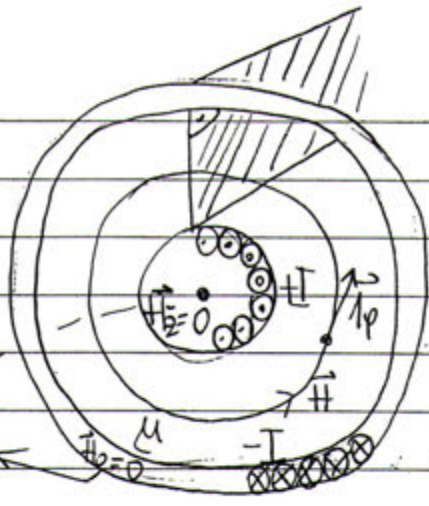


celotna
elektrina
 $Q = q \cdot l$

$$\vec{E} = \vec{r} \cdot \frac{q}{2\pi\epsilon r}$$

$$U = \int \vec{E} \cdot d\vec{s} = \frac{q}{2\pi\epsilon} \ln \frac{R_0}{R_2}$$

$$C = \frac{Q}{U} = \frac{q \cdot l}{q \cdot \frac{1}{2\pi\epsilon} \ln \frac{R_0}{R_2}} = 2\pi\epsilon l / \ln \frac{R_0}{R_2}$$



ker ne zaja me toka

$$\vec{H} = \vec{1}_\varphi \frac{I}{2\pi r}$$

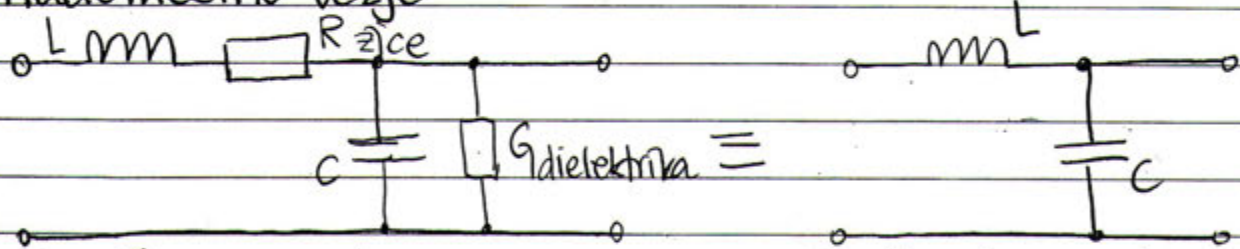
$$\vec{B} = \vec{1}_\varphi \mu \frac{I}{2\pi r}$$

$$\Phi = \int \vec{B} \cdot \vec{n} \cdot dA = \int_{R_2}^{R_0} \int_0^L \vec{B} \cdot \vec{1}_\varphi dr dz = \int_{R_2}^{R_0} \int_0^L \mu \frac{I}{2\pi r} dr dz$$

$$\Rightarrow \Phi = \frac{\mu I}{2\pi} \ln \frac{R_0}{R_2} \cdot L$$

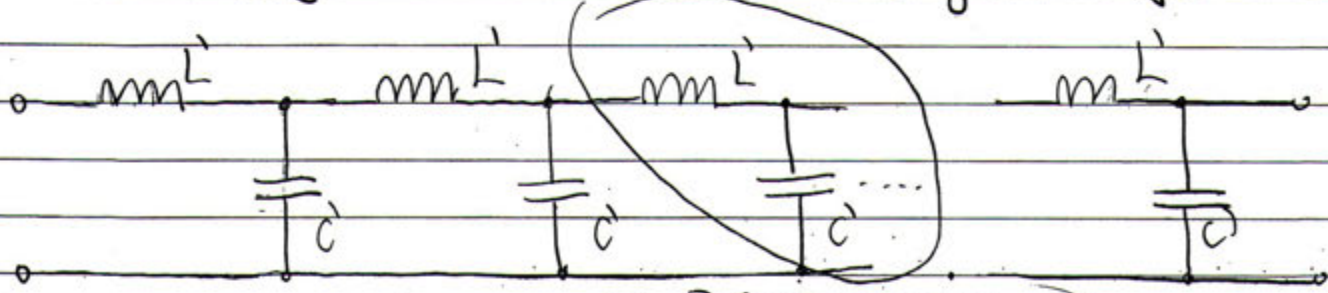
$$L = \frac{\Phi}{I} \Rightarrow L = \frac{\mu}{2\pi} \ln \frac{R_0}{R_2} \cdot L$$

Nadomestno vezje



resnično vezje

brezizgubno vezje



N število odsekov

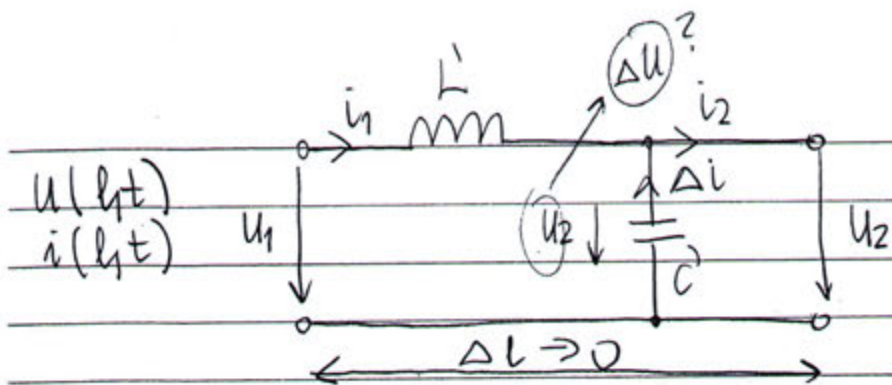
induktivnost enega kratkega odseka

$$L' = \frac{L}{N}$$

kapacitivnost enega kratkega odseka

$$C' = \frac{C}{N}$$

Resnica: $N \rightarrow \infty$



$$\Delta u = u_2 - u_1 = -L' \frac{di_1}{dt}$$

$$L' = L/l \Delta l$$

$$\Delta i = i_2 - i_1 = -C' \frac{du_2}{dt}$$

$$C' = C/l \Delta l$$

$$\Delta u = -L' \frac{di_1}{dt} = -L/l \Delta l \cdot \frac{di_1}{dt}$$

$$\Delta i = -C' \frac{du_2}{dt} = -C/l \Delta l \cdot \frac{du_2}{dt}$$

$$\Delta l \rightarrow 0 \Rightarrow l_1 \approx l_2, \text{ ko } \Delta l \rightarrow 0$$

$$u_2 \approx u_1, \text{ ko } \Delta l \rightarrow 0$$

$$\frac{\Delta u}{\Delta l} = \frac{du}{dl} = -L/l \frac{di_1}{dt} = \frac{du}{dz}$$

$$\frac{\Delta i}{\Delta l} = \frac{di}{dl} = -C/l \frac{du_2}{dt} = \frac{di}{dz}$$

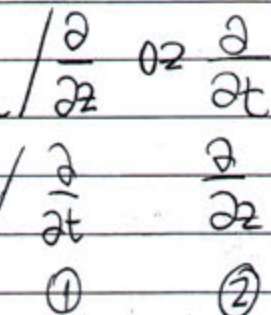
$$\Rightarrow u(z,t): \frac{\partial u(z,t)}{\partial z} = -L/l \frac{\partial i(z,t)}{\partial t}$$

$$i(z,t): \frac{\partial i(z,t)}{\partial z} = -C/l \frac{\partial u(z,t)}{\partial t}$$

| | |
|-----------|--|
| $u(z,t):$ | $\frac{\partial u}{\partial z} = -L/l \frac{\partial i}{\partial t}$ |
| $i(z,t):$ | $\frac{\partial i}{\partial z} = -C/l \frac{\partial u}{\partial t}$ |

Brezizgubna
telegrafaska enačba
v časovnem
prostoru

za u za i



① ②

Rezitev:

$$\Rightarrow \frac{\partial^2 u}{\partial z^2} = -L/l \frac{\partial^2 i}{\partial z \partial t}$$

$$\frac{\partial^2 i}{\partial z \partial t} = -C/l \frac{\partial^2 u}{\partial t^2}$$

vstavimo

iz ①: $\frac{\partial^2 u}{\partial z^2} = (L/l)(C/l) \frac{\partial^2 u}{\partial t^2}$ Enodimenzijska valovna enačba

iz ②: $\frac{\partial^2 i}{\partial z^2} = (L/l)(C/l) \frac{\partial^2 i}{\partial t^2}$ (linearna enačba)

$u(z,t) = ?$, $i(z,t) = ?$

Ugibam: $u(z,t) = u(t \pm \frac{z}{v})$ → zato, ker t [s] in z [m]

$i(z,t) = i(t \pm \frac{z}{v})$ želimo, da je funkcija ene same spremenljivke

$$\frac{\partial u}{\partial t} = u' ; \frac{\partial^2 u}{\partial t^2} = u''$$

vstavimo v *

$$\frac{\partial u}{\partial z} = \pm \frac{1}{v} u' ; \frac{\partial^2 u}{\partial z^2} = \pm \frac{1}{v^2} u''$$

konstanta v ni odvisna od oddaljenosti

$$\Rightarrow \frac{1}{v^2} u'' = (L/l)(C/l) u''$$

$$\frac{1}{v^2} = (L/l)(C/l)$$

$$v = \sqrt{\frac{1}{(L/l)(C/l)}}$$

Zgled: TRAKASTI DUOVOD:

$$v = \sqrt{\frac{1}{\mu \frac{d}{w} \epsilon \frac{w}{d}}} = \frac{1}{\sqrt{\mu \epsilon}}$$

Rezitev enodimenzijske valovne enačbe

hitrost svetlobe

$$\frac{1}{\sqrt{\mu_0 \epsilon_0}} = c_0$$

KOAKSIALNI KABEL:

$$v = \sqrt{\frac{1}{\frac{\mu}{2\pi} \ln \frac{R_0}{R_2} \frac{2\pi \epsilon}{\ln \frac{R_0}{R_2}}}} = \frac{1}{\sqrt{\mu \epsilon}}$$

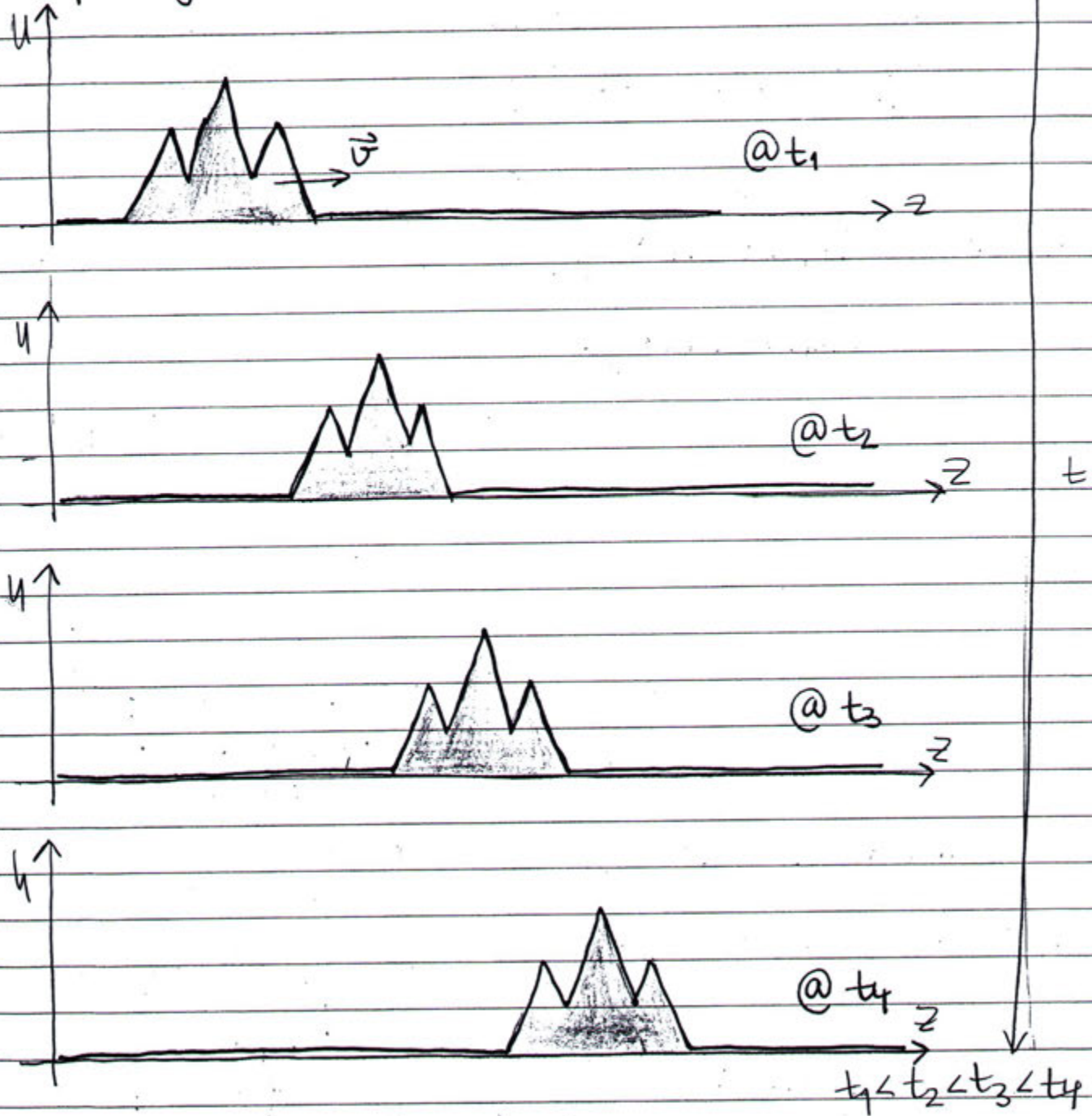
svetlobi ne mirujejo, ampak se gibljejo s to hitrostjo (se spreminja v odvisnosti od snovi)

Možni rešitvi:

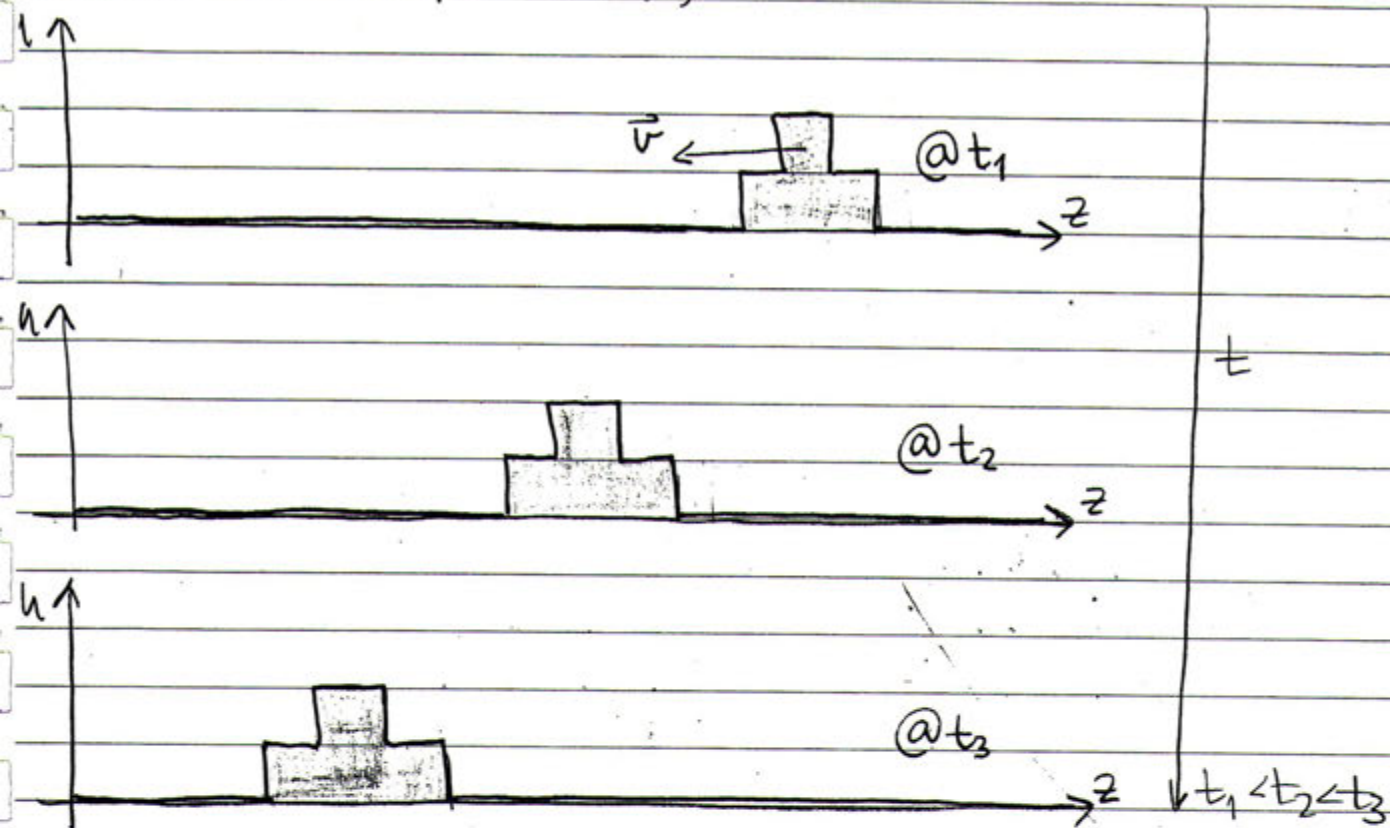
$$u(z,t) = u\left(t - \frac{z}{v}\right) \rightarrow \text{NAPREDUJÓCI VAL}$$

$$u(z,t) = u\left(t + \frac{z}{v}\right) \rightarrow \text{ODBITI VAL}$$

Napredujúci val $u\left(t - \frac{z}{v}\right)$



Odbiti val $u(z,t) = (t + \frac{z}{v})$



Kako vemo, ali je val napredujoči ali odbiti?

$$\frac{\partial i}{\partial z} = -C/l \frac{\partial u}{\partial t} = \pm \frac{1}{v} \frac{\partial i}{\partial t}$$

$$i(z,t) = i(t \pm \frac{z}{v})$$

$$\frac{\partial i}{\partial z} = \pm \frac{1}{v} i' = \pm \frac{1}{v} \frac{\partial i}{\partial t}$$

Napredujoči val in odbiti val lahko hkrati obstajata na nekem delu vodnika

$$-C/l \cdot u' = \pm \frac{1}{v} i' \int \dots dt$$

$$-C/l \cdot u = \pm \frac{1}{v} i + konst$$

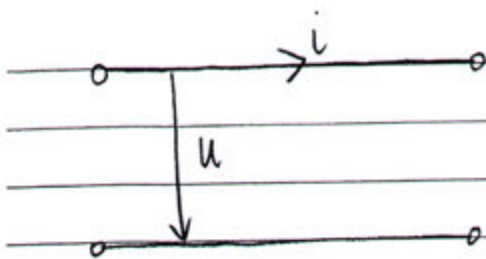
zaradi tega

enosmerna komponenta

samo izmenično:

$$i = \pm v \cdot C/l \cdot u = \pm \sqrt{\frac{1}{C/l \cdot L/l}} \cdot C/l \cdot u = \pm \sqrt{\frac{C}{L}} u$$

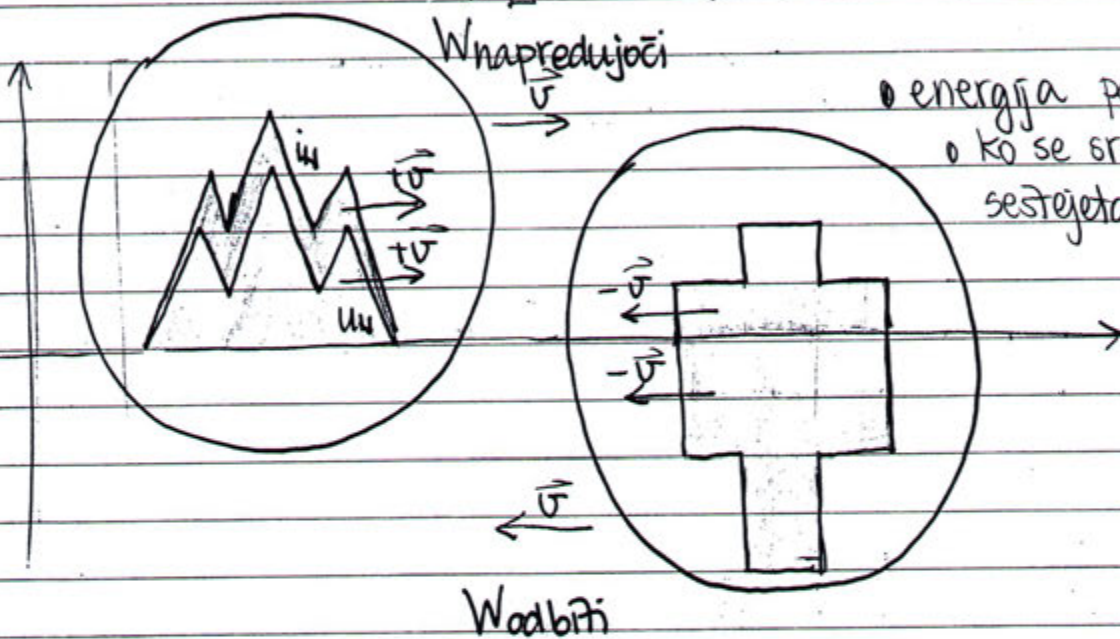
$$v = \sqrt{\frac{1}{L/C}}$$



Napredujoči val: $i = + \frac{C}{L} \cdot u$

razlikujeta se po predznaku toka

Odbiti val: $i = - \frac{C}{L} \cdot u$



$$u_n = \pm \sqrt{L/C} \cdot i_n = Z_k \cdot i_n$$

$$u_o = \pm \sqrt{L/C} \cdot i_o = Z_k \cdot i_o$$

Karakteristična impedanca: $Z_k = \sqrt{L/C} \quad [\Omega]$

Zgled: TRAKASTI DVOVOD

$$Z_k = \sqrt{\frac{\mu \frac{d}{w}}{\epsilon \frac{w}{d}}} = \frac{d}{w} \sqrt{\frac{\mu}{\epsilon}} \Rightarrow Z_k = 377 \Omega \sqrt{\frac{\mu_r}{\epsilon_r} \frac{d}{w}}$$

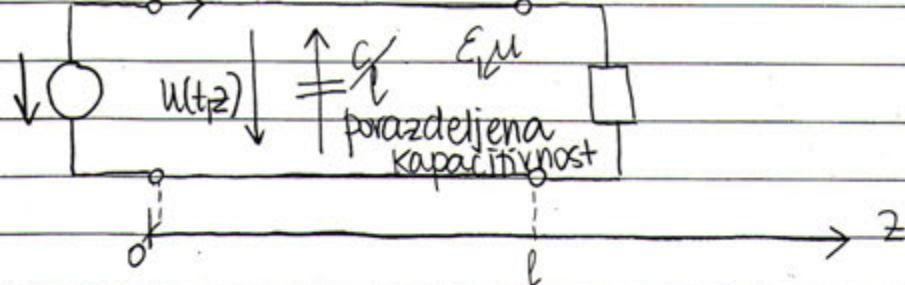
KOAKSIALNI KABEL

$$Z_k = \sqrt{\frac{\frac{\mu}{2\pi} \ln \frac{R_o}{R_z}}{2\pi \epsilon \ln \frac{R_o}{R_z}}} = \sqrt{\frac{\mu}{\epsilon}} \cdot \frac{\ln \frac{R_o}{R_z}}{2\pi} \quad Z_k = 60 \Omega \sqrt{\frac{\mu_r}{\epsilon_r} \ln \frac{R_o}{R_z}}$$

$$\sqrt{\frac{\mu_0}{\epsilon_0}} \approx 120\pi \Omega \approx 377 \Omega$$

karakteristična impedanca se z obliko dvovalda spreminja

1-D naloga: L/l porazdeljena induktivnost



| | |
|---|-------------------------------------|
| $\frac{\partial^2 u(t,z)}{\partial z^2} = C/l \cdot L/l \frac{\partial^2 u(t,z)}{\partial t^2}$ | Telegrafska enačba (brezizgubna) |
| $\frac{\partial^2 i(t,z)}{\partial z^2} = C/l \cdot L/l \frac{\partial^2 i(t,z)}{\partial t^2}$ | |

- rešitve enačbe: $u(t,z) = u(t \pm \frac{z}{v})$

poljubna funkcija ene spremenljivke

$$v = \frac{1}{\sqrt{C/l \cdot L/l}} = \frac{1}{\sqrt{\epsilon \mu}}$$

prazen prostor: $v = \frac{1}{\sqrt{\epsilon_0 \mu_0}} = c_0$

dve linearno neodvisni rešitvi:

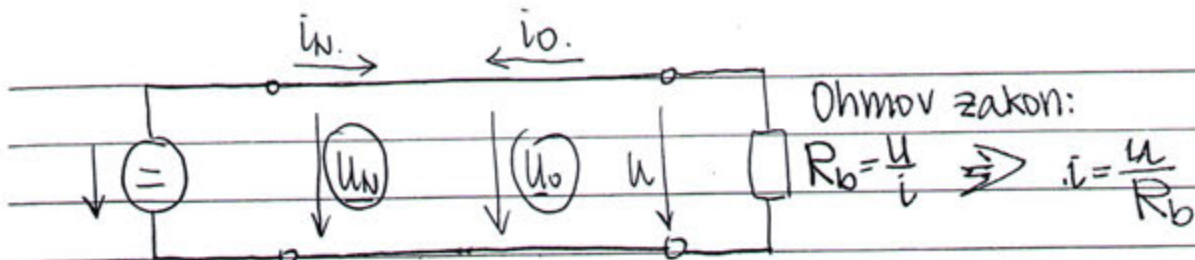
$$u(t,z) = \underbrace{u(t - \frac{z}{v})}_{\text{nápredujúci val}} + \underbrace{u(t + \frac{z}{v})}_{\text{odbiti val}}$$

karakteristična impedanca: $\frac{U}{I} = \pm Z_k$

$$Z_k = \sqrt{\frac{L/l}{C/l}} = \sqrt{\frac{L}{C}}$$

$$\frac{U_{\text{napr.}}}{I_{\text{napr.}}} = +Z_k \Rightarrow i_{\text{napr.}} = \frac{U_{\text{napr.}}}{Z_k} *$$

$$\frac{U_{\text{odbiti}}}{I_{\text{odbiti}}} = -Z_k \Rightarrow i_{\text{odbiti}} = \frac{-U_{\text{odbiti}}}{Z_k} *$$



U_N, U_o podana \rightarrow na bremenu

$$U = U_N + U_o$$

$$i = i_w + i_o$$

$$i_z * \quad i = \frac{U_N}{Z_k} - \frac{U_o}{Z_k}$$

$$i = \frac{U_N + U_o}{R_b} = \frac{U_N - U_o}{Z_k}$$

ohmov zakon

$$U_o \left(\frac{1}{R_b} + \frac{1}{Z_k} \right) = U_N \left(\frac{1}{Z_k} - \frac{1}{R_b} \right) / Z_k \cdot R_b$$

$$U_o (Z_k + R_b) = U_N (R_b - Z_k)$$

razmerje: $\frac{U_o}{U_N} = \frac{R_b - Z_k}{R_b + Z_k}$ opisuje za kakšno breme gre. razmerje odbitega in napredujočega vala.

odbojnost: $\Gamma = \frac{U_o}{U_N} = \frac{R_b - Z_k}{R_b + Z_k}$

PAZI!

- vedno definirana na napetosti U ali el. poljsko jakostjo \vec{E}
- če definirana na i ali \vec{H} obraten predznak

- Zgled

• PRILAGODJENO BREME: $R_b = Z_k \Rightarrow \Gamma = 0$

• KRATEK STIK: $R_b = 0 \Rightarrow \Gamma = -1$

• ODPRTE SPONKE: $R_b = \infty \Rightarrow \Gamma = 1$

• $Z_k = 50 \Omega, R_b = 100 \Omega \Rightarrow \Gamma = \frac{100 \Omega - 50 \Omega}{100 \Omega + 50 \Omega} = \frac{50 \Omega}{150 \Omega} = \underline{\underline{0,333}}$

• $Z_k = 50 \Omega, R_b = 10 \Omega \Rightarrow \Gamma = \frac{10 \Omega - 50 \Omega}{10 \Omega + 50 \Omega} = \frac{-40 \Omega}{60 \Omega} = \underline{\underline{-0,667}}$

lastnost odbojnosti:

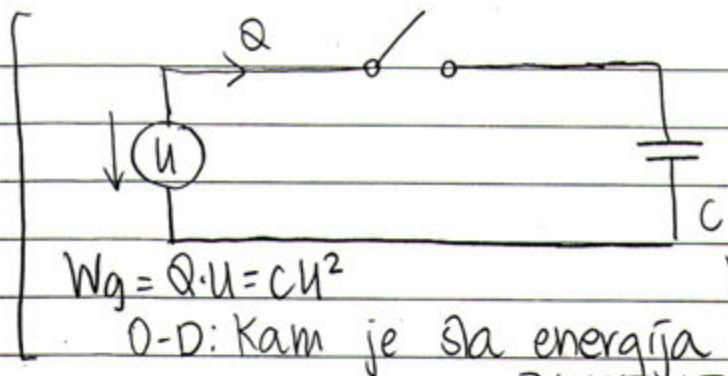
pasivno breme: $|\Gamma| \leq 1$

\rightarrow odbiti val sibejsi od napredujočega vala

predznak: (-) breme manjše od Z_k

(+) breme večje od Z_k

ko vključimo stikalo se prazen kondenzator napolni na napetost U



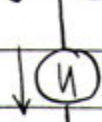
$$W_c = \frac{1}{2} \cdot C \cdot U^2$$

$$W_g = Q \cdot U = C \cdot U^2$$

0-D: Kam je šla energija

ZVONENJE SIGNALA

$$R_g = 0 \Rightarrow \Gamma_g = -1$$



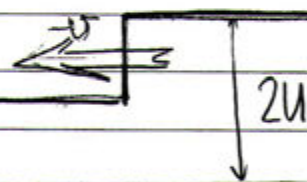
odprte sponke $\Gamma_b = 1$

o sklenemo stikalo U



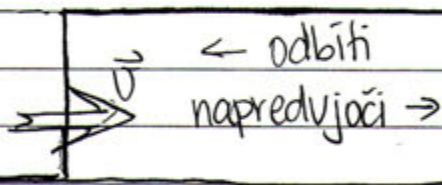
fronta napredujočega vala

na koncu se odbije vsi val = napr. val



$\Gamma = 1$
0.5 fronta odbitega vala; napetost se podvoji $\rightarrow z$

odbiti val e nekaj odbije in se nihci

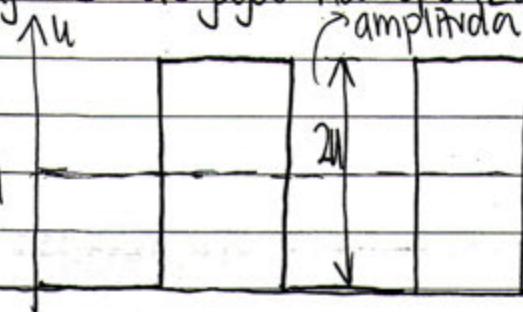


* tresimo v generator z

imamo generator $z + U$ in odboj od odboja $z - U$, fronta napreduje iz 0 naprej

zmanjka napredujočega vala

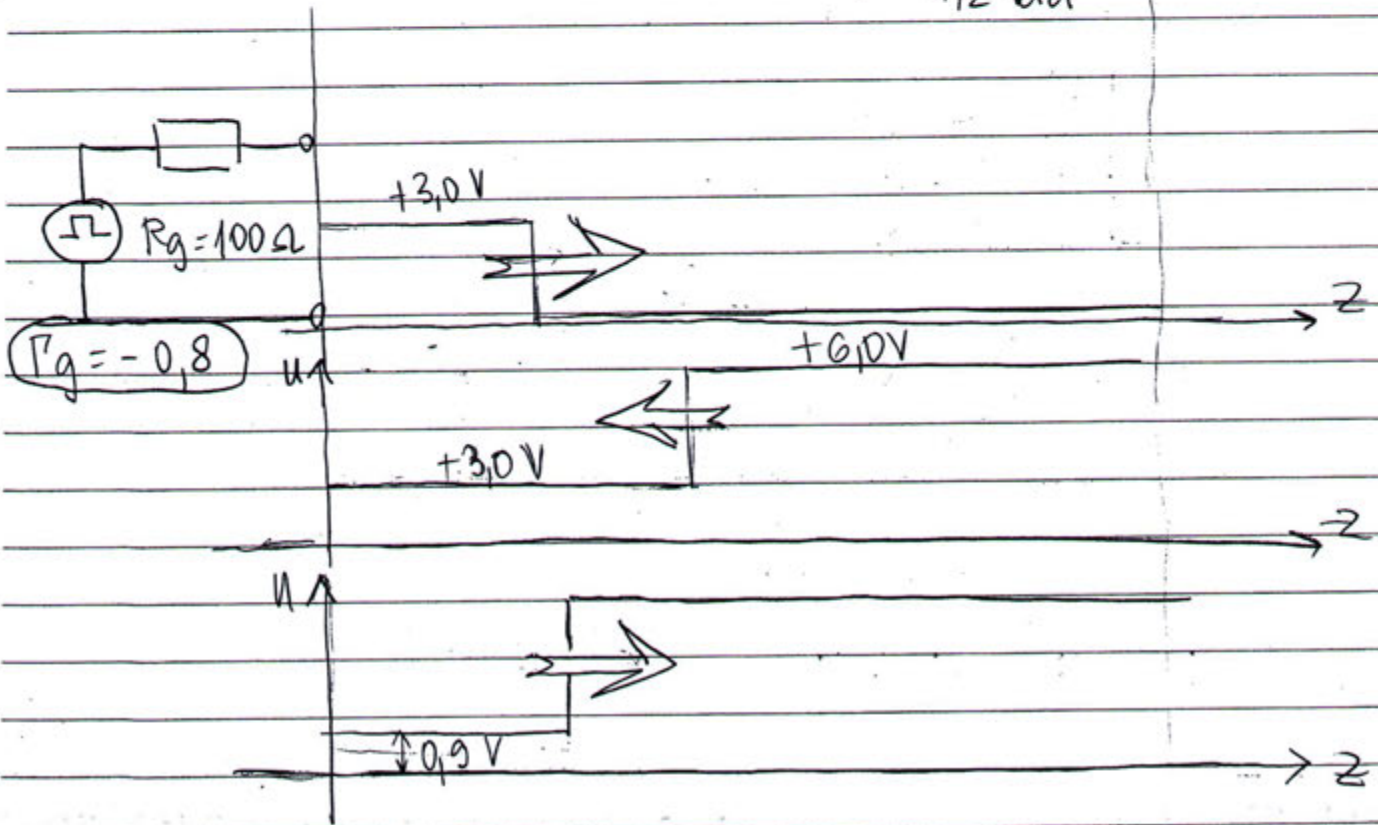
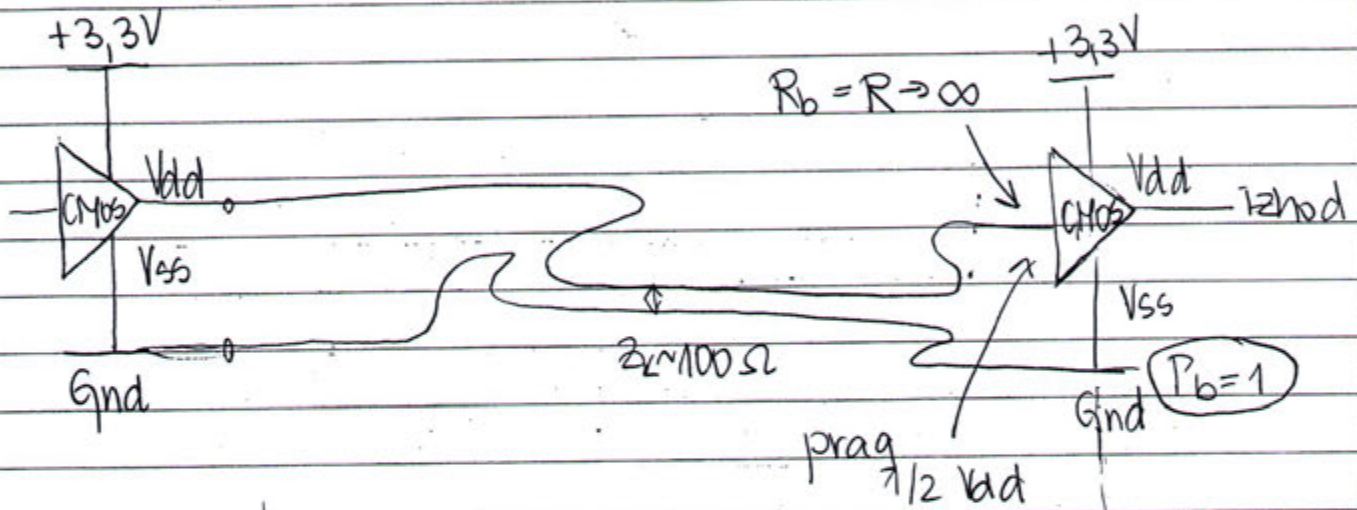
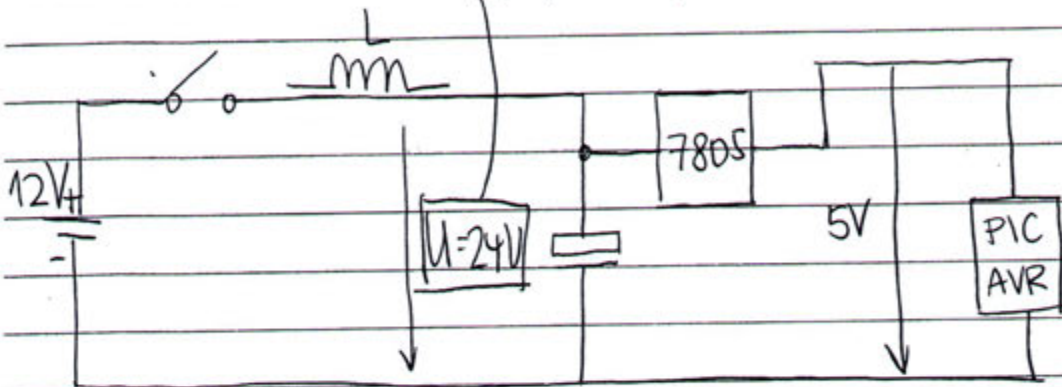
Kaj se dogaja na sponkah?

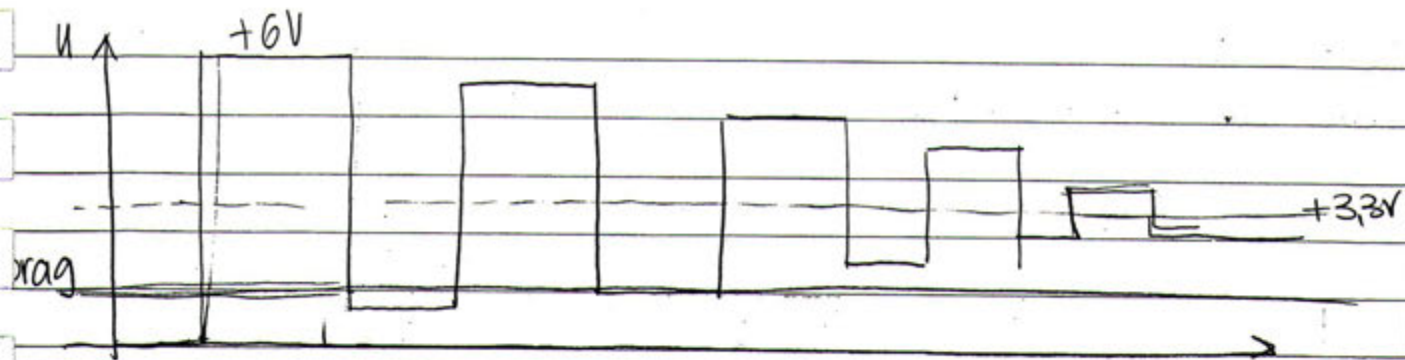


* pol napetosti od odbitega, pol pa od napredujočega vala

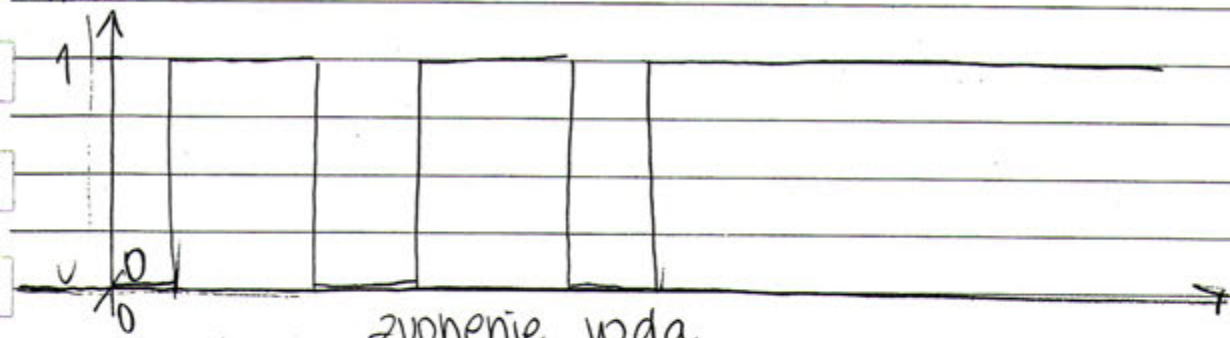
Primer:

glej nazaj 2u!



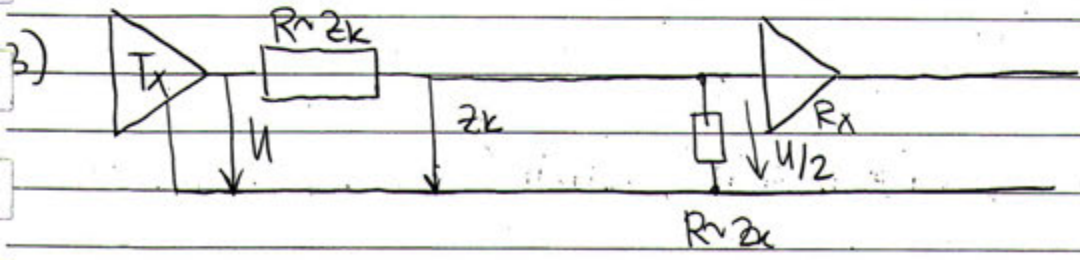
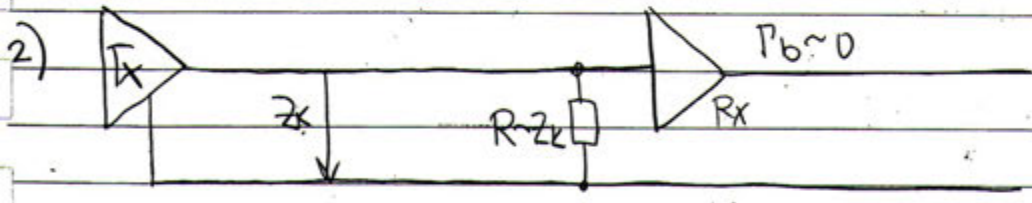
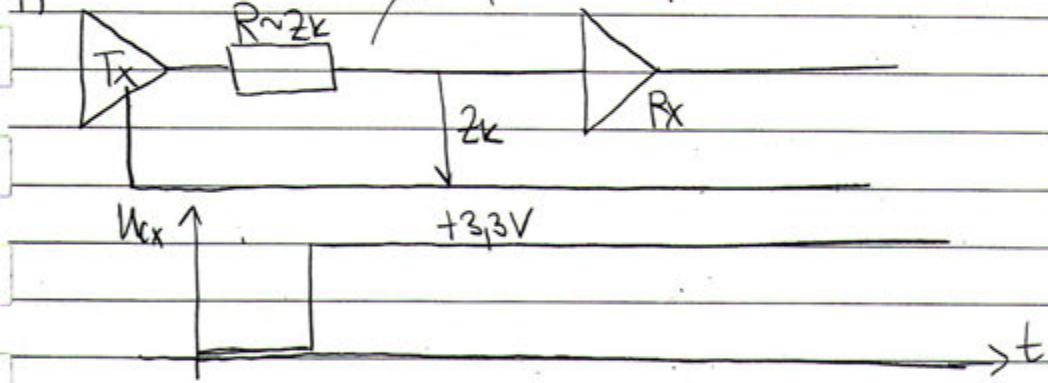


izhod:

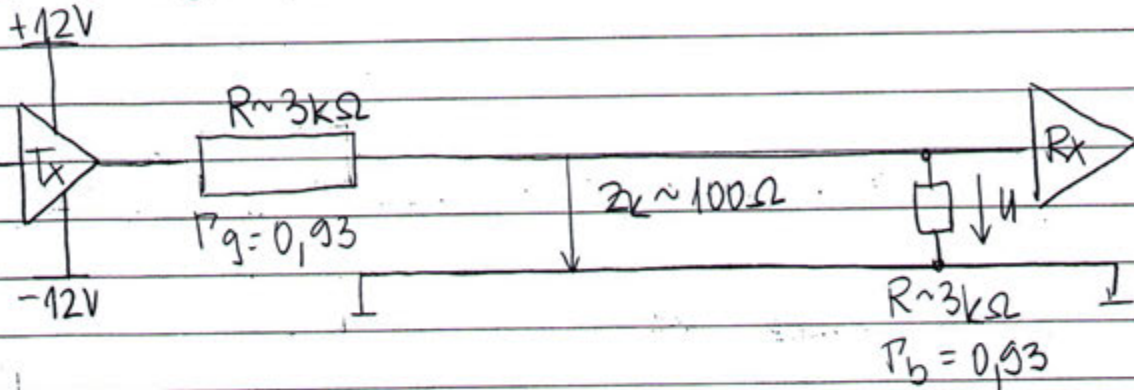


zvonjenje voda

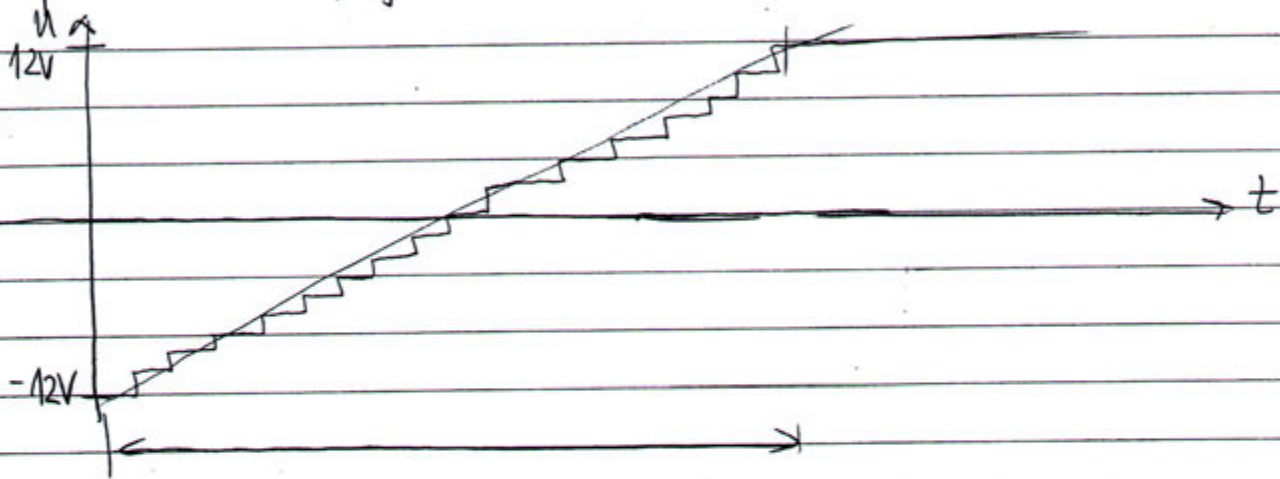
Kako to rešimo? Da preprečimo zvonjenje voda za poredni upor R da vodila ne zvonijo



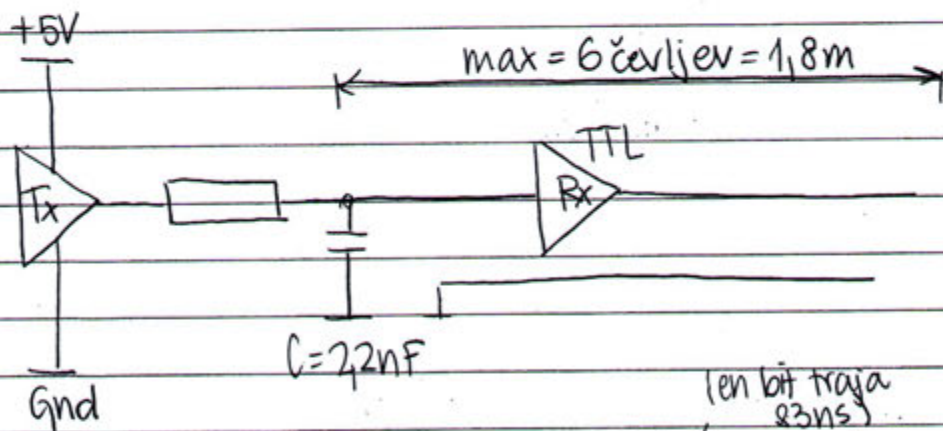
COM port
RS-232 ($C < 115 \text{ kbit/s}$)



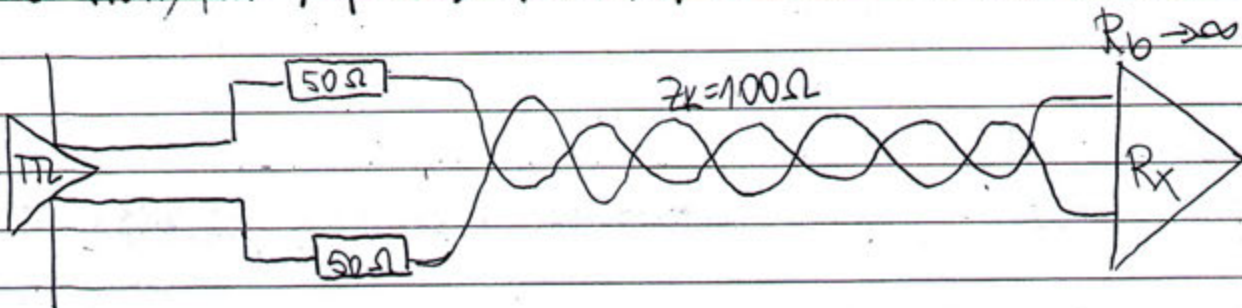
napetost na sprejemniku:



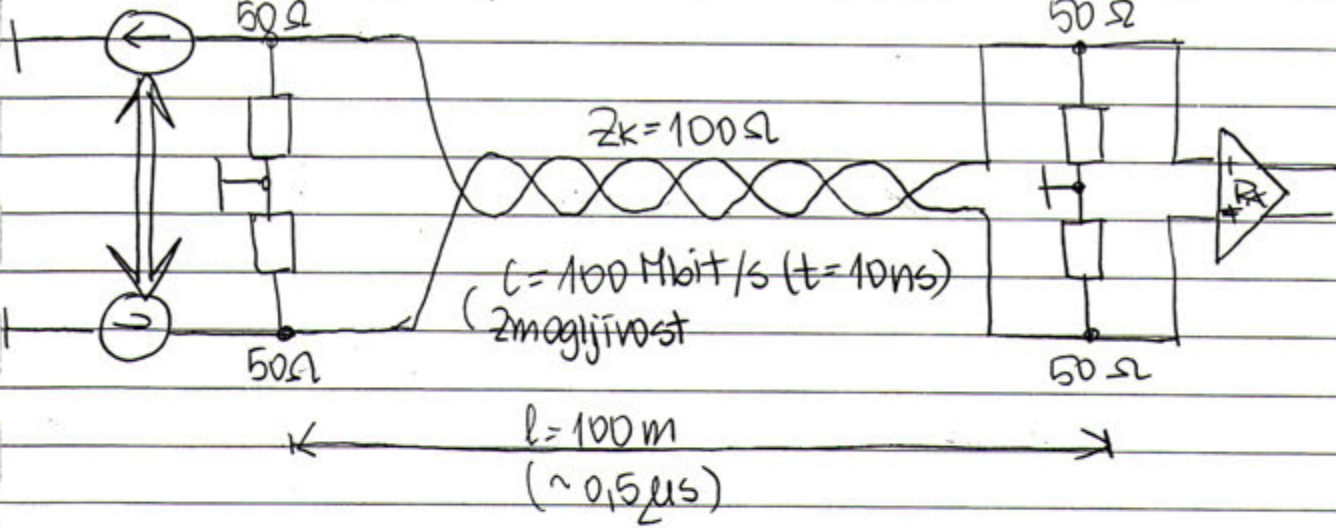
LPT (tiskalnik)



USB (low/full) speed $\Rightarrow 1,5 \text{ Mbit/s} / 12 \text{ Mbit/s} \Rightarrow l = 2 \text{ m}$ (10 ns)

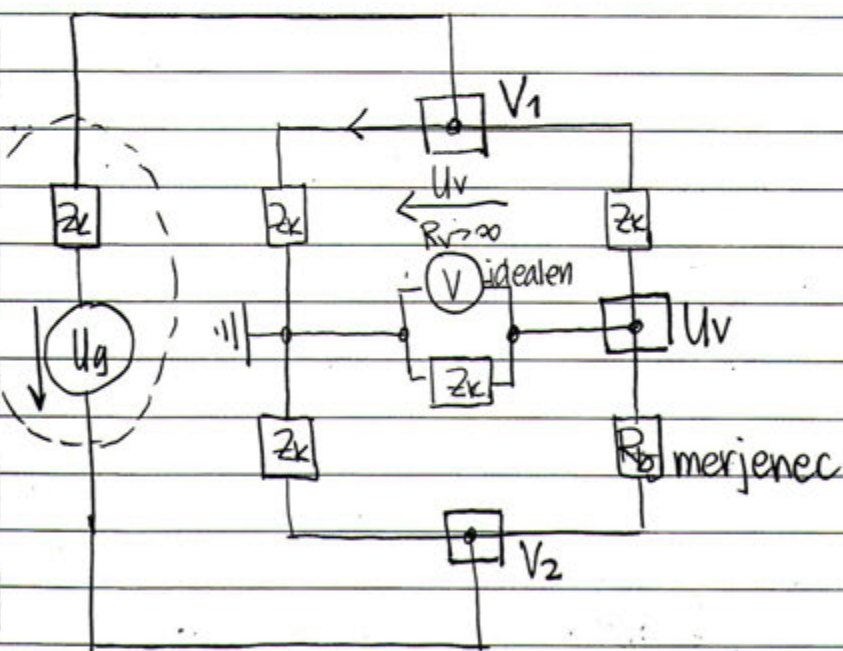


Ethernet/UTP (hi-speed USB 120 Mbit/s)



Meritev odbojnosti Γ ?

Postižek:



Vozlišne enačbe

$$I: 0 = V_1 \frac{1}{Z_k} + (V_1 - U_v) \frac{1}{Z_k} + (V_1 - V_2 - U_g) \frac{1}{Z_k} \quad (1)$$

$$IV: 0 = (U_v - V_1) \frac{1}{Z_k} + U_v \frac{1}{Z_k} + (U_v - V_2) \frac{1}{R_0} \quad (2)$$

$$II: 0 = V_2 \frac{1}{Z_k} + (V_2 - V_1 + U_g) \frac{1}{Z_k} + (V_2 - U_v) \frac{1}{R_0} \quad (3)$$

V_1, V_2 izračimo

$$z(1) \Rightarrow -V_1 \frac{3}{z_k} = -\frac{U_v}{z_k} - \frac{U_2 + U_g}{z_k}$$

$$3V_1 = U_v + U_2 + U_g \quad (\text{vstavimo v (2) in (3)})$$

$$iz(2) \Rightarrow 0 = (3U_v - (U_v + V_2 + U_g)) \frac{1}{z_k} + \frac{3U_v}{z_k} + \frac{3U_v}{R_b} - \frac{3V_2}{R_b} =$$

$$= U_v \left(\frac{5}{z_k} + \frac{3}{R_b} \right) - \frac{V_2}{z_k} - \frac{3V_2}{R_b} - \frac{U_g}{z_k} \quad / \cdot 5$$

$$iz(3) \Rightarrow 0 = \frac{3V_2}{z_k} + \frac{3V_2}{z_k} - \frac{U_v + V_2 + U_g}{z_k} + \frac{3U_g}{z_k} + \frac{3V_2}{R_b} - \frac{3U_v}{R_b} =$$

$$= -\frac{U_v}{z_k} - \frac{3U_v}{R_b} + \frac{5V_2}{z_k} + \frac{3V_2}{R_b} + \frac{2U_g}{z_k}$$

seštejemo:

$$0 = \frac{4U_v}{z_k} + \frac{4V_2}{z_k} + \frac{U_g}{z_k} \quad / \cdot 3 \quad \frac{z_k}{R_b} \Rightarrow 0 = \frac{12U_v}{R_b} + \frac{12V_2}{R_b} + \frac{3U_g}{R_b}$$

odštejemo:

$$0 = \frac{24U_v}{z_k} + \frac{12U_v}{R_b} - \frac{12V_2}{R_b} - \frac{3U_g}{z_k}$$

$$0 = \frac{24U_v}{z_k} + \frac{24U_v}{R_b} - \frac{3U_g}{z_k} + \frac{3U_g}{R_b} \quad / : 3$$

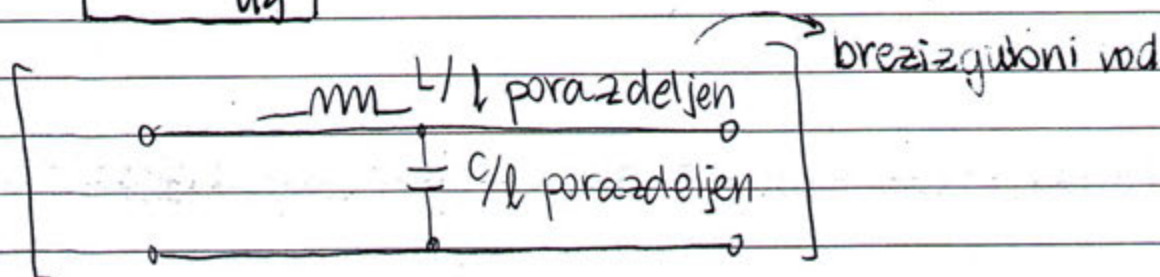
$$0 = 8U_v \left(\frac{1}{z_k} + \frac{1}{R_b} \right) + U_g \left(\frac{1}{R_b} - \frac{1}{z_k} \right) \quad / \cdot R_b z_k$$

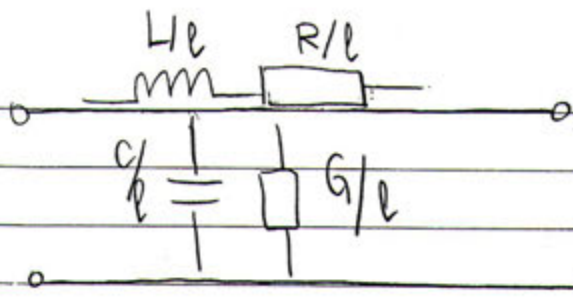
$$0 = 8U_v (R_b + z_k) + U_g (z_k - R_b)$$

$$U_v = \frac{U_g}{8} \frac{R_b - z_k}{R_b + z_k} \Rightarrow U_v = \frac{U_g}{8} \quad \text{P sorazmernost}$$

z odbojnostjo
za merjenje potrebujemo
le realne elemente

$$P = \frac{8U_v}{U_g}$$



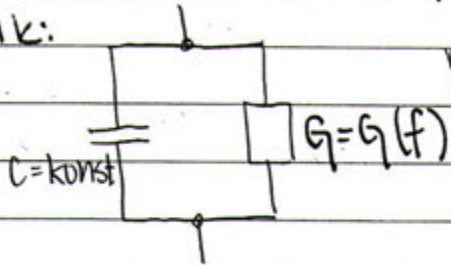


Upoštevati moramo še
 upornost in prevodnost
 ↓
 izgubni vod

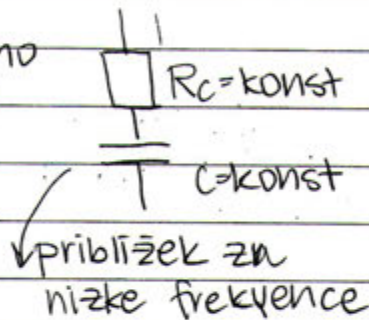
žica: $L = \text{konst.}$ $R = \alpha \sqrt{f}$

Upor odvisen od frekvence

dielektrik:



nadomestno vezje



Reševanje Telegrafске enačbe v frekvenčnem prostoru

$$u(t) = \text{Re} [\hat{U} e^{j\omega t}]$$

1) brezizgubna Telegrafska enačba

$$\frac{\partial^2 u}{\partial z^2} = C/l \cdot L/l \quad \frac{\partial^2 u}{\partial t^2} = \mu \epsilon \frac{\partial^2 u}{\partial t^2}$$

poskus: nastavek, ki ga ljubimo
 časovni prostor: $u(z, t) = u(t \pm \frac{z}{v})$ iz časovnega prostora

$$u(z, t) = \text{Re} [\hat{U}_0 e^{j\omega(t \pm \frac{z}{v})}] \quad \text{nov nastavek } u = U_0 e^{j\omega(t \pm \frac{z}{v})}$$

$$\frac{\partial^2 u}{\partial z^2} = \frac{\omega^2}{v^2} U_0 e^{j\omega(t \pm \frac{z}{v})} = -\frac{\omega^2}{v^2} u$$

$$\frac{\partial^2 u}{\partial t^2} = -\omega^2 u$$

Vstavimo v diferencialno enačbo:

$$-\frac{\omega^2}{v^2} u = -\omega^2 \mu \epsilon u$$

Impedanca (ne upornost)
 bremena

$$v = \frac{1}{\sqrt{\mu \epsilon}}$$

$$Z_k = \sqrt{\frac{L/l}{C/l}}$$

$$\Gamma = \frac{Z_b - Z_k}{Z_b + Z_k}$$

↳ v splošnem primeru
 je Γ kompleksen.

Velja $|\Gamma| \leq 1$ za pasivno breme

Vidimo, da veljajo enake enačbe.

kazalec

$$U = U_0 e^{j\omega(t \pm \frac{z}{v})} = U_0 e^{j(\omega t + \varphi)}$$

$$\varphi = \omega \cdot \frac{z}{v} = \frac{\omega}{v} \cdot z$$

fazna konstanta β pri izmeničnih
veličinah
(valovno število k)

$$\frac{\omega}{v} = \beta = k = \omega \sqrt{\mu \epsilon}$$

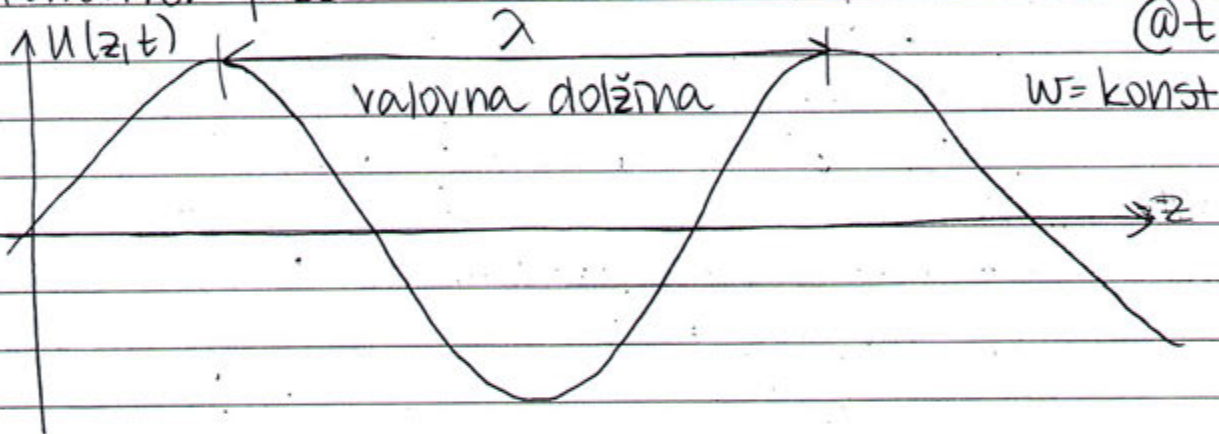
↑ koliko radianov naredi
faza na 1 m razdalje $\left[\frac{\text{rad}}{\text{m}} \right]$

$$\begin{aligned} U &= U_0 e^{j(\omega t + \beta z)} \\ U &= U_0 e^{j(\omega t + kz)} \end{aligned}$$

prazen prostor
 μ_0, ϵ_0

$$k_0 = \frac{\omega}{c_0} = \omega \sqrt{\mu_0 \epsilon_0}$$

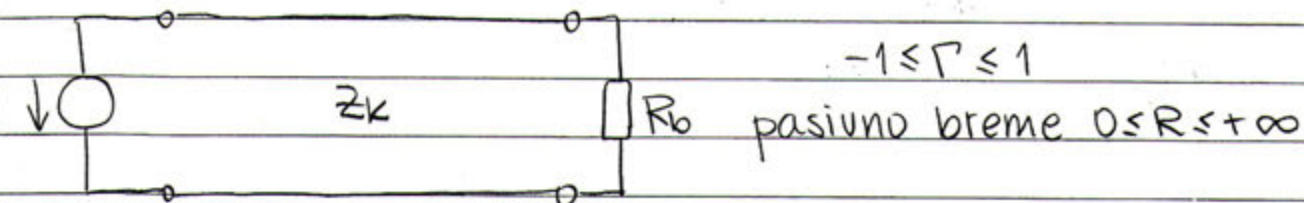
Ponovitev faze:



$$\lambda \cdot \beta = \lambda \cdot k = 2\pi$$

$$\lambda = \frac{2\pi}{k} \quad \text{oz.} \quad k = \frac{2\pi}{\lambda}$$

ponovitev:

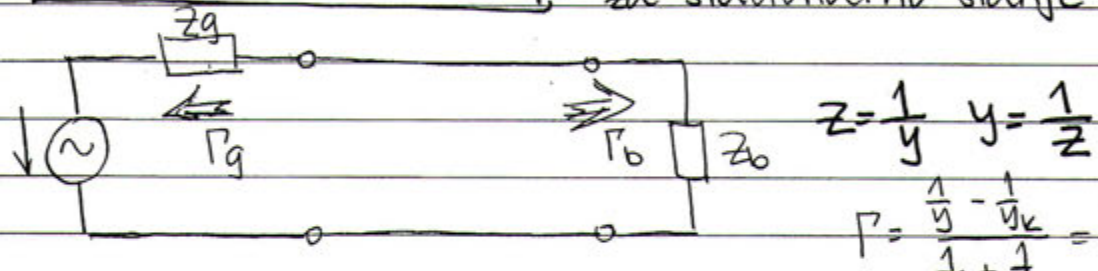


odbojnost: $\Gamma = \frac{R - Z_k}{R + Z_k} \iff R = Z_k \frac{1 + \Gamma}{1 - \Gamma}$

Kaj se dogaja z napredujočim in odbitnim valom?

$u_N = \text{Re} [U_N e^{j(\omega t + \beta z)}]$
 $u_o = \text{Re} [U_o e^{j(\omega t + \beta z)}]$
 $\beta = k = \omega \sqrt{\mu \epsilon} = \frac{\omega}{v}$

resitev: en sam v
 \implies stacionarno stanje
 odbojnost najlaže računamo za stacionarno stanje



$\Gamma = \frac{\frac{1}{Y} - \frac{1}{Y_k}}{\frac{1}{Y} + \frac{1}{Y_k}} = \frac{Y_k - Y}{Y_k + Y}$

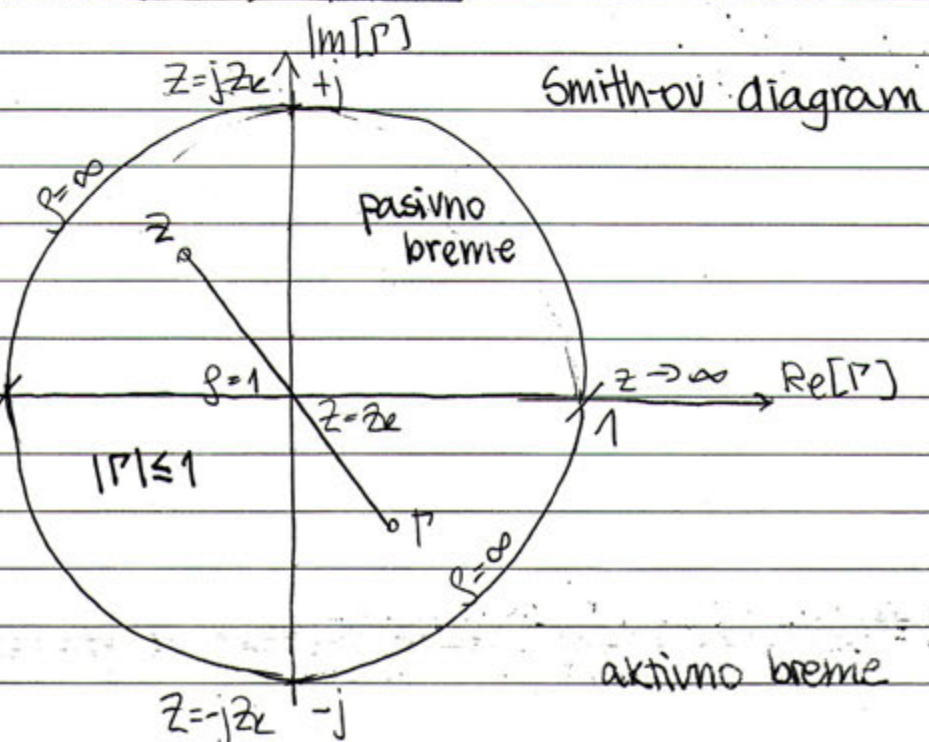
za izmenične veličine:

$\Gamma = \frac{Z - Z_k}{Z + Z_k}$ i $\Gamma = \frac{Y - Y_k}{Y + Y_k}$

pasivno breme: $\text{Re}[Z] \geq 0 \implies |\Gamma| \leq 1$

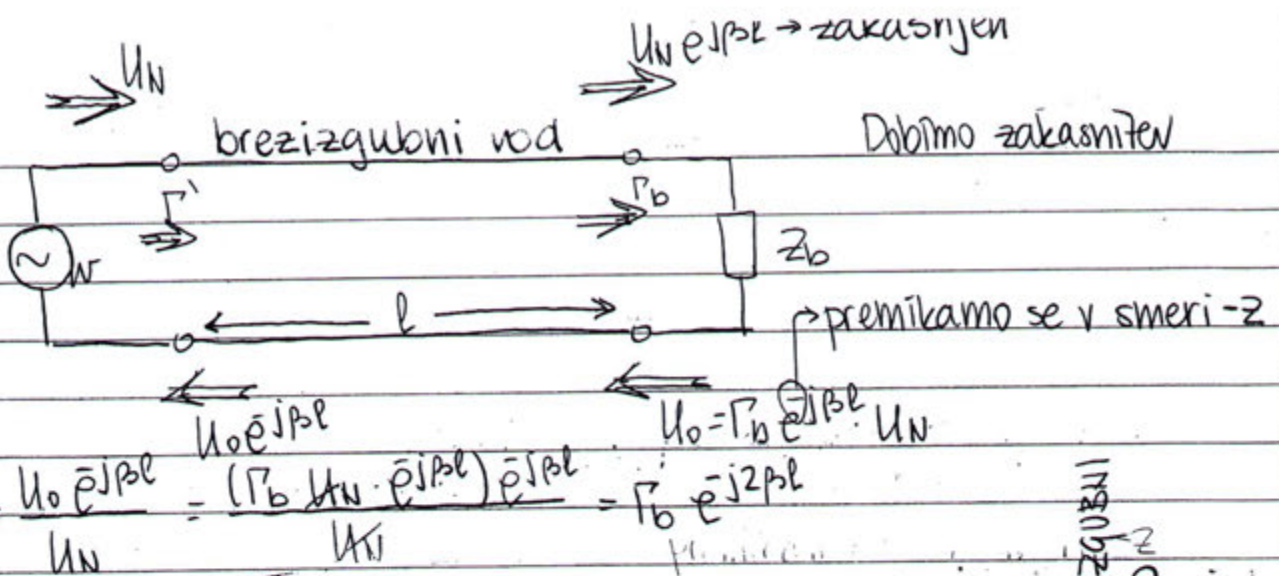
aktivno breme: $\text{Re}[Z] < 0 \implies |\Gamma| > 1$ - OJAČAN ODBOJ!

$Z_k = 50 \Omega$



za admitanco obrneš za 180°

aktivno breme

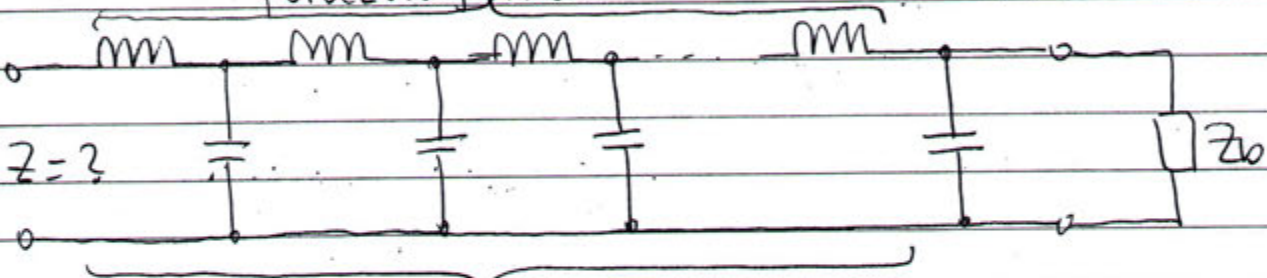


$$\Gamma' = \frac{U_0 e^{j\beta l}}{U_N} = \frac{(U_0 e^{j\beta l})}{U_N} = \frac{(\Gamma_0 U_N e^{j\beta l})}{U_N} = \Gamma_0 e^{-j2\beta l}$$

Γ' po vodu ostaja po velikosti enak, njegova faza se vrti. (Smithov diagram)

BREZIZGUBNI VOD

Porazdeljena L



porazdeljena C

$$\Gamma_0 = \frac{Z_0 - Z_k}{Z_0 + Z_k}$$

odbojnost se zasuka

$$\Gamma' = \Gamma_0 e^{j2\beta l}$$

faza se zasuka za 2x svetlobno hitrostjo in spet pretvori v impedanco

$$Z' = Z_k \frac{1 + \Gamma'}{1 - \Gamma'}$$

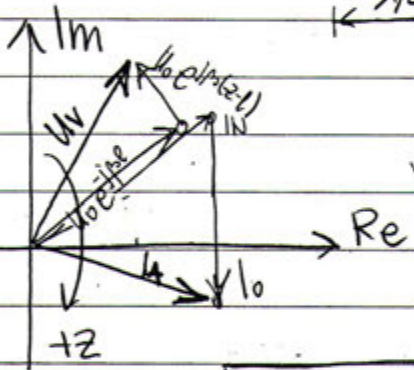
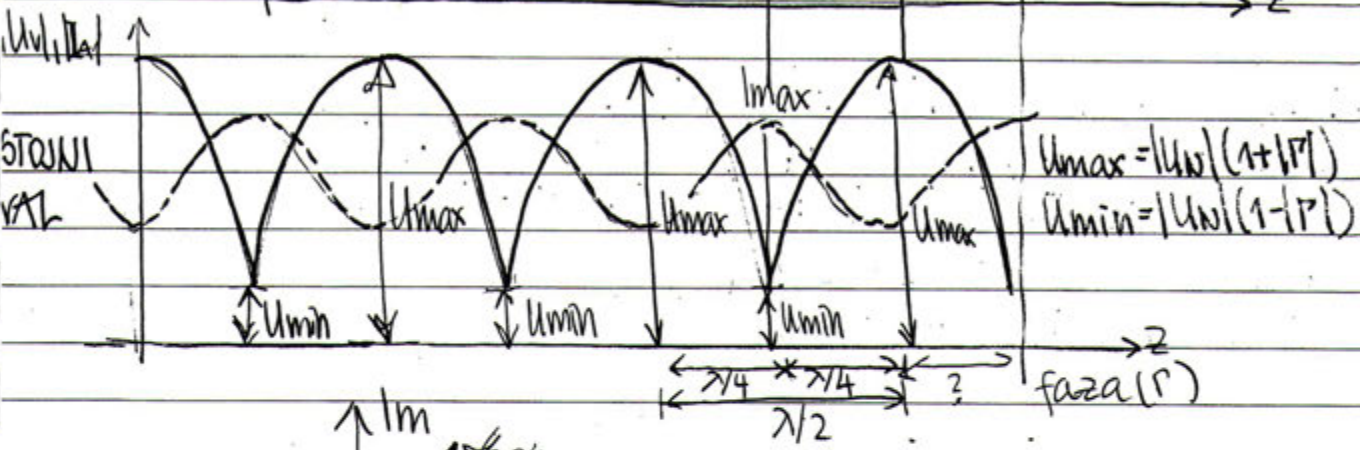
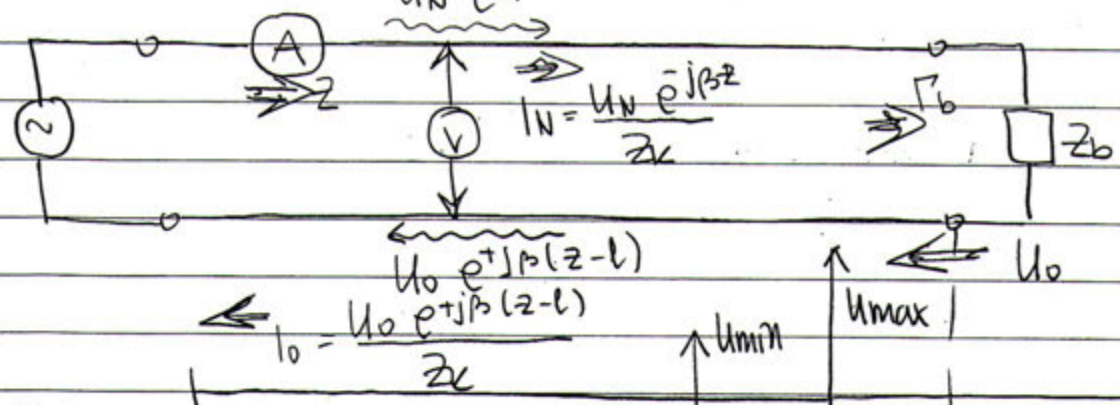
$$= Z_k \frac{1 + \Gamma_0 e^{j2\beta l}}{1 - \Gamma_0 e^{j2\beta l}} = Z_k \frac{1 + \frac{Z_0 - Z_k}{Z_0 + Z_k} e^{-2j\beta l}}{1 - \frac{Z_0 - Z_k}{Z_0 + Z_k} e^{-2j\beta l}}$$

$$Z' = Z_k \frac{Z_0 e^{j\beta l} + Z_k e^{j\beta l} + Z_0 e^{j\beta l} - Z_k e^{j\beta l}}{Z_0 e^{j\beta l} + Z_k e^{j\beta l} - Z_0 e^{-j\beta l} + Z_k e^{-j\beta l}} =$$

$$= Z_k \frac{2Z_0 \cos(\beta l) + 2jZ_k \sin(\beta l)}{2jZ_0 \sin(\beta l) + 2Z_k \cos(\beta l)}$$

$$Z' = Z_k \frac{Z_0 \cos(\beta l) + jZ_k \sin(\beta l)}{Z_k \sin(\beta l) + Z_0 \cos(\beta l)} = Z_k \frac{Z_0 + jZ_k \tan(\beta l)}{Z_k + jZ_0 \tan(\beta l)}$$

STOJNI VAL



minimumi in maximumi so vedno na istem mestu tega voda

razmerje stojnega vala:
$$\rho = \frac{U_{max}}{U_{min}} = \frac{1+|\Gamma|}{1-|\Gamma|} = \frac{I_{max}}{I_{min}}$$

valovitost:

$1 \leq \rho \leq \infty$ stojni val toka ima enako razmerje kot stojni val napetosti

$(1-|\Gamma|)\rho = 1+|\Gamma|$

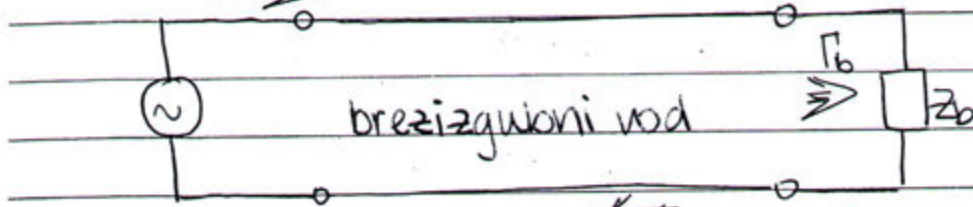
$(\rho-1) = |\Gamma|(\rho+1) \Rightarrow |\Gamma| = \frac{\rho-1}{\rho+1}$ samo velikost $|\Gamma|$ brez faze

aktivno breme:

$|\Gamma| > 1 \Rightarrow \rho = \frac{|\Gamma|+1}{|\Gamma|-1} \Rightarrow |\Gamma| = \frac{\rho+1}{\rho-1}$

Moč:

$$P_N = \frac{1}{2} U_N I_N^* = \frac{|U_N|^2}{2 Z_k}$$



$$P_b = P_N - P_o = P_N (1 - |\Gamma|^2)$$

moč na bremenu

$$P_o = \frac{1}{2} U_o I_o^* = \frac{|U_o|^2}{2 Z_k} = |\Gamma|^2 P_N$$

$$\Gamma_{dB} = 10 \log \frac{P_o}{P_N} = 10 \log |\Gamma|^2$$

slabljenje odboja: $\Gamma_{dB} = 20 \log |\Gamma|$

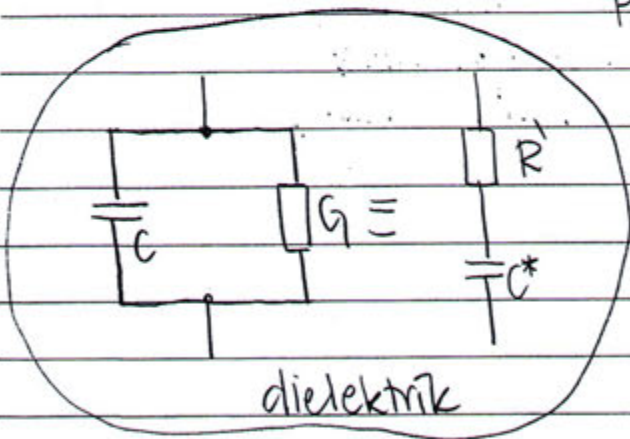
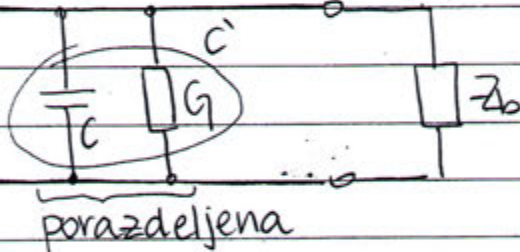
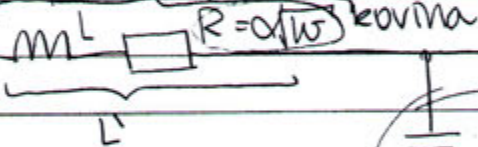
Izgube: $\alpha_{dB} = 10 \log_{10} \frac{P_b}{P_N} = 10 \log (1 - |\Gamma|^2)$

razmerje

• njegova vrednost: $\rho_{dB} = 20 \log \frac{U_{max}}{U_{min}} = 20 \log \rho$

↳ običajno se NE uporablja v dB

porazdeljena



$$L' = L + \frac{R}{j\omega}$$

$$C' = C + \frac{G}{j\omega}$$

* faza konstanta je kompleksna, notri je sedaj poleg faze tudi amplituda

majhna

$$Z_k = \sqrt{\frac{L'/l}{C'/l}} = \sqrt{\frac{L'}{C'}} = \sqrt{\frac{L + R/j\omega}{C + G/j\omega}} = \sqrt{\frac{j\omega L + R}{j\omega C + G}}$$

kompleksen; majhen imaginaren del $\frac{1}{2} \text{Im}[Z_k] \ll \text{Re}[Z_k]$

↳ običajno ne opazim

$$K = \frac{L'}{l} \cdot \frac{C'}{l} \cdot \omega = \omega \left(L + \frac{R}{j\omega} \right) / l \cdot \left(C + \frac{G}{j\omega} \right) / l = \beta - j\alpha \leftarrow \text{slabljenje}$$

kompleksno valovno število

faza konstanta *

$$u = \operatorname{Re}[U \cdot e^{j(\omega t \pm kz)}] = \operatorname{Re}[U \cdot e^{j(\omega t \pm (\beta - j\alpha)z)}]$$

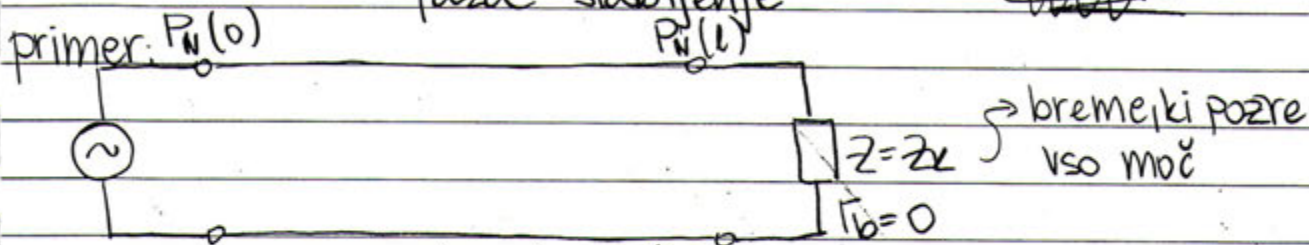
$$u_N = \operatorname{Re}[U_N e^{j\omega t} e^{-j\beta z} e^{-\alpha z}]$$

amplituda pada z razdaljo

$$u_0 = \operatorname{Re}[U_0 \cdot e^{j\omega t} e^{j\beta z} e^{+\alpha z}]$$

ce imamo izgube imamo tudi slabljenje vala

faza slabljenje



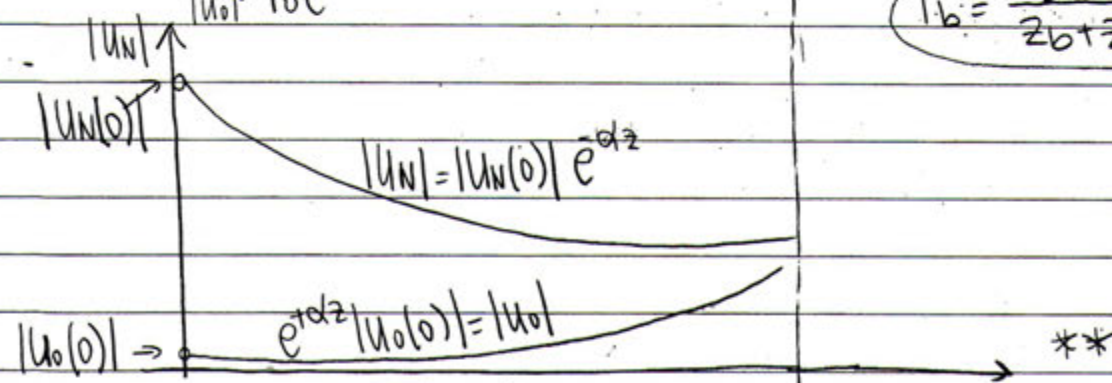
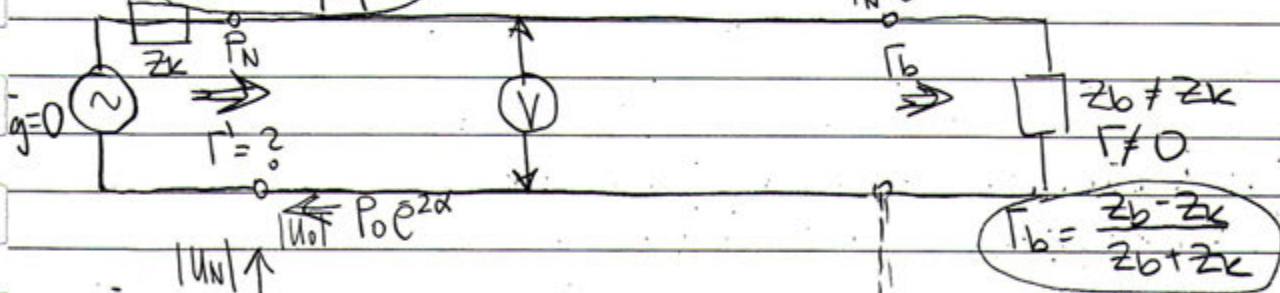
$$P_N = \operatorname{Re}\left[\frac{|U_N|^2}{2 \cdot Z_L}\right] = P_N(z)$$

\rightarrow ker amplituda napredujočega vala pada z razdaljo $\Rightarrow P_N(0) \neq P_N(z)$

slabljenje: $\frac{P_N(0)}{P_N(l)} = a = \frac{(e^{-\alpha \cdot 0})^2}{(e^{-\alpha l})^2} = e^{2\alpha l}$

$$a_{dB} = 10 \log_{10} \frac{P_N(0)}{P_N(l)} = 10 \log_{10} e^{2\alpha l} = 10 \frac{\ln e}{\ln 10} \cdot 2\alpha l \text{ [dB]}$$

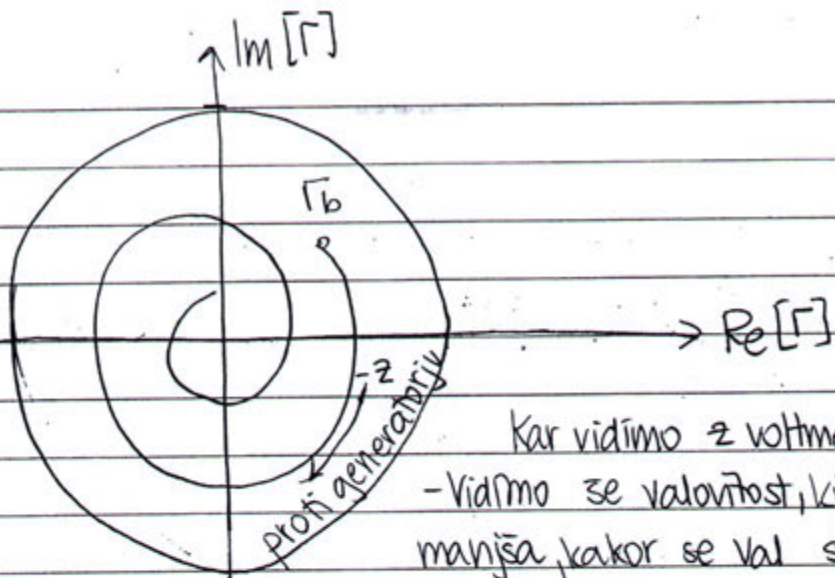
primer: $Z = Z_L \frac{1+\Gamma'}{1-\Gamma'}$



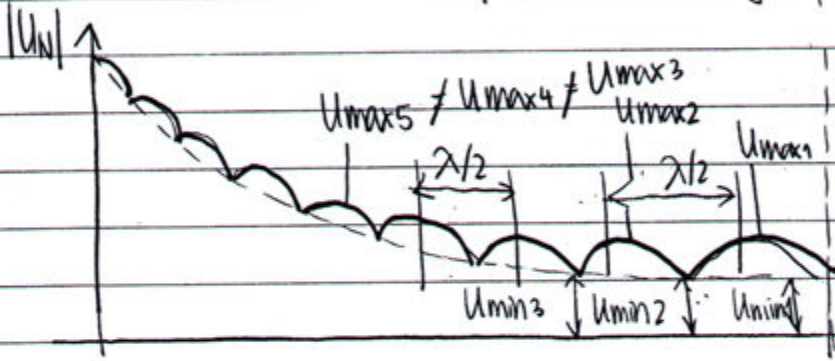
$$\Gamma' = \Gamma_b e^{-j2\beta l} e^{-2\alpha l}$$

vrti se po fazi in spreminja se mu velikost \rightarrow glej graf

$|\Gamma'| \leq |\Gamma_b|$ P na naši poti ni več konstantno velika (se manjša)



Kar vidimo z voltmetrom
- vidimo se valovitost, ki postaja manjša, kakor se val šabi



izgubni vod: ρ NI definiran

Maximumi in minimumi so različno veliki, zato ne moremo definirati razmerja

na bremenu: $P_b = (1 - |\Gamma_b|^2) P_u e^{-2\alpha l}$

- Zgled: žična palica

koaksialni kabel: $f \sim 100 \text{ MHz}$; $\alpha = \frac{1}{100} \beta$; $R \approx \frac{1}{100} \omega L$

če: $l < \lambda$.. obravnavamo kot brezizguben

če: $l > 30\lambda$.. obravnavamo izgube

- Zgled: svetlobno vlakno: $f \sim 194 \text{ THz}$; $\lambda_0 = 1,55 \mu\text{m}$

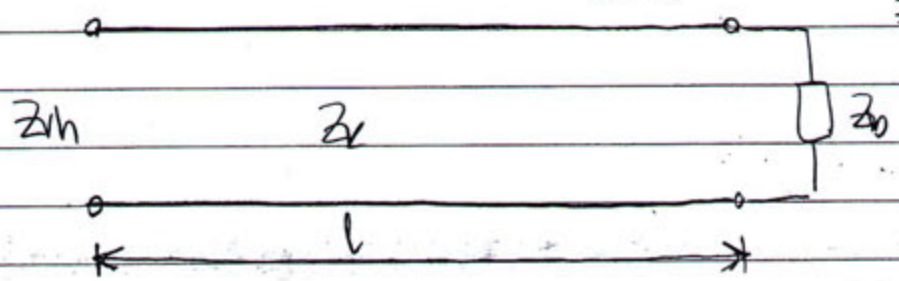
$l < 10^8 \lambda$.. brezizgubno

$l > 3 \cdot 10^8 \lambda$.. izgubni vod

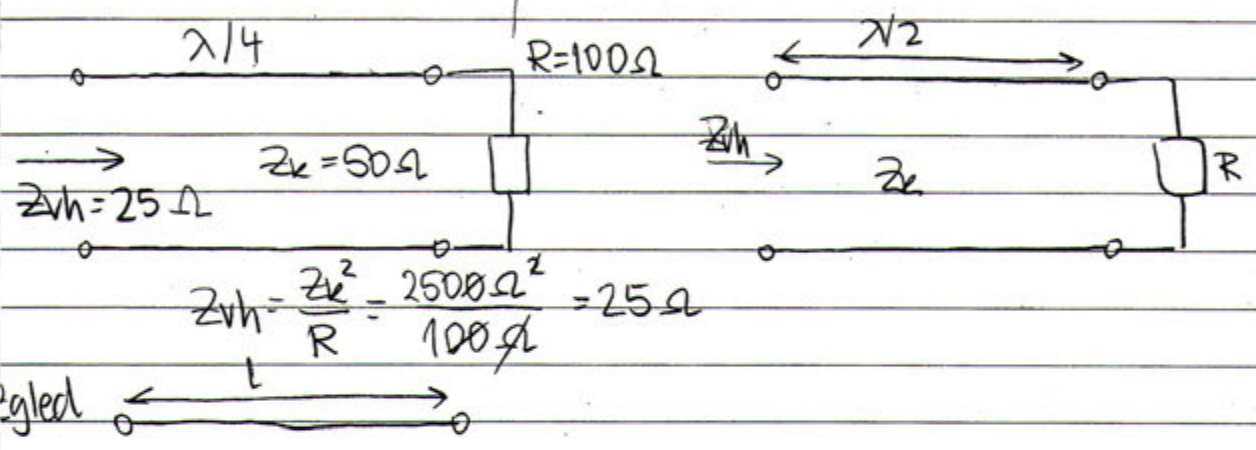
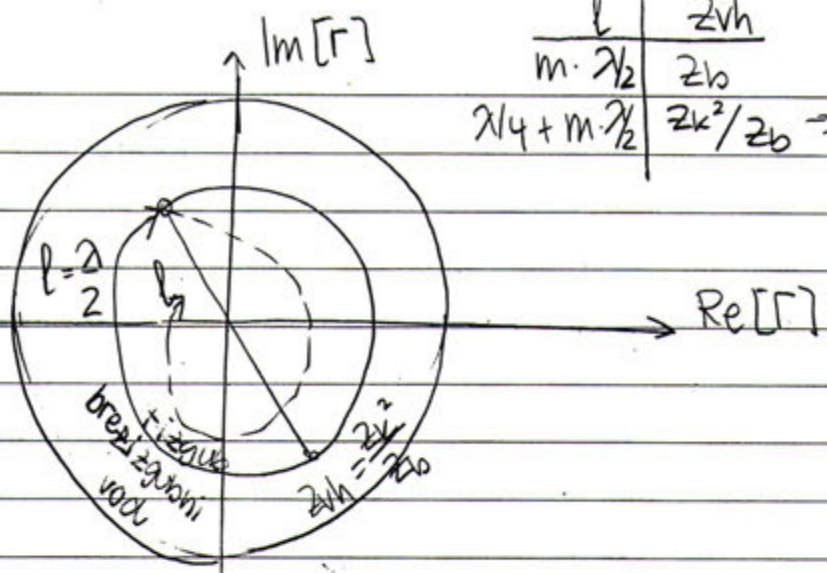
Reševanje po korakih:

$$\Gamma_b = \frac{z_b - z_0}{z_b + z_0} \Rightarrow z = z_0 \frac{1 + \Gamma_b}{1 - \Gamma_b}$$

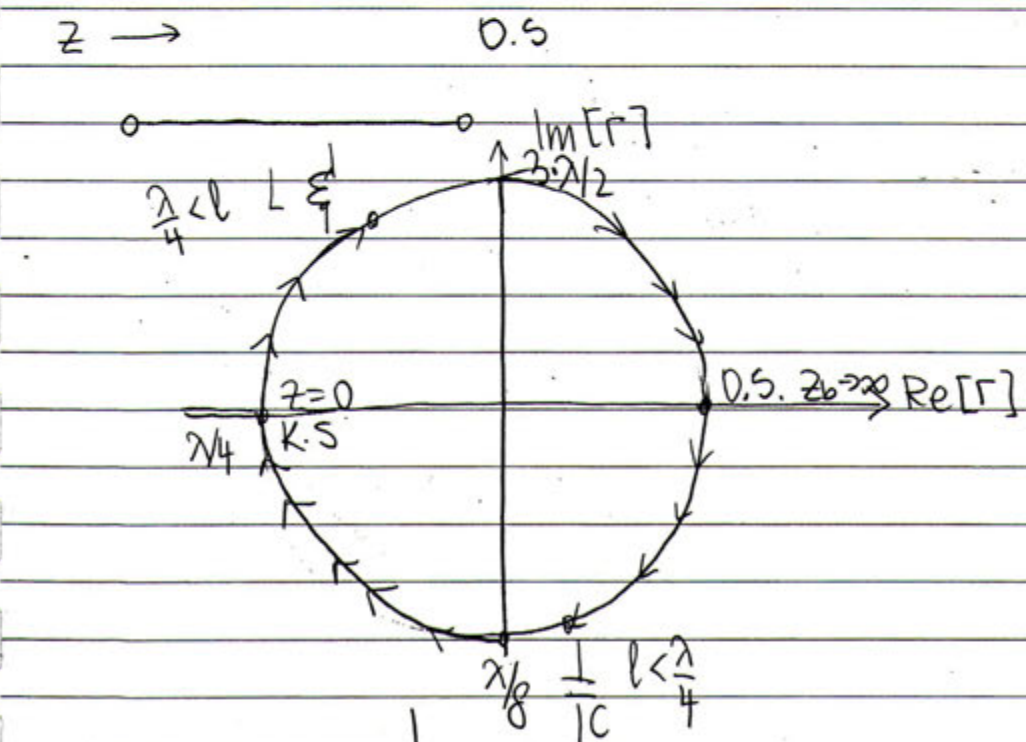
$$\Rightarrow \Gamma^l = \Gamma_b e^{j\beta l} e^{-2\alpha l}$$



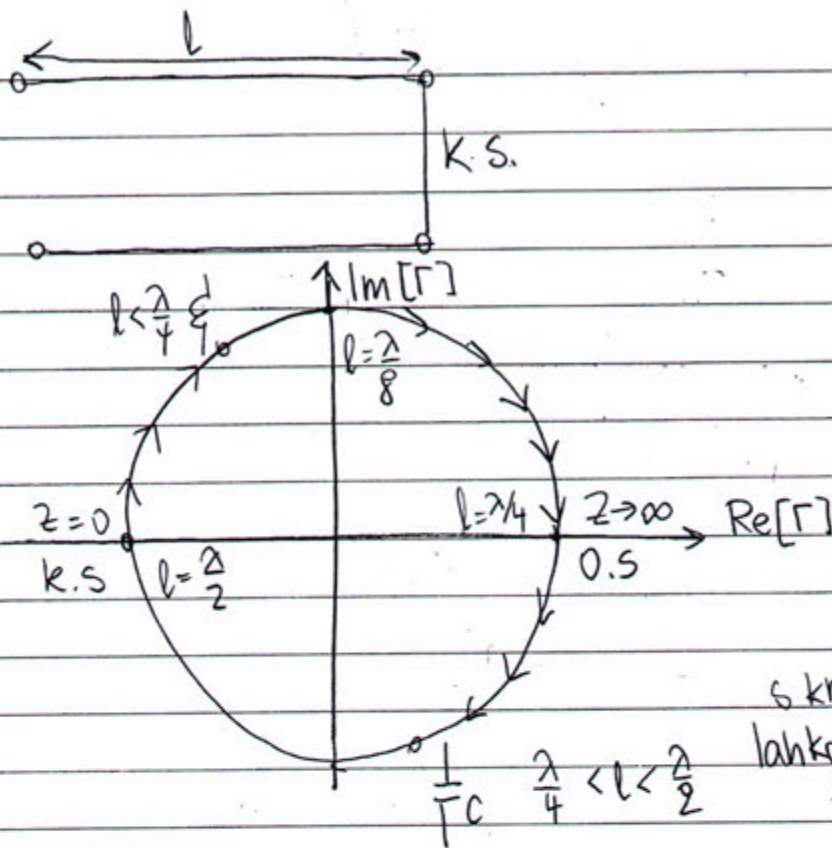
| | | |
|---------------------------------|-----|--|
| $m=1,2,3\dots$ | l | Z_{vh} |
| $m \cdot \lambda/2$ | | Z_0 |
| $\lambda/4 + m \cdot \lambda/2$ | | $Z_0^2/Z_L \rightarrow$ inverter (inverzija bremena) |



$$Z_{vh} = \frac{Z_0^2}{R} = \frac{2500 \Omega^2}{100 \Omega} = 25 \Omega$$

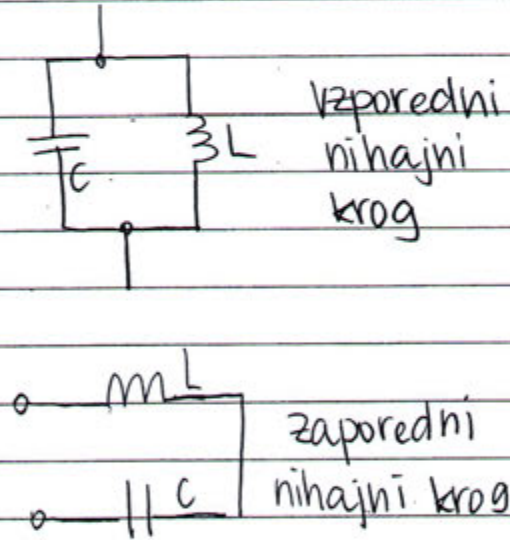
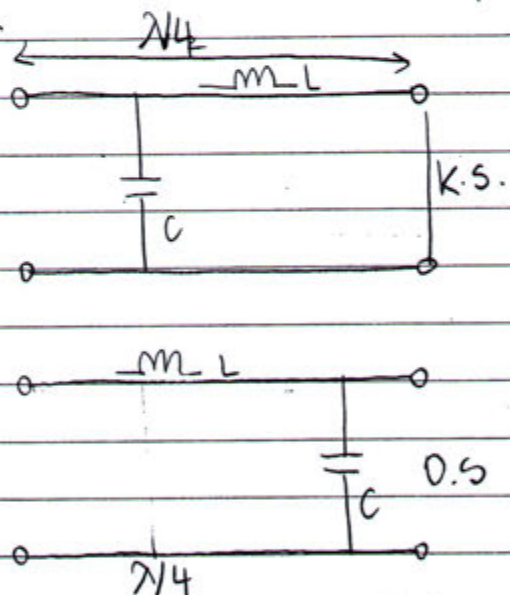


Z odprtimi sponkami lahko realiziramo kondenzator

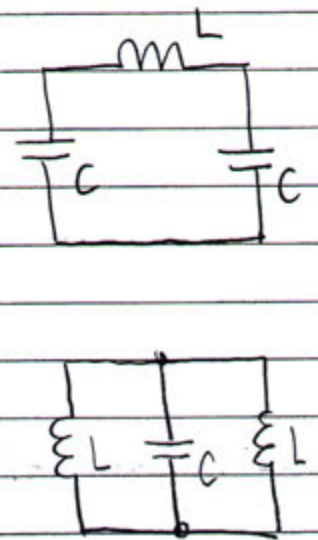
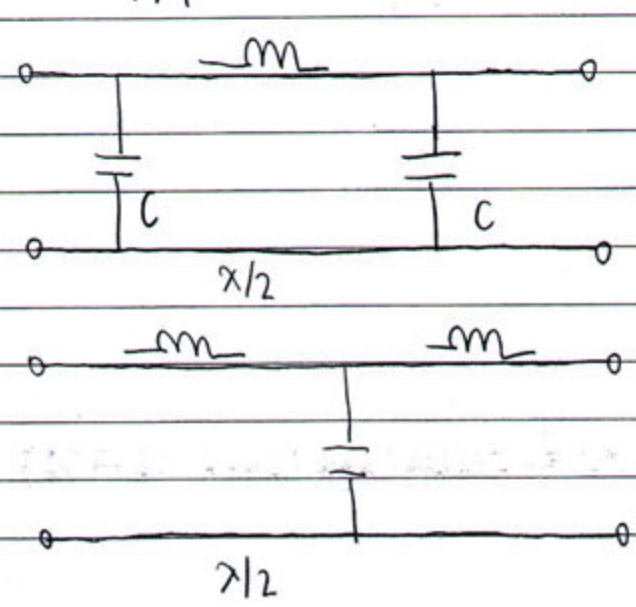


-Zgled:

četrtvalni rezonator

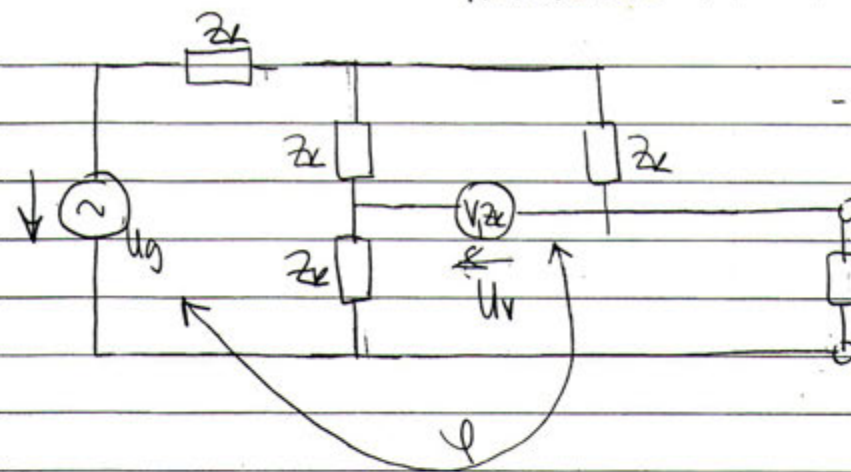


polovni rezonator



mostiček

MERJENJE V FREKVENČNEM PROSTORU



- paziti moramo kaj nam meri voltmeter
 ali meri le velikost Γ
 Z_b ($|\Gamma|$), ali tudi fazo
 vektorski v-meter

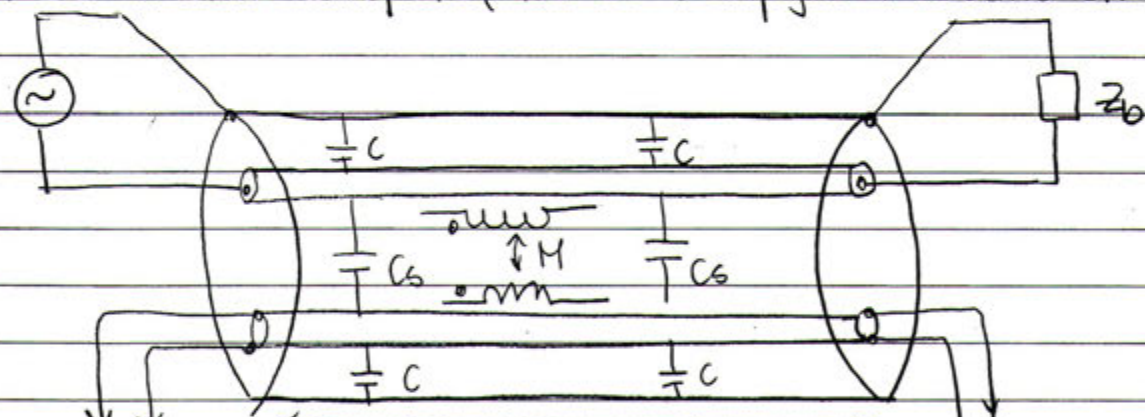
$$U_v = U_g \frac{Z_b - Z_k}{Z_b + Z_k} = \frac{U_g \Gamma}{8}$$

voltmeter: $|U_v| = \frac{|U_g|}{8} |\Gamma| \Rightarrow |\Gamma|$

enako ko enosmerno.

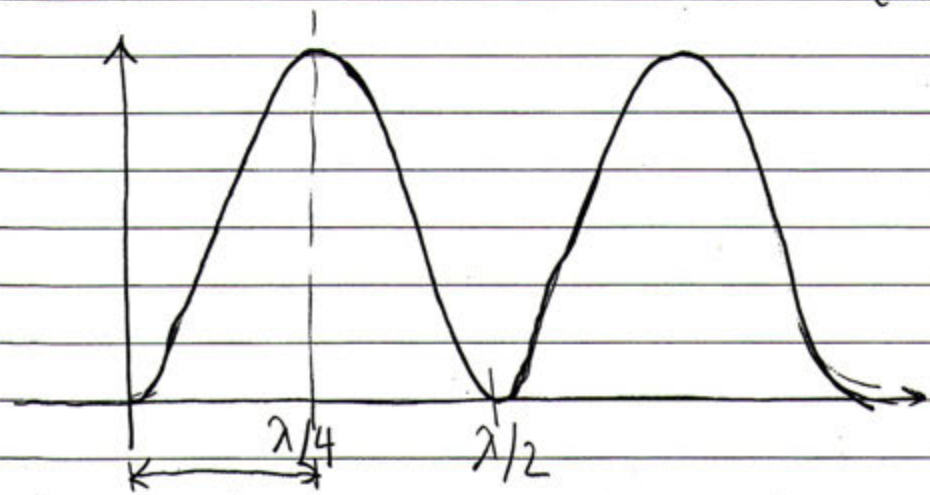
voltmeter + faza φ : $U_v = \frac{U_g}{8} \Gamma \Rightarrow \Gamma$: vektorski voltmeter
 Razmo le na fazo odbojnosti

Proti-smerni sklopnik (moč se sklapija v obratno smer)

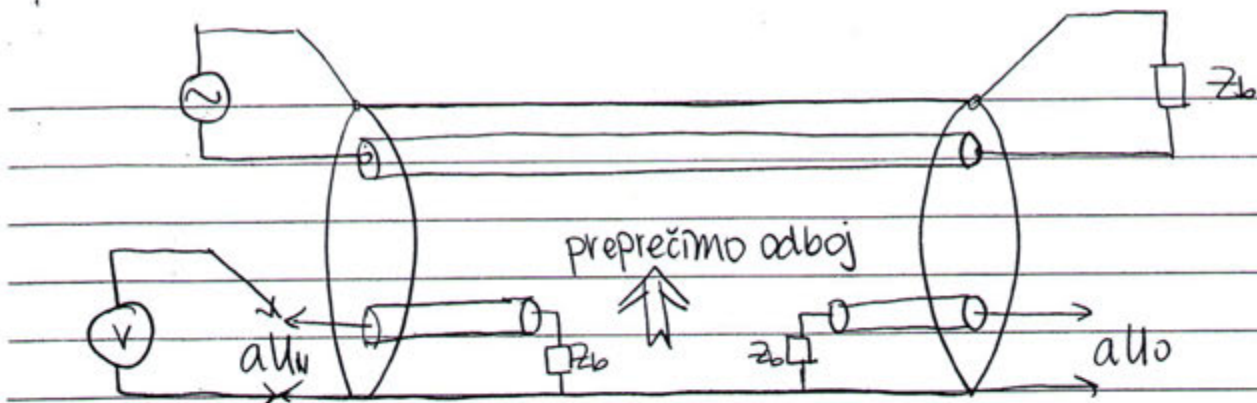


napredujoči val (vzorec)

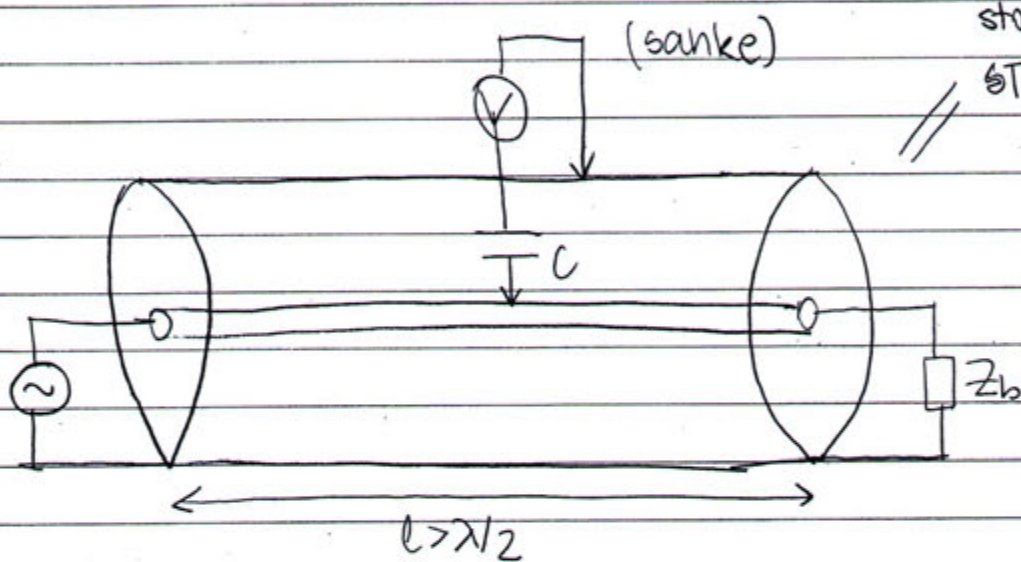
odbojni val (vzorec)



območje uporabe kratkega sklopnika



skalarni: $|P|$
vektorski Γ



za merjenje
stojnega vala
STOJNI VAL

vsaj 1x max in vsaj 1x min
za računanje $f = \frac{v_{max}}{v_{min}}$

1D.. skalarne veličine

3D.. skalarne veličine + vektorske veličine

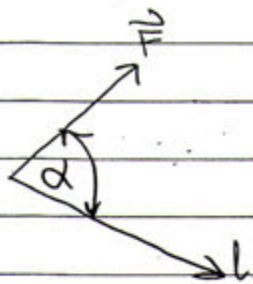
masa m .. skalar

hitrost \vec{v} .. vektor

Računanje z vektorji

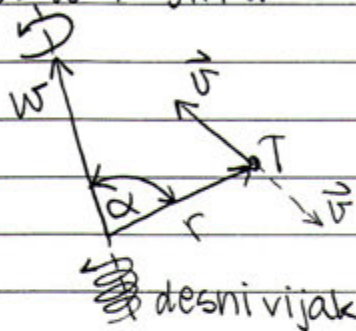
$$W = F \cdot l \cdot \cos \alpha = \vec{F} \cdot \vec{l}$$

↑ skalarni produkt



$$V = W r \cdot \sin \alpha = \vec{W} \times \vec{r}$$

↑ vektorski produkt



predznak?

PRAVILO DESNEGA VJAKA

Koordinatni sistem

• 3D (g_1, g_2, g_3)

• pravokotni

$$\vec{F} = (F_1, F_2, F_3); \vec{l} = (l_1, l_2, l_3)$$

skalarni

$$W = \vec{F} \cdot \vec{l} = F_1 l_1 + F_2 l_2 + F_3 l_3$$

$$\vec{W} = (W_1, W_2, W_3); \vec{r} = (r_1, r_2, r_3)$$

$$\vec{V} = \vec{W} \times \vec{r} = \begin{vmatrix} g_1 & g_2 & g_3 \\ W_1 & W_2 & W_3 \\ r_1 & r_2 & r_3 \end{vmatrix}$$

predznak

• desnoročni (pove predznak)

Kartezični koordinatni sistem (x, y, z)

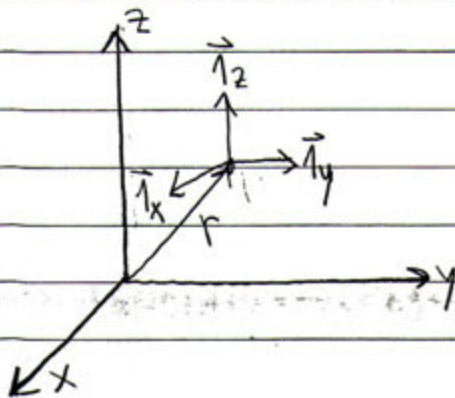
$$-\infty < x [m] < +\infty$$

$$-\infty < y [m] < +\infty$$

$$-\infty < z [m] < +\infty$$

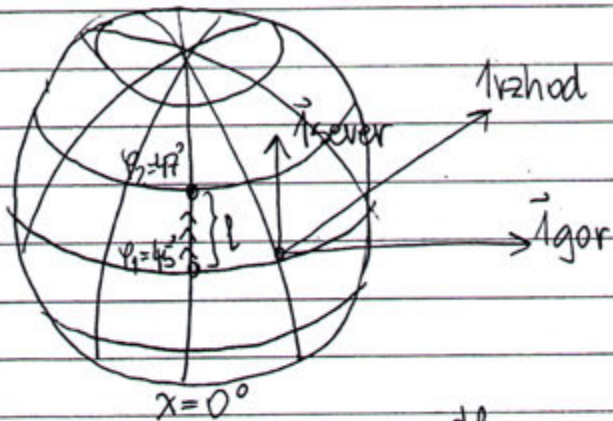
$$\vec{r}(x, y, z) = \vec{i}_x \cdot x + \vec{i}_y \cdot y + \vec{i}_z \cdot z$$

$$\text{desnoročnost: } \vec{i}_x \times \vec{i}_y = \vec{i}_z$$



$$\vec{i}_1 \times \vec{i}_2 = \vec{i}_3$$

(λ, φ, h) \rightarrow numerična višina



$$\begin{aligned} -180^\circ < \lambda [^\circ] < +180^\circ \\ -90^\circ < \varphi [^\circ] < +90^\circ \\ -6378 < h [\text{km}] < +\infty \end{aligned}$$

$$\vec{i}_{\text{vzhod}} \times \vec{i}_{\text{sever}} = \vec{i}_{\text{gor}}$$

$\lambda \quad \varphi \quad h$

\leftarrow obseg Zemlje

če $h=0$ in $\lambda = \text{konst}$: $\frac{dl}{d\varphi} = 111 \text{ km/}^\circ = \frac{40000 \text{ km}}{360^\circ} = \frac{1}{h_\varphi} h_\varphi$

$$\boxed{dl = h_\varphi \cdot d\varphi} \quad [\text{km}] dl / d\varphi [^\circ]$$

Lamé-jev koeficient

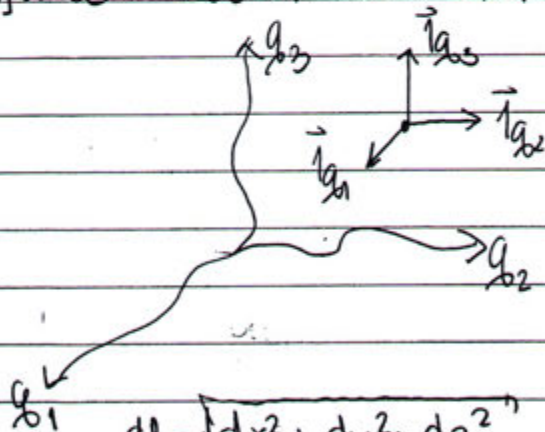
$V = 10$ litrov goriva

poraba avta = ? Koliko goriva na 100 km? $V/l = ?$

$$\frac{dV}{dl} = \frac{dV}{d\varphi} \cdot \frac{d\varphi}{dl} = \frac{dV}{d\varphi} \cdot \frac{1}{h_\varphi} \quad \leftarrow \quad \frac{10 \text{ l}}{111 \text{ km}} = \frac{10 \text{ l}}{111 \text{ km}} \cdot \frac{10}{10} = \frac{9 \text{ l}}{100 \text{ km}}$$

da bo 100 km

poljubni koordinatni sistem (q_1, q_2, q_3)



desnoročnost: $\vec{i}_{q_1} \times \vec{i}_{q_2} = \vec{i}_{q_3}$
Lamé-jevi koeficienti:

$$\begin{aligned} q_1 &\rightarrow h_1 \\ q_2 &\rightarrow h_2 \\ q_3 &\rightarrow h_3 \end{aligned}$$

$$dl = \sqrt{dx^2 + dy^2 + dz^2}$$

$$dx = \frac{\partial x}{\partial q_1} dq_1 \quad dy = \frac{\partial y}{\partial q_1} dq_1 \quad dz = \frac{\partial z}{\partial q_1} dq_1$$

pot v smeri q_1
premak v smeri q_1

$$dl = h_1 \cdot dq_1 = dq_1 \sqrt{\left(\frac{\partial x}{\partial q_1}\right)^2 + \left(\frac{\partial y}{\partial q_1}\right)^2 + \left(\frac{\partial z}{\partial q_1}\right)^2}$$

element dolžine

Kako izračunamo Lamé-jeve koeficiente?

$$h_1 = \sqrt{\left(\frac{\partial x}{\partial q_1}\right)^2 + \left(\frac{\partial y}{\partial q_1}\right)^2 + \left(\frac{\partial z}{\partial q_1}\right)^2}$$

$$h_2 = \sqrt{\left(\frac{\partial x}{\partial q_2}\right)^2 + \left(\frac{\partial y}{\partial q_2}\right)^2 + \left(\frac{\partial z}{\partial q_2}\right)^2}$$

$$h_3 = \sqrt{\left(\frac{\partial x}{\partial q_3}\right)^2 + \left(\frac{\partial y}{\partial q_3}\right)^2 + \left(\frac{\partial z}{\partial q_3}\right)^2}$$

povezava s kartezičnim koordinatnim sistemom:

$$\begin{cases} x(q_1, q_2, q_3) \\ y(q_1, q_2, q_3) \\ z(q_1, q_2, q_3) \end{cases}$$

kakšne funkcije so?

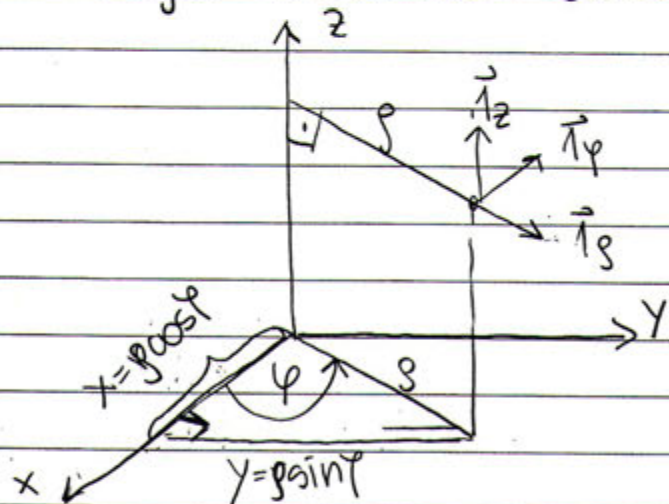
kartezični
koor. sist.

poljubni
koor. sist.

element ploskrice: $dA = dx dy = h_1 h_2 dq_1 dq_2$

element volumna: $dV = dx dy dz = h_1 h_2 h_3 dq_1 dq_2 dq_3$

Valjni koordinatni sistem (ρ, φ, z)



$$\vec{e}_\rho \times \vec{e}_\varphi = \vec{e}_z$$

$$0 \leq \rho [\text{m}] < +\infty$$

$$0 \leq \varphi [\text{rad}] < 2\pi$$

$$-\infty < z [\text{m}] < +\infty$$

Povezave med koordinatami:

$$\rho = \sqrt{x^2 + y^2}$$

$$\varphi = \arctan(y/x) \text{ (KVADRANT?)}$$

$$z = z$$

obratna smer

$$x = \rho \cos \varphi$$

$$y = \rho \sin \varphi$$

$$z = z$$

Lamé-jevi koeficienti:

$$h_\rho = \sqrt{\left(\frac{\partial x}{\partial \rho}\right)^2 + \left(\frac{\partial y}{\partial \rho}\right)^2 + \left(\frac{\partial z}{\partial \rho}\right)^2} = \sqrt{\cos^2 \varphi + \sin^2 \varphi + 0} = 1 \text{ [neimenovano]}$$

$$\underline{h_\rho} = \sqrt{\left(\frac{\partial x}{\partial \rho}\right)^2 + \left(\frac{\partial y}{\partial \rho}\right)^2 + \left(\frac{\partial z}{\partial \rho}\right)^2} = \sqrt{\rho^2 \sin^2 \varphi + \rho^2 \cos^2 \varphi + 0} = \underline{\rho} \text{ [m/rad]}$$

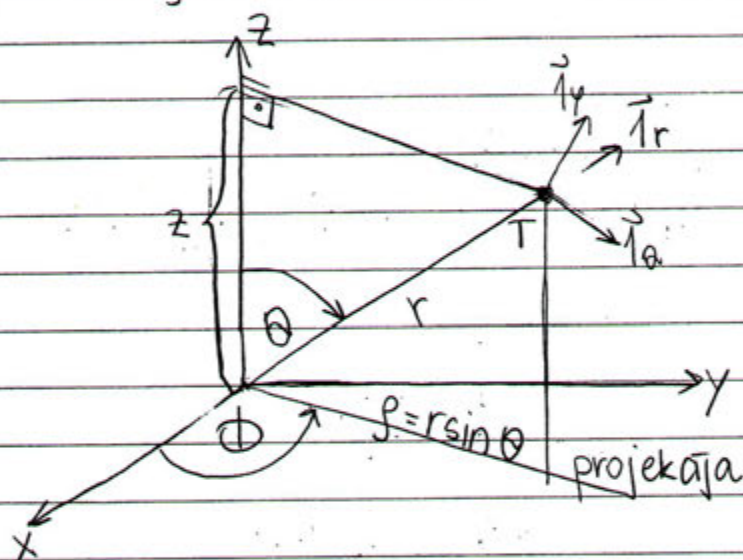
$$\underline{h_z} = \sqrt{\left(\frac{\partial x}{\partial z}\right)^2 + \left(\frac{\partial y}{\partial z}\right)^2 + \left(\frac{\partial z}{\partial z}\right)^2} = \sqrt{0+0+1} = \underline{1} \text{ [neimenovano]}$$

smer \vec{i}_ρ : $dl = d\rho$ [m]

smer \vec{i}_φ : $dl = \rho d\varphi$ [m]

smer \vec{i}_z : $dl = dz$ [m]

Krogelni koordinatni sistem (r, θ, ϕ)



$$\vec{i}_r \times \vec{i}_\theta = \vec{i}_\varphi$$

severni tečaj $0 \leq r \text{ [m]} < +\infty$
 $0 \leq \theta \text{ [rad]} \leq \pi$ južni tečaj
 $0 \leq \phi \text{ [rad]} \leq 2\pi$

Povezave med koordinatami:

$$r = \sqrt{x^2 + y^2 + z^2}$$

$$\theta = \arccos(z/r) \leftarrow \text{SINGULARNOST?}$$

$$\phi = \arctan(y/x) \leftarrow \text{(KVADRANT?)}$$

obratno

$$x = r \sin \theta \cos \phi$$

$$y = r \sin \theta \sin \phi$$

$$z = r \cos \theta$$

Lamë-jevi koeficienti:

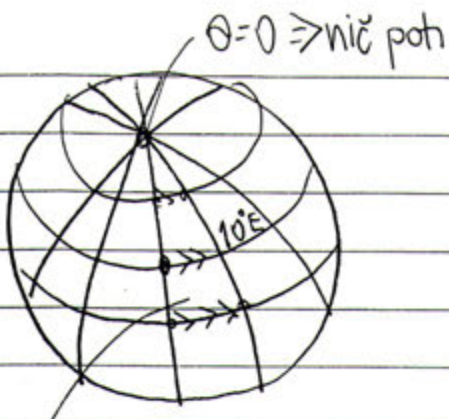
$$\underline{h_r} = \sqrt{\left(\frac{\partial x}{\partial r}\right)^2 + \left(\frac{\partial y}{\partial r}\right)^2 + \left(\frac{\partial z}{\partial r}\right)^2} = \sqrt{\sin^2 \theta \cos^2 \phi + \sin^2 \theta \sin^2 \phi + \cos^2 \theta} = \underline{1} \text{ [neim]}$$

$$\underline{h_\theta} = \sqrt{r^2 \cos^2 \theta \cos^2 \phi + r^2 \cos^2 \theta \sin^2 \phi + r^2 \sin^2 \theta} = \underline{r} \text{ [m/rad]}$$

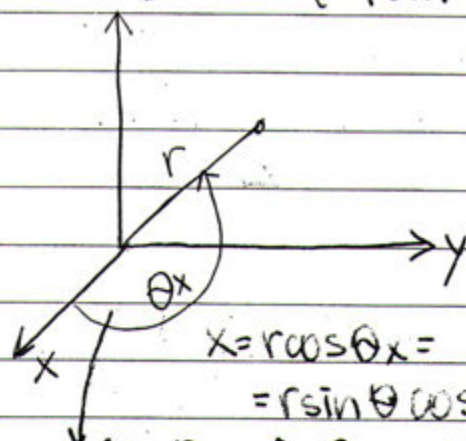
$$\underline{h_\phi} = \sqrt{r^2 \sin^2 \theta \sin^2 \phi + r^2 \sin^2 \theta \cos^2 \phi + 0} = \underline{r \sin \theta} \text{ [m/rad]}$$

Preobrazba ...
Koordinatni sistem

(r, θ, ϕ)



najdaljša pot na Ekvatorju



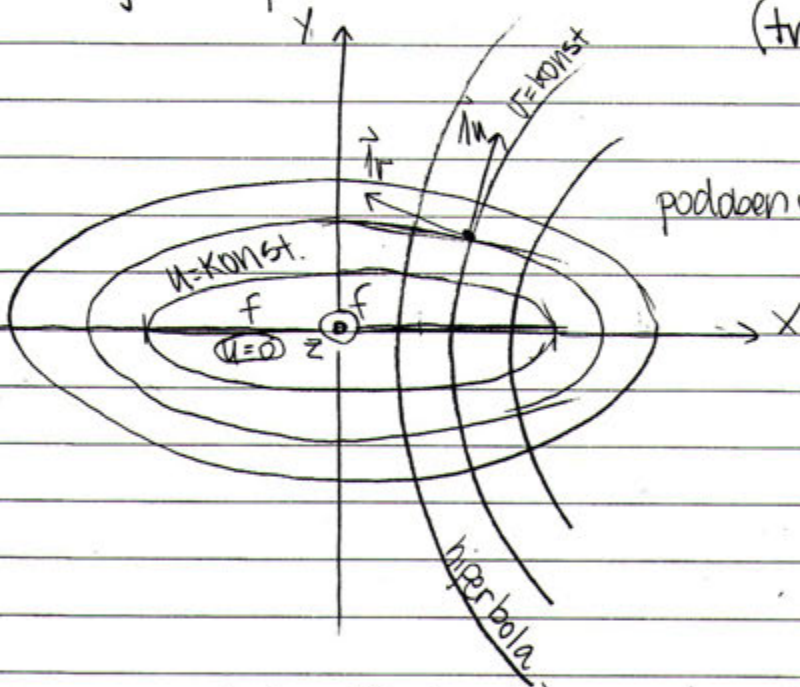
$$x = r \cos \theta_x =$$

$$= r \sin \theta \cos \phi$$

$$\cos \theta_x = \sin \theta \cos \phi$$

$$\sin \theta_x = \sqrt{1 - \sin^2 \theta \cos^2 \phi}$$

Valjni eliptični koordinatni sistem (u, v, z)
(trakovi)



$$0 < u [\text{neim}] < +\infty$$

podoben ϕ $0 \leq v [\text{rad}] \leq 2\pi$

$$-\infty \leq z [\text{m}] < +\infty$$

Povezave med koordinatami:

$$x = f \cosh u \cos v$$

$$y = f \sinh u \cdot \sin v$$

$$z = z$$

primerjava z valjnim k.s.

$$x = \rho \cos \varphi$$

$$y = \rho \sin \varphi$$

$$z = z$$

$$\cosh^2 u = \sinh^2 u + 1$$

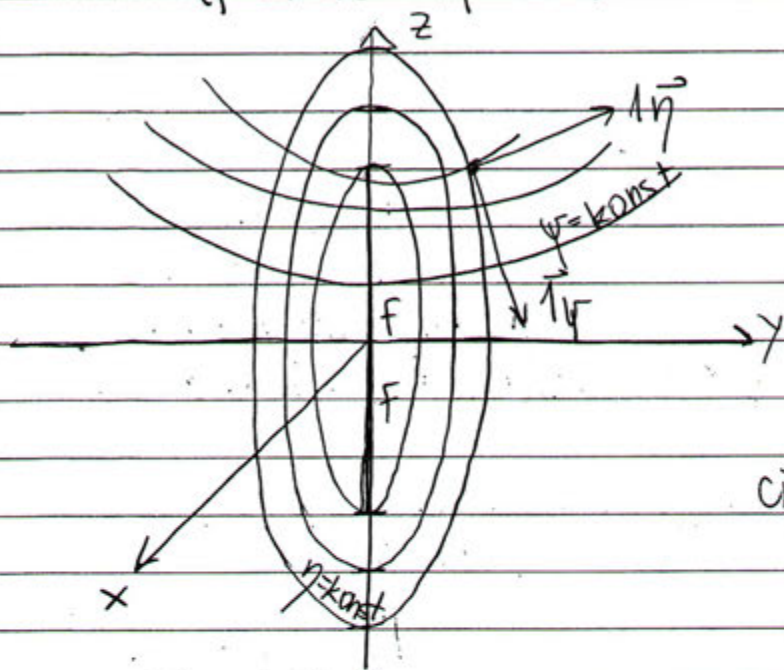
Lamé-jevi koeficienti:

$$h_u = \sqrt{f^2 \sinh^2 u \cos^2 v + f^2 \cosh^2 u \sin^2 v + 0} = f \sqrt{\sinh^2 u + \sin^2 v} \quad [\text{m}]$$

$$h_v = \sqrt{f^2 \cosh^2 u \sin^2 v + f^2 \sinh^2 u \cos^2 v + 0} = f \sqrt{\sinh^2 u + \sin^2 v} \quad [\text{m/rad}]$$

$$h_z = \sqrt{0 + 0 + 1} = 1 \quad [\text{neim}]$$

Palica \Rightarrow cigara (η, ψ, ϕ) poldolgovat elipsoid
(prolate elipsoid)



cigara \leftrightarrow krogelni
 $\eta \leftrightarrow r$
 $\psi \leftrightarrow \theta$
 $\phi = \phi$

Povezave med koordinatami:

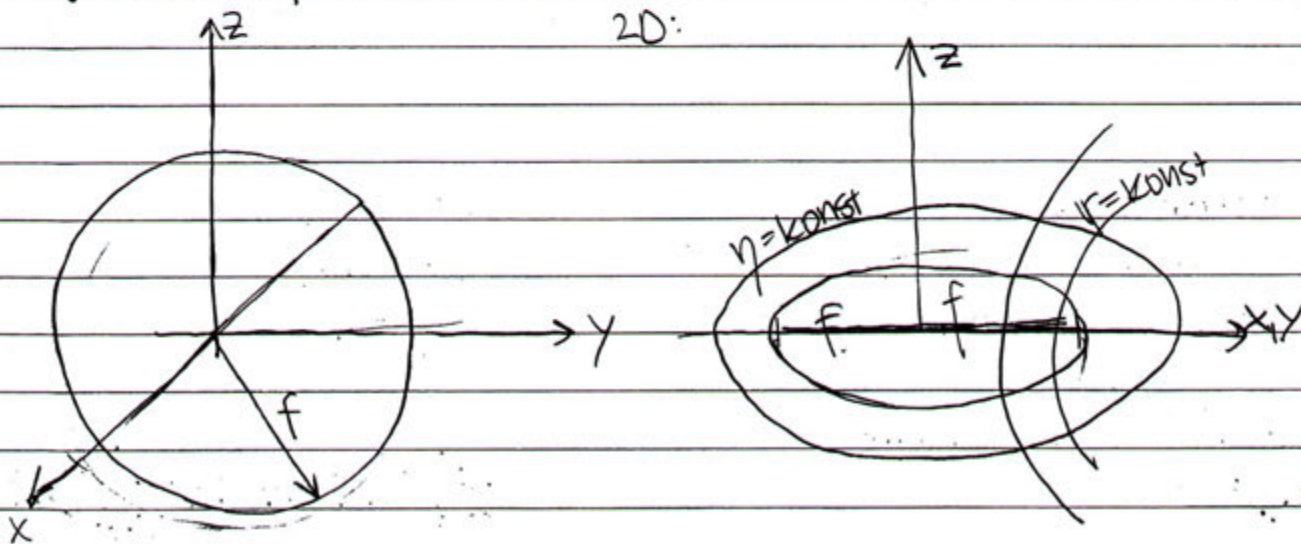
$$x = f \sinh \eta \cdot \sin \psi \cdot \cos \phi$$

$$y = f \sinh \eta \cdot \sin \psi \cdot \sin \phi$$

$$z = f \cosh \eta \cdot \cos \psi$$

Disk \rightarrow polpet (η, ψ, ϕ)
(oblate elipsoid)

2D:



Povezave med koordinatami:

$$x = f \cdot \cosh \eta \cdot \sin \psi \cdot \cos \varphi$$

$$y = f \cdot \cosh \eta \cdot \sin \psi \cdot \sin \varphi$$

$$z = f \cdot \sinh \eta \cdot \cos \psi$$

← potencial

skalarna funkcija: $V(x, y, z) = V(\vec{r})$

$$\frac{\partial V}{\partial x} \quad \frac{\partial V}{\partial y} \quad \frac{\partial V}{\partial z} \quad \dots \text{ 3 različni odvodi}$$

vektorska funkcija: $\vec{E}(x, y, z) = \vec{E}(\vec{r}) =$

$$= \hat{i}_x E_x(x, y, z) + \hat{i}_y E_y(x, y, z) + \hat{i}_z E_z(x, y, z)$$

$$\frac{\partial E_x}{\partial x} \quad \frac{\partial E_x}{\partial y} \quad \frac{\partial E_x}{\partial z} \quad \dots \quad \frac{\partial E_z}{\partial z} \quad \dots \text{ 9 različnih odvodov}$$

DEF: $\vec{E} = -\hat{i}_s \frac{\partial V}{\partial s}$ smer kamor se potencial največ spreminja

↑
max

smerni odvod

↓
gradient

$$\vec{E} = -\text{grad } V(\vec{r}) = -\left[\hat{i}_x \frac{\partial V}{\partial x} + \hat{i}_y \frac{\partial V}{\partial y} + \hat{i}_z \frac{\partial V}{\partial z} \right] = -\vec{\nabla} V(\vec{r})$$

\downarrow [V/m] \downarrow [m⁻¹] \downarrow [V]

nabla: → gradient

$$\vec{\nabla} = \hat{i}_x \frac{\partial}{\partial x} + \hat{i}_y \frac{\partial}{\partial y} + \hat{i}_z \frac{\partial}{\partial z}$$

[m⁻¹]

samo kartezični

koordinatni sistem

kjer $h_x = h_y = h_z = 1$

poljubni koordinatni sistem

(g_1, g_2, g_3)

OSTALI! UPOŠTEVAJ SE

LANÉ-JEVE KOEFICIENTE

$$-\vec{E} = -\text{grad } V = \vec{\nabla} V = \hat{i}_{g_1} \frac{\partial V}{\partial g_1} + \hat{i}_{g_2} \frac{\partial V}{\partial g_2} + \hat{i}_{g_3} \frac{\partial V}{\partial g_3}$$

→
glej naprej

$$\text{grad } V = \vec{e}_1 \left(\frac{1}{h_1} \frac{\partial V}{\partial q_1} \right) + \vec{e}_2 \frac{1}{h_2} \frac{\partial V}{\partial q_2} + \vec{e}_3 \frac{1}{h_3} \frac{\partial V}{\partial q_3}$$

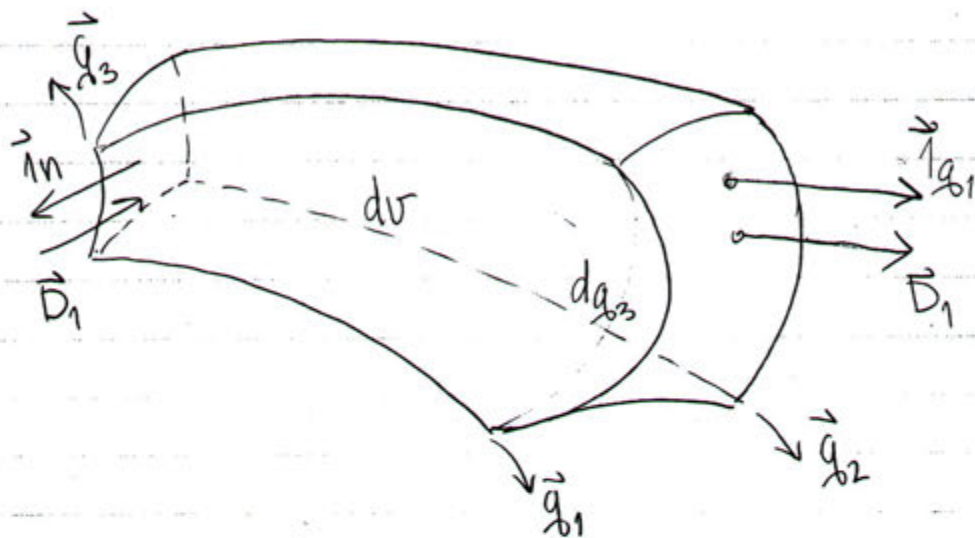
→ ravninski koordinatni sistem $(x, y, z) \Rightarrow h_x = 1, h_y = 1, h_z = 1$

$$\text{grad } V(x, y, z) = \vec{e}_x \frac{\partial V}{\partial x} + \vec{e}_y \frac{1}{1} \frac{\partial V}{\partial y} + \vec{e}_z \frac{\partial V}{\partial z} \quad [V/m]$$

→ sferični koordinatni sistem $(r, \theta, \phi) \Rightarrow h_r = 1, h_\theta = r, h_\phi = r \sin \theta$

$$\text{grad } V(r, \theta, \phi) = \vec{e}_r \frac{\partial V}{\partial r} + \vec{e}_\theta \frac{1}{r} \frac{\partial V}{\partial \theta} + \vec{e}_\phi \frac{1}{r \sin \theta} \frac{\partial V}{\partial \phi}$$

kocka v krivocrtnem



$$dv = h_1 h_2 h_3 dq_1 dq_2 dq_3$$

$$dA = h_2 h_3 dq_2 dq_3$$

$h_1(\vec{r}), h_2(\vec{r}), h_3(\vec{r})$... lahko se odvajajo

$$\rho = \frac{1}{h_1 h_2 h_3} \left[\frac{\partial (h_2 h_3 D_1)}{\partial q_1} + \frac{\partial (h_1 h_3 D_2)}{\partial q_2} + \frac{\partial (h_1 h_2 D_3)}{\partial q_3} \right]$$

IZVORNOST V KRIVOCRTNEM SISTEMU

valjni koordinatni sistem (ρ, φ, z) :

$$h_\rho = 1, h_\varphi = \rho, h_z = 1$$

$$\vec{D} = \frac{1}{\rho} \left[\frac{\partial}{\partial \rho} (\rho D_\rho) + \frac{\partial}{\partial \varphi} D_\varphi + \frac{\partial}{\partial z} (\rho D_z) \right]$$

$$\text{div } \vec{D} = \frac{\partial D_\rho}{\partial \rho} + \frac{D_\rho}{\rho} + \frac{1}{\rho} \frac{\partial D_\varphi}{\partial \varphi} + \frac{\partial D_z}{\partial z}$$

$$\boxed{\text{div } \vec{D} = \frac{1}{\rho} \frac{\partial}{\partial \rho} (\rho D_\rho) + \frac{1}{\rho} \frac{\partial D_\varphi}{\partial \varphi} + \frac{\partial D_z}{\partial z}}$$

krogelni koordinatni sistem: (r, θ, ϕ) :

$$h_r = 1, h_\theta = r, h_\phi = r \sin \theta$$

$$\operatorname{div} \vec{D} = \frac{1}{r \sin \theta} \left[\frac{\partial}{\partial r} (r^2 \sin \theta D_r) + \frac{\partial}{\partial \theta} (r \sin \theta D_\theta) + \frac{\partial}{\partial \phi} (r D_\phi) \right]$$

$$\operatorname{div} \vec{D} = \frac{1}{r^2} \frac{\partial}{\partial r} (r^2 D_r) + \frac{1}{r \sin \theta} \frac{\partial}{\partial \theta} (\sin \theta D_\theta) + \frac{1}{r \sin \theta} \frac{\partial D_\phi}{\partial \phi}$$

⇒ Gaussov izrek

$$\int_V \operatorname{div} \vec{D} \cdot dV = \oint_A \vec{D} \cdot \vec{n} \cdot dA$$



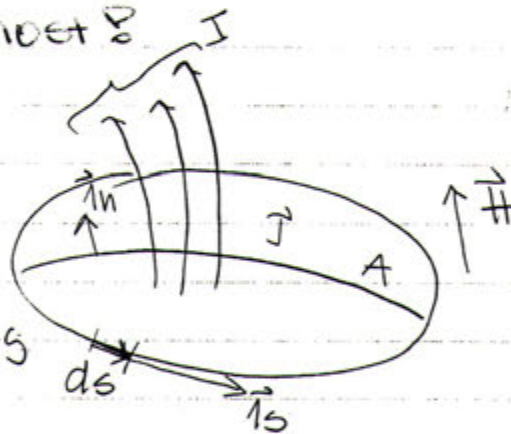
Gaussov zakon v diferencialni obliki:

$$\int_V \rho dV \Rightarrow \rho = \operatorname{div} \vec{D}$$



slabost: singularnost ρ

Amperov zakon:



$$\oint_S \vec{H} \cdot d\vec{s} = I = \int_A \vec{J} \cdot \vec{n} \cdot dA$$

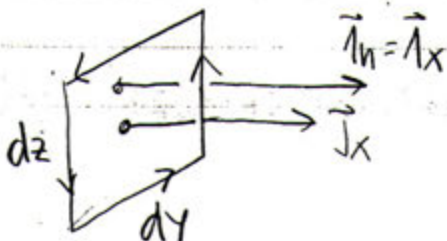
$\frac{[A \cdot m]}{[A \cdot m]} \quad [A] \quad \downarrow$
 celotni tok

$\vec{n} = \vec{i}_x, \Delta A \Rightarrow 0$ spet bi imeli radi dimenzij \Rightarrow dif. majhna oblika

$$\oint \vec{H} \cdot d\vec{s} = J_x \Delta A$$

$$J_x = \lim_{\Delta A \rightarrow 0} \frac{\oint \vec{H} \cdot d\vec{s}}{\Delta A} = \vec{i}_x \cdot \operatorname{rot} \vec{H}$$

vrtnčenje; rotor (curl)



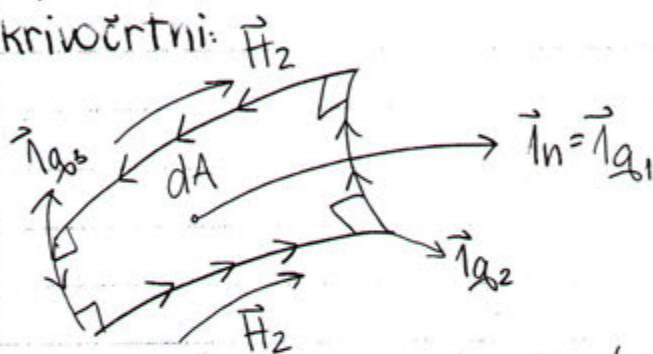
$$J_x = \frac{\partial H_z}{\partial y} - \frac{\partial H_y}{\partial z}$$

$$\vec{J} = \text{rot } \vec{H} = \begin{vmatrix} \vec{1}_x & \vec{1}_y & \vec{1}_z \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ H_x & H_y & H_z \end{vmatrix} = \vec{\nabla} \times \vec{H}$$

Stokesov izrek:

$$\oint_S \vec{H} \cdot d\vec{s} = \int_A \text{rot } \vec{H} \cdot \vec{1}_n dA$$

krivolinijski:



$$dA = h_2 h_3 dq_2 dq_3$$

$$dl_2 = h_2 dq_2$$

$$dl_3 = h_3 dq_3$$

$$J_1 = \frac{1}{h_2 h_3} \left(\frac{\partial}{\partial q_2} (h_3 H_3) - \frac{\partial}{\partial q_3} (h_2 H_2) \right)$$

$$\text{rot } \vec{H} = \vec{J} = \frac{1}{h_1 h_2 h_3} \begin{vmatrix} h_1 \vec{1}_{q_1} & h_2 \vec{1}_{q_2} & h_3 \vec{1}_{q_3} \\ \frac{\partial}{\partial q_1} & \frac{\partial}{\partial q_2} & \frac{\partial}{\partial q_3} \\ h_1 H_1 & h_2 H_2 & h_3 H_3 \end{vmatrix}$$

valjni koordinatni sistem (ρ, φ, z):

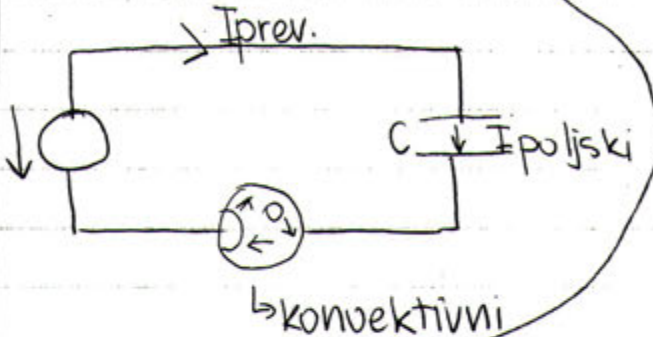
$$\text{rot } \vec{H} = \frac{1}{\rho} \begin{vmatrix} \vec{1}_\rho & \rho \vec{1}_\varphi & \vec{1}_z \\ \frac{\partial}{\partial \rho} & \frac{\partial}{\partial \varphi} & \frac{\partial}{\partial z} \\ H_\rho & \rho H_\varphi & H_z \end{vmatrix}$$

krogelni koordinatni sistem (r, θ, ϕ):

$$\text{rot } \vec{H} = \frac{1}{r \sin \theta} \begin{vmatrix} \vec{1}_r & r \vec{1}_\theta & r \sin \theta \vec{1}_\phi \\ \frac{\partial}{\partial r} & \frac{\partial}{\partial \theta} & \frac{\partial}{\partial \phi} \\ H_r & r H_\theta & r \sin \theta H_\phi \end{vmatrix}$$

$$\text{rot } \vec{H} = \vec{J} = \vec{J}_{\text{prevodniški}} + \vec{J}_{\text{konvektivni}} + \underbrace{\frac{\partial \vec{D}}{\partial t}}_{\text{poljski}}$$

celotni tok



$$\vec{J}_{\text{prevodniški}} = \gamma \cdot \vec{E}$$

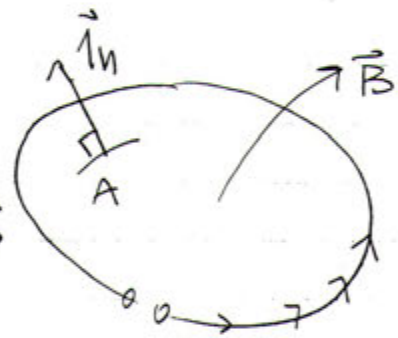
↑
prevodno sneno

Amperov zakon v diferencialni obliki:

$$\text{rot } \vec{H} = \vec{J} + \frac{\partial \vec{D}}{\partial t}$$

Faradayev zakon:

$$u_i = -\frac{d\Phi}{dt} = -\frac{d}{dt} \int_A \vec{B} \cdot \vec{n} dA = \oint_S \vec{E} \cdot d\vec{s}$$



$$\oint_S \vec{E} \cdot d\vec{s} = \int_A \text{rot } \vec{E} \cdot \vec{n} dA$$

$$u_i = \oint_S \vec{E} \cdot d\vec{s}$$

$$\text{Uporaben zgled: } \frac{d(\vec{n} \cdot A)}{dt} = 0 \quad \nabla \cdot \vec{B} = 0$$

$$\hookrightarrow \frac{d}{dt} \int_A \vec{B} \cdot \vec{n} dA = \int_A \left(\frac{d\vec{B}}{dt} \right) \cdot \vec{n} dA \quad \leftarrow \text{kadar ploskica ni funkcija časa}$$

Faradayev zakon v diferencialni obliki:

$$\text{rot } \vec{E} = -\frac{d\vec{B}}{dt}$$

MAXWELLOVE ENAČBE V DIFERENCIALNI OBLIKI:

- | | | |
|---|---|---------|
| ① | $\text{rot } \vec{H} = \vec{J} + \frac{\partial \vec{D}}{\partial t}$ | Amper |
| ② | $\text{rot } \vec{E} = -\frac{\partial \vec{B}}{\partial t}$ | Faraday |
| ③ | $\text{div } \vec{D} = \rho$ | Gauss |

$$\Delta x \rightarrow 0$$

$$\Delta A \rightarrow 0$$

$$\Delta U \rightarrow 0$$



težava: vse funkcije morajo biti $\nabla \circ$
zvezne in uveljavljive

Elektromagnetna naloga:

podatki \Rightarrow izvori: \vec{J}, ρ

$$\vec{E} = ?, \vec{H} = ?$$

ϵ, μ nista funkciji koordinat

preprosta snov: linearna, izotropna \uparrow homogena

$$\vec{B} = \mu \vec{H}, \vec{D} = \epsilon \vec{E}$$

Harmoniske relacije: $\nabla \circ$
 $\frac{\partial}{\partial t} = j\omega$

$$\textcircled{1} \text{ rot } \vec{H} = \vec{J} + \epsilon \frac{\partial \vec{E}}{\partial t} \Rightarrow \text{rot } \vec{H} = \vec{J} + j\omega \epsilon \vec{E} / \text{rot} \uparrow (\text{za } H)$$

$$\textcircled{2} \text{ rot } \vec{E} = -\mu \frac{\partial \vec{H}}{\partial t} \Rightarrow \text{rot } \vec{E} = -j\omega \mu \vec{H} / \text{rot} \uparrow (\text{za } E)$$

$$\textcircled{3} \epsilon \cdot \text{div } \vec{E} = \rho \Rightarrow \epsilon \text{div } \vec{E} = \rho$$

Velja:

$$1) \text{ div } (\text{grad } V) = \vec{\nabla} \cdot (\vec{\nabla} V) = \Delta V = \frac{\partial^2 V}{\partial x^2} + \frac{\partial^2 V}{\partial y^2} + \frac{\partial^2 V}{\partial z^2}$$

$$2) \text{ rot } (\text{grad } V) = \vec{\nabla} \times (\vec{\nabla} V) = 0 \quad \text{gradientno polje nima vrtilcev!}$$

$$3) \text{ grad } (\text{div } \vec{F}) = \vec{\nabla} (\vec{\nabla} \cdot \vec{F})$$

$$4) \text{ div } (\text{rot } \vec{F}) = \vec{\nabla} \cdot (\vec{\nabla} \times \vec{F}) = 0 \quad \text{polje vrtilcev nima izvorov!}$$

$$5) \text{ rot } (\text{rot } \vec{F}) = \vec{\nabla} \times (\vec{\nabla} \times \vec{F})$$

$$6) \rightarrow \text{grad } (\text{div } \vec{F}) - \text{rot } (\text{rot } \vec{F}) = \Delta \vec{F} \leftarrow \text{vektorski Laplace}$$

samo v kartezičnih koordinatah:

$$\Delta \vec{F} = \hat{1}_x \Delta F_x + \hat{1}_y \Delta F_y + \hat{1}_z \Delta F_z$$

$$z \textcircled{2} \quad \text{rot}(\text{rot} \vec{E}) = -j\omega\mu \text{rot} \vec{H} \stackrel{\textcircled{1}}{=} -j\omega\mu (\vec{J} + j\omega\epsilon \vec{E})$$

$$\begin{aligned} \text{rot}(\text{rot} \vec{E}) &= -j\omega\mu \vec{J} + \omega^2\mu\epsilon \vec{E} \stackrel{\textcircled{6}}{=} \text{grad}(\text{div} E) - \Delta \vec{E} \stackrel{\textcircled{3}}{=} \\ &= \text{grad}(\epsilon \rho) - \Delta \vec{E} \end{aligned}$$

? $\rightarrow \rho/\epsilon$

$$\boxed{\Delta \vec{E} + \omega^2\mu\epsilon \vec{E} = \text{grad}(\rho/\epsilon) + j\omega\mu \vec{J}} \quad \textcircled{3}$$

ni uporabna
ker ρ in \vec{J}
morata biti
vezani ρ

prostor brez izvorov: $\rho = 0, \vec{J} = 0$

$$\boxed{\Delta \vec{E} + \omega^2\mu\epsilon \vec{E} = 0}$$

valovna enačba (nehomogena)

$$\text{rot}(\text{rot} \vec{H}) = \text{rot} \vec{J} + j\omega\epsilon \text{rot} \vec{E} = \text{rot} \vec{J} + j\omega\epsilon (-j\omega\mu \vec{H})$$

\Downarrow

$$\text{grad}(\text{div} \vec{H}) = \Delta \vec{H} = \text{rot} \vec{J} + \omega^2\mu\epsilon \vec{H}$$

$\underbrace{0}_{\text{od } \textcircled{1}} \text{ od } \textcircled{1} \text{ div}(\text{rot} \vec{E}) = 0$
 $\text{div} \vec{B} = 0$

$$\boxed{\Delta \vec{H} + \omega^2\mu\epsilon \vec{H} = -\text{rot} \vec{J}} \quad \textcircled{3}$$

neuporabna ρ

prostor brez tokov: $\vec{J} = 0$

$$\boxed{\Delta \vec{H} + \omega^2\mu\epsilon \vec{H} = 0}$$

nehomogena valovna enačba

OET1:

fja treh koordinat

$$\text{Elektrostatika: } \vec{E}(\vec{r}) = -\text{grad} V(\vec{r}) \Rightarrow \text{rot} \vec{E} = 0 \Rightarrow \omega = 0 \quad \times$$

OET2:

$$\text{Magnetostatika: } \vec{H}(\vec{r}) = -\text{grad} V_m(\vec{r}) \Rightarrow \text{rot} \vec{H} = 0 \Rightarrow \omega = 0 \quad \times$$

*

\Downarrow
 $\vec{J} = 0$ ni izvora

Vektorski potencial

$$\vec{B} = \text{rot } \vec{A} = \text{rot } \vec{V}_m'$$

različno od *

$$\text{div } \vec{A} = \text{poljubna} \quad ?$$

Coulombova izbira
 $\text{div } \vec{A} = 0$

Lorentzova izbira
 $j\omega \epsilon \mu V + \text{div } \vec{A} = 0$
 $\Rightarrow \text{div } \vec{A} = -j\omega \epsilon \mu V$

$$\vec{H} = \frac{1}{\mu} \text{rot } \vec{A}$$

$$\text{rot } \vec{E} = -j\omega \mu \vec{H} = -j\omega \text{rot } \vec{A}$$

$$\text{rot } (\vec{E} + j\omega \vec{A}) = 0$$

$$\vec{E} + j\omega \vec{A} = -\text{grad } V \quad \leftarrow \begin{array}{l} \text{poljuben grad} \Rightarrow \text{ker rot grad} = 0 \\ \text{skalarni potencial} \end{array}$$

$$\vec{E} = -j\omega \vec{A} - \text{grad } V \quad \leftarrow \begin{array}{l} \text{skalarni potencial} \\ \text{div } \quad \text{što je dogovor, saj rot(grad } V) = 0 \end{array}$$

$$\vec{J}, \rho \xrightarrow{1. \text{ korak}} \vec{A}, V \xrightarrow{2. \text{ korak}} \vec{E}, \vec{H} : \text{računski postopek}$$

$$\text{rot } \vec{H} = \text{rot} \left(\frac{1}{\mu} \text{rot } \vec{A} \right) = \vec{J} + j\omega \epsilon (-j\omega \vec{A} - \text{grad } V) \quad (\vec{A}, V)$$

$$\frac{1}{\mu} \text{rot} (\text{rot } \vec{A}) = \frac{1}{\mu} (\text{grad}(\text{div } \vec{A}) - \Delta \vec{A}) = \vec{J} + \omega^2 \epsilon \vec{A} - j\omega \epsilon (\text{grad } V) / \mu$$

$$\Delta \vec{A} + \omega^2 \mu \epsilon \vec{A} = -\mu \vec{J} + \text{grad}(\text{div } \vec{A}) + j\omega \mu \epsilon \text{grad } V =$$

$$= -\mu \vec{J} + \text{grad} (j\omega \mu \epsilon V + \text{div } \vec{A})$$

valovna enačba z
nehomogenim delom

= 0; Lorentzova izbira

Valovna enačba: za vektorski potencial

$$\Delta \vec{A} + \omega^2 \mu \epsilon \vec{A} = -\mu \vec{J}$$

vektorski potencial za
Lorentzovo izbiro ga
poganjajo samo tokovi
(ne elektrine)

IZVORI: div
 vrtinci: rot

§. prostorska elektrina

③ M.E.

$$\text{div } \vec{E} = -j\omega \text{div } \vec{A} - \text{div}(\text{grad } V)$$

$$\frac{\rho}{\epsilon} = -j\omega(-j\omega\mu\epsilon V) - \Delta V = -\omega^2\mu\epsilon V - \Delta V$$

valovna enačba: za skalarni potencial

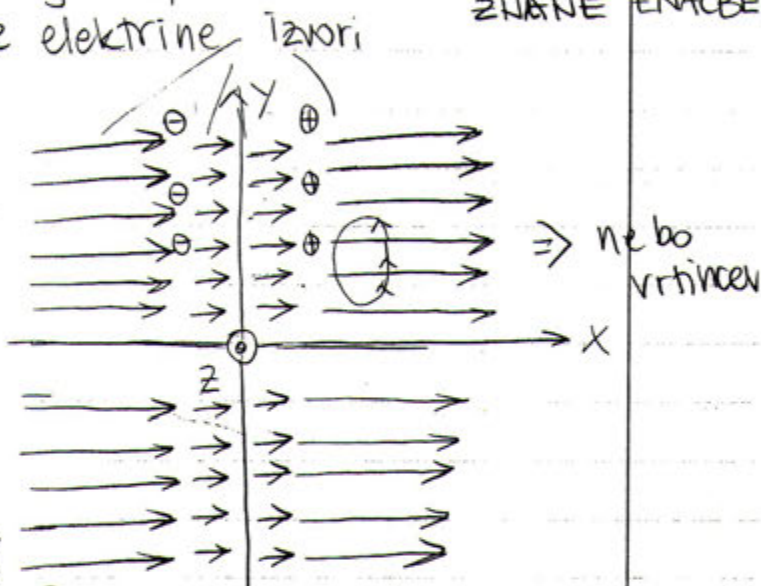
$$\Delta V + \omega^2\mu\epsilon V = -\rho/\epsilon$$

elektrostatske
 probleme rešjam
 z ugasnjeno
 frekvenco ($\omega=0$)
 \Rightarrow DOBIMO ZE
 ZNANE ENACBE

- enačbi sta povezani preko ρ in \vec{J} ;
 čim večji tok zmanjkuje elektrine izvori

- Zgled: $\vec{F} = \vec{1}_x \cdot \alpha x^2$
 izvori = ?, vrtinci = ?

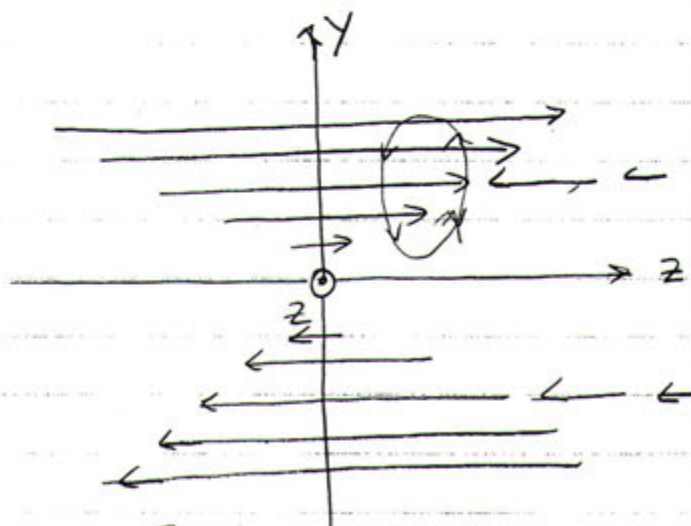
$$\text{rot } \vec{F} = \begin{vmatrix} \vec{1}_x & \vec{1}_y & \vec{1}_z \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ \alpha x^2 & 0 & 0 \end{vmatrix} = \underline{0}$$



\Rightarrow ni vrtincev!
 $\text{div } \vec{F} = \frac{\partial F_x}{\partial x} = \underline{2\alpha x}$ so izvori!

- Zgled: $\vec{F} = \vec{1}_x \alpha y$

$$\text{rot } \vec{F} = \begin{vmatrix} \vec{1}_x & \vec{1}_y & \vec{1}_z \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ \alpha y & 0 & 0 \end{vmatrix} = 0 - 0 - \vec{1}_z \alpha = \underline{-\vec{1}_z \alpha}$$

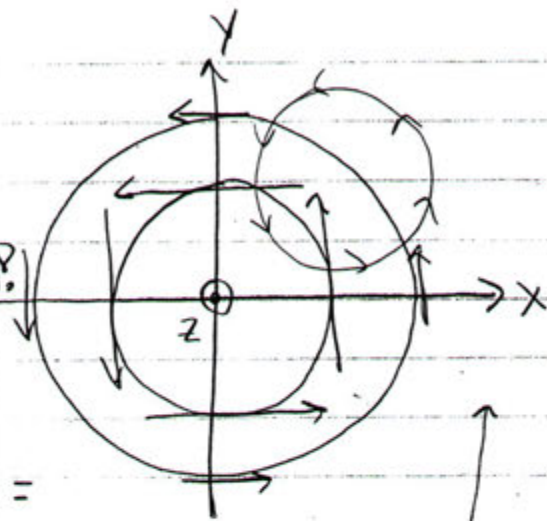


$\text{div } \vec{F} = \frac{\partial}{\partial x}(\alpha y) = \underline{0}$ ni izvorov!

- Zgled: $(\rho, \varphi, z): \vec{F} = \vec{1}_\varphi \cdot \frac{\alpha}{\rho}$

→ SINGULARNOST?

pri $\rho=0 \Rightarrow$ zato ni vrtilcev?



$$\text{rot } \vec{F} = \frac{1}{\rho} \begin{vmatrix} \vec{1}_\rho & \rho \vec{1}_\varphi & \vec{1}_z \\ \frac{\partial}{\partial \rho} & \frac{\partial}{\partial \varphi} & \frac{\partial}{\partial z} \\ 0 & \rho \frac{\alpha}{\rho} & 0 \end{vmatrix} =$$

$$= \frac{1}{\rho} \vec{1}_z \frac{\partial}{\partial \rho} \left(\rho \frac{\alpha}{\rho} \right) = \underline{0} \text{ ni vrtilcev?}$$

$$\text{div } \vec{F} = \frac{1}{\rho} \left[\frac{\partial}{\partial \varphi} \left(1 \cdot \frac{\alpha}{\rho} \right) \right] = \underline{0} \text{ ni izvorov?}$$

→ veljajo na zelo majhnem prostoru

Maxwell (diferencialno)

- ① $\text{rot } \vec{H} = \vec{J} + j\omega \vec{D}$.. Amperov
- ② $\text{rot } \vec{E} = -j\omega \vec{B}$; $\vec{B} = \mu \vec{H}$.. Faradayev
- ③ $\text{div } \vec{D} = \rho$; $\vec{D} = \epsilon \vec{E}$.. Gaussov

brez izvorov: $\rho = 0$; $\vec{J} = 0$

$$\begin{aligned} \Delta \vec{E} + \omega^2 \mu \epsilon \vec{E} &= 0 \\ \Delta \vec{H} + \omega^2 \mu \epsilon \vec{H} &= 0 \end{aligned} \quad \left. \begin{array}{l} \searrow \\ \swarrow \end{array} \right\} \text{valovni enačbi}$$

Imamo izvore: $\rho \neq 0$; $\vec{J} \neq 0$

$$\vec{B} = \text{rot } \vec{A} \quad (\vec{H} = \frac{1}{\mu} \text{rot } \vec{A})$$

$$\vec{E} = -j\omega \vec{A} - \text{grad } V$$

A. magnetni potencial

V. skalarni potencial

$$\Delta \vec{A} + \omega^2 \mu \epsilon \vec{A} = -\mu \vec{J}$$

$$\Delta V + \omega^2 \mu \epsilon V = -\rho / \epsilon$$

Zakaj so te veličine potenciali?

Energija?

DET 1: Elektrostatika

→ koliko energije prispeva elektrina

$$W_e = \frac{1}{2} \int_V \vec{E} \cdot \vec{D} \, dv = \frac{1}{2} \int_V \rho V \, dv \quad \rightarrow \text{ne pove kje se ta energija nahaja}$$

$$\omega = 0; \quad \frac{d}{dt} = 0$$

$$\Delta V = -\rho / \epsilon; \quad \vec{E} = -\text{grad } V = \epsilon \vec{E}$$

$$\vec{E} \cdot \vec{D} = (-\text{grad } V) \cdot (-\epsilon \text{ grad } V) = \epsilon \text{ grad } V \cdot \text{grad } V$$

$$\text{div} (\epsilon V \text{ grad } V) = \vec{\nabla} \cdot (\epsilon V \vec{\nabla} V) = \epsilon \vec{\nabla} V \cdot \vec{\nabla} V + \epsilon V \Delta V$$

$$\text{div} (V (-\vec{D})) = \vec{E} \cdot \vec{D} + \epsilon V (-\rho / \epsilon) = \vec{E} \cdot \vec{D} - \rho V / \epsilon \quad \int_V \rho \, dv$$

$$-\int_V \text{div} (V \vec{D}) \, dv = \int_V \vec{E} \cdot \vec{D} \, dv - \int_V \rho V \, dv = \oint_{A \rightarrow \infty} V \vec{D} \cdot \vec{n} \, dA = 0$$

Gauss
A → ∞ celoten prostor

izberem $V(\infty) = 0$

A. vektorski potencial

-Zgled:



$$V = \frac{Q}{4\pi\epsilon r}$$

$$\vec{E} = \vec{r} \frac{Q}{4\pi\epsilon r^2}$$

$$W = \frac{1}{2} \int_V \epsilon \vec{E} \cdot \vec{E} \, dv = \frac{1}{2} \int_a^\infty \int_0^\pi \int_0^{2\pi} \epsilon \left(\frac{Q}{4\pi\epsilon r^2} \right)^2 r^2 \sin\theta \, d\theta \, d\phi \, dr$$

$$= \frac{1}{2} \cdot 2\pi \cdot 2 \cdot \frac{Q^2}{16\pi^2 \epsilon} \left(0 + \frac{1}{a} \right) = \frac{Q^2}{8\pi\epsilon a}$$

$$W = \frac{1}{2} \int_V \rho \cdot V \, dv = \frac{1}{2} \sum_i Q_i \cdot V_i = \frac{1}{2} Q \cdot \frac{Q}{4\pi\epsilon a} = \frac{Q^2}{8\pi\epsilon a}$$

OET2: Magnetostatika

$$W_m = \frac{1}{2} \int_V \vec{H} \cdot \vec{B} \, dv$$

$$W = 0; \frac{d}{dt} = 0 \Rightarrow \text{rot } \vec{H} = \vec{J} + \mu_0 \vec{D}$$

$$\vec{H} \cdot \vec{B} = \vec{H} \cdot \text{rot } \vec{A}$$

$$\text{div}(\vec{A} \times \vec{H}) = \vec{\nabla} \cdot (\vec{A} \times \vec{H}) = \vec{H} \cdot (\vec{\nabla} \times \vec{A}) - \vec{A} \cdot (\vec{\nabla} \times \vec{H})$$

$$\text{div}(\vec{A} \times \vec{H}) = \vec{H} \cdot \text{rot } \vec{A} - \vec{A} \cdot \text{rot } \vec{H} = \vec{H} \cdot \vec{B} - \vec{A} \cdot \vec{J} \quad / \int_V dv$$

$$\int_V \text{div}(\vec{A} \times \vec{H}) \, dv = \oint_A (\vec{A} \times \vec{H}) \cdot \vec{n} \, dA = \int_V \vec{H} \cdot \vec{B} \, dv - \int_V \vec{J} \cdot \vec{A} \, dv$$

$A \rightarrow \infty$

izberem $A(\infty) = 0$

$$W_m = \frac{1}{2} \int_V \vec{H} \cdot \vec{B} \, dv = \frac{1}{2} \int_V \vec{J} \cdot \vec{A} \, dv$$

normirana energija za vsak tok

Elektrodinamika: konst

$$W \neq 0, \frac{d}{dt} \neq 0$$

$$\vec{v} = \frac{d\vec{r}}{dt} = 0, \frac{d\epsilon}{dt} = 0, \frac{d\mu}{dt} = 0$$

$$W = W_e + W_m = \frac{1}{2} \int_V (\vec{E} \cdot \vec{D} + \vec{H} \cdot \vec{B}) \, dv$$

$$\frac{dW}{dt} = \frac{1}{2} \int_V \left[\frac{d}{dt} (\vec{E} \cdot \vec{D} + \vec{H} \cdot \vec{B}) \right] \, dv$$

\vec{A} . potencial: vsakemu toku pripiše energijo (ker ima energija smer $\Rightarrow \vec{A}$ vektor)

$$\frac{d}{dt} (\vec{E} \cdot \vec{D}) = \frac{\partial \vec{E}}{\partial t} \cdot \vec{D} + \vec{E} \cdot \frac{\partial \vec{D}}{\partial t} = 2\vec{E} \cdot \frac{\partial \vec{D}}{\partial t}$$

$$\frac{d}{dt} (\vec{H} \cdot \vec{B}) = \frac{\partial \vec{H}}{\partial t} \cdot \vec{B} + \vec{H} \cdot \frac{\partial \vec{B}}{\partial t} = 2\vec{H} \cdot \frac{\partial \vec{B}}{\partial t}$$

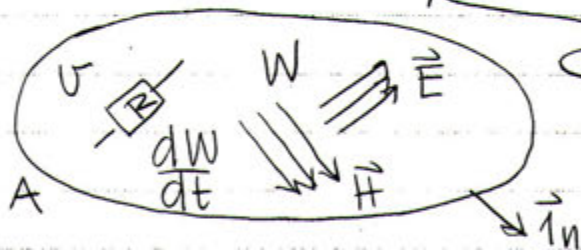
$$\Rightarrow \frac{dW}{dt} = \int_V (\vec{E} \cdot \frac{\partial \vec{D}}{\partial t} + \vec{H} \cdot \frac{\partial \vec{B}}{\partial t}) dV = \int_V (\vec{E} \cdot \text{rot} \vec{H} - \vec{E} \cdot \vec{J} - \vec{H} \cdot \text{rot} \vec{E}) dV \leftarrow \begin{matrix} \text{Maxwell. enačbe} \\ \textcircled{1} \text{ rot} \vec{H} = \vec{J} + \frac{\partial \vec{B}}{\partial t} \\ \textcircled{2} \text{ rot} \vec{E} = - \frac{\partial \vec{B}}{\partial t} \Rightarrow \frac{\partial \vec{B}}{\partial t} = - \text{rot} \vec{H} \end{matrix}$$

$$\vec{E} \cdot \text{rot} \vec{H} - \vec{H} \cdot \text{rot} \vec{E} = \vec{E} \cdot (\nabla \times \vec{H}) - \vec{H} \cdot (\nabla \times \vec{E}) = \nabla \cdot (\vec{H} \times \vec{E})$$

$$\Rightarrow \frac{dW}{dt} = \int_V [-\text{div}(\vec{E} \times \vec{H}) - \vec{E} \cdot \vec{J}] dV \leftarrow \text{Gauss} \textcircled{1}$$

$$\frac{dW}{dt} = - \oint_A (\vec{E} \times \vec{H}) \cdot \vec{n} dA - \int_V \vec{E} \cdot \vec{J} dV \quad \text{Poynting-ov izrek}$$

energija, ki potuje P, ki se troši na upor



Sprememba energije po času je enaka moči, ki se troši na upor in energiji, ki potuje

$$\frac{dW}{dt} = - \oint_A (\vec{E} \times \vec{H}) \cdot \vec{n} dA - \int_V \vec{E} \cdot \vec{J} dV$$

potujoča energija
smer: ven iz V

Poyntingov vektor (gostota moči!) $\vec{S} = \vec{E} \times \vec{H}$

↳ pove kam potuje energija

$$\left[\frac{V}{m} \right] \cdot \left[\frac{A}{m} \right] = \left[\frac{W}{m^2} \right]$$

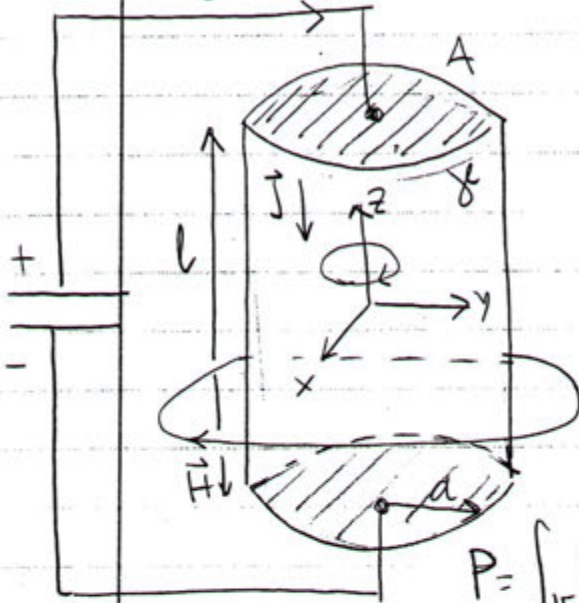
\vec{E} \vec{H}

$$VA = W$$

Zgled:



-Zgled: I (ρ, γ, z)



$$\vec{J} = -\vec{1}_z \frac{I}{A} = \gamma \vec{E}$$

$$\vec{E} = -\vec{1}_z \frac{I}{\gamma A}$$

$$U = |\vec{E}| \cdot l = \frac{I l}{\gamma A}$$

$$P = U \cdot I = \frac{I^2 l}{\gamma A} = I^2 \left(\frac{l}{\gamma A} \right) = I^2 R$$

$$P = \int_V \vec{E} \cdot \vec{J} dV = \int_l \int_A \frac{I^2}{\gamma A} dA dl = \frac{I^2 l}{\gamma A}$$

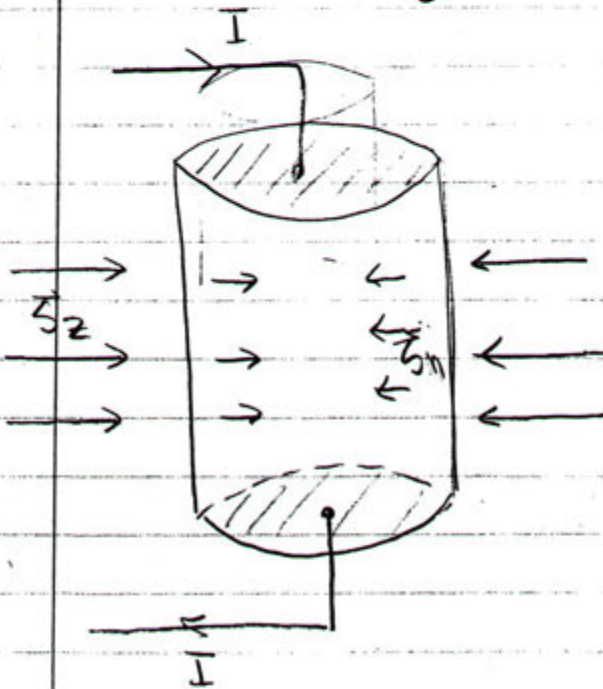
notranji $\leftarrow \vec{H}_n = \vec{1}_\varphi \frac{I}{2\pi a^2} \rho$

$$\vec{S}_n = -\vec{1}_\rho \frac{I^2 \rho}{2\pi \gamma A a^2}$$

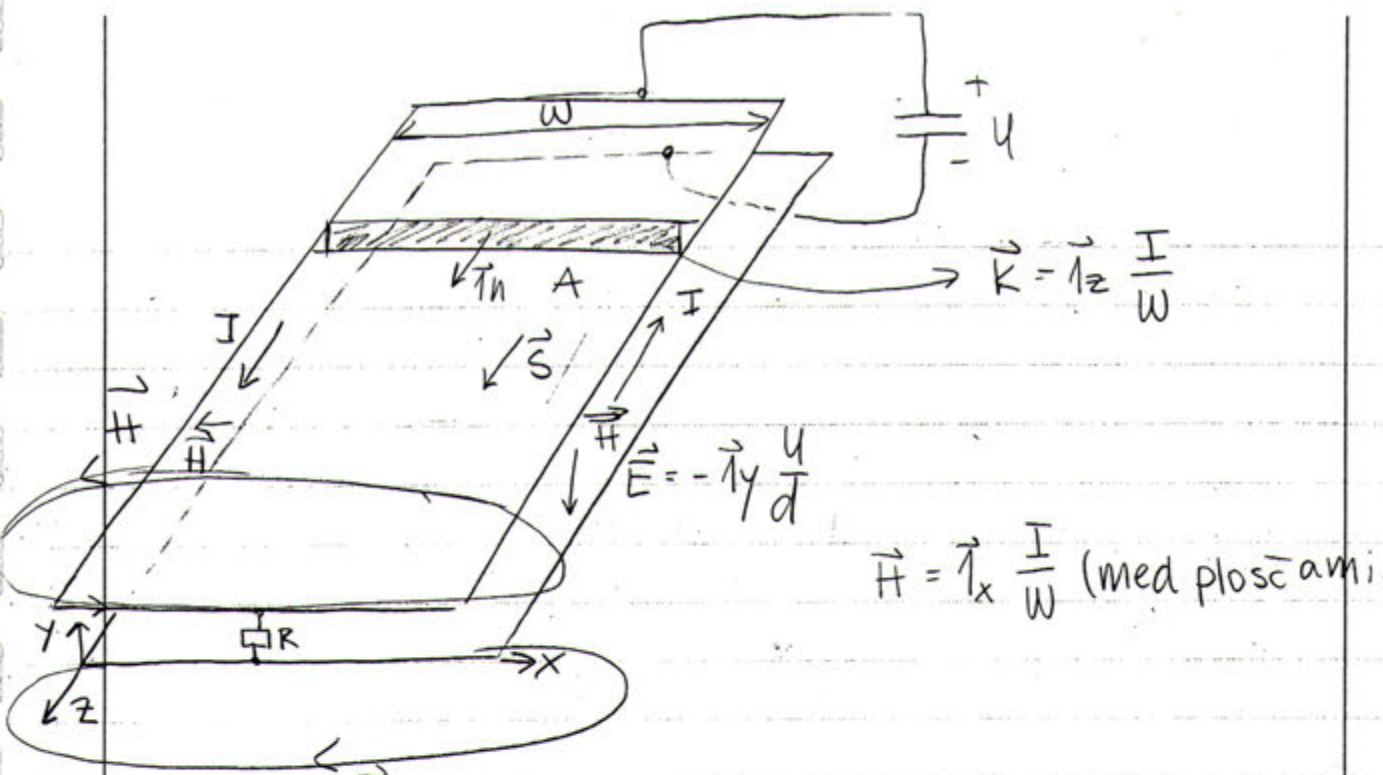
zunajni $\leftarrow \vec{H}_z = -\vec{1}_\varphi \frac{I}{2\pi \rho}$

$$\vec{S}_z = -\vec{1}_\rho \frac{I^2}{2\pi \gamma A \rho}$$

moč vstopa bočno v upor (ne po žicah)



moč ne teče po žicah, ampak po prostoru med žicami



$$\vec{K} = \vec{1}_z \frac{I}{w}$$

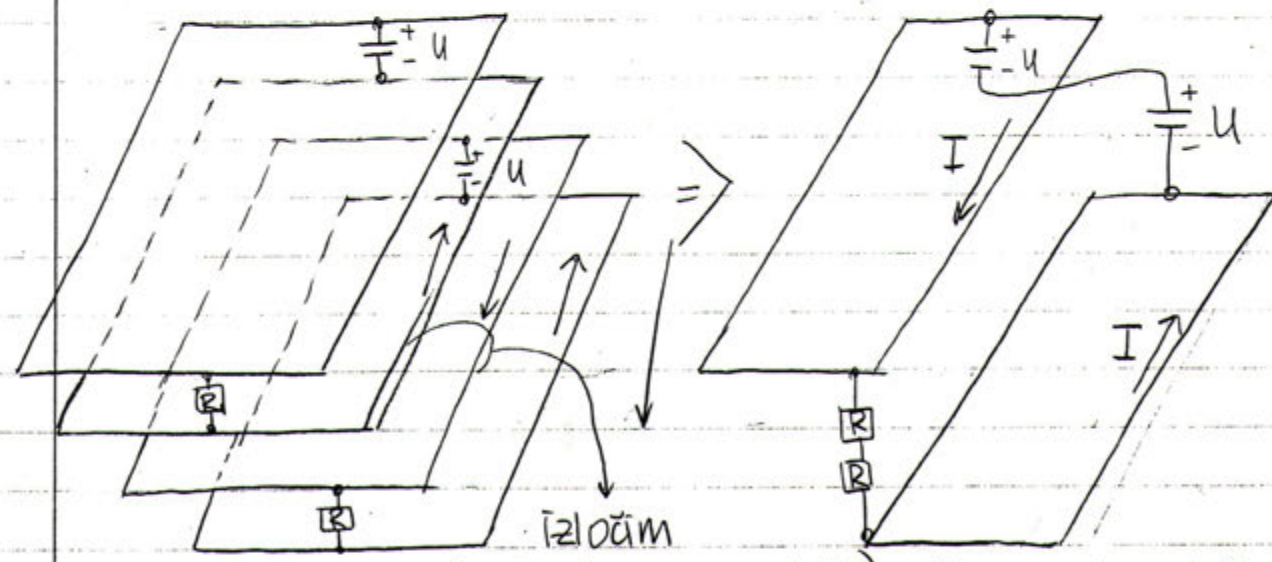
$$\vec{H} = \vec{1}_x \frac{I}{w} \text{ (med ploščama)}$$

$$\vec{E} = -\vec{1}_y \frac{U}{d}$$

$$\vec{S} = \vec{E} \times \vec{H} = -\vec{1}_y \frac{U}{d} \times \vec{1}_x \frac{I}{w} = \vec{1}_z \frac{UI}{d \cdot w}$$

elotna el moč

$$P = \int_A \vec{S} \cdot \vec{1}_n dA = \int_0^w \int_0^d \vec{1}_z \frac{UI}{d \cdot w} \cdot \vec{1}_z dx dy = \underline{\underline{U \cdot I}}$$



(uničujoči prehodi ±I) → tokova se izničata

enosmerne trenutne veličine: $P = U \cdot I$ dokaz da kljub temu

$$\vec{S} = \vec{E} \times \vec{H} \quad \text{če plošči izločimo}$$

moč vseeno teče ⇒ moč

ne teče po žicah,

ampak med njima

kazalci za
harmoniske
veličine
pomemben
fazni kot

$$P = \frac{1}{2} U \cdot I^*$$

$$P = U_{\text{eff}} \cdot I_{\text{eff}}^*$$

$$\vec{S} = \frac{1}{2} \vec{E} \times \vec{H}$$

$$\vec{S} = \vec{E}_{\text{eff}} \vec{H}_{\text{eff}}^*$$

vršne
vrednosti

$$\Delta \vec{A} + \omega^2 \mu \epsilon \vec{A} = -\vec{j} \quad \text{GREENOV SKALARNI IZREK}$$

$$\Delta V + \omega^2 \mu \epsilon V = -\rho/\epsilon$$

$V(\vec{r})$.. iskana funkcija

$U(\vec{r})$.. ugibanje

$$\text{div}(U \cdot \text{grad} V) = \text{grad} U \cdot \text{grad} V + U \Delta V$$

$$\text{div}(V \cdot \text{grad} U) = \text{grad} V \cdot \text{grad} U + V \Delta U$$

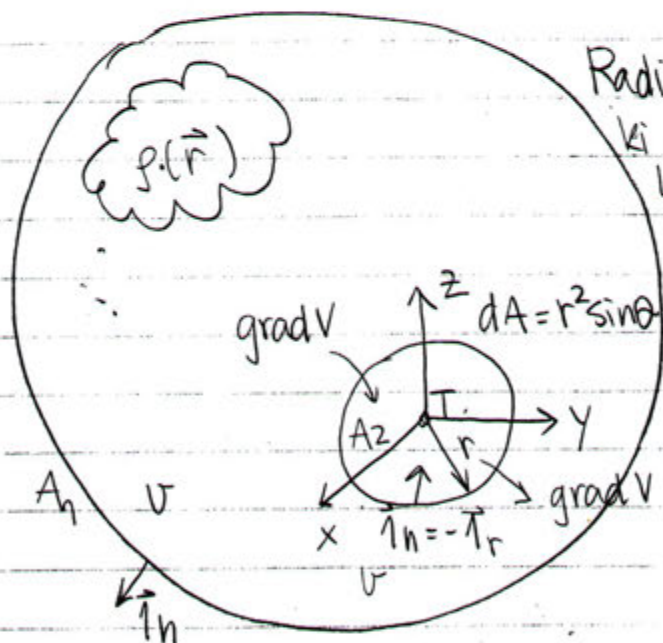
Greenov skalarni izrek:

$$\text{div}(U \text{grad} V - V \text{grad} U) = U \Delta V - V \Delta U \quad / \int_V dv$$

$$\int_V \text{div}(U \text{grad} V - V \text{grad} U) dv = \oint_A (U \cdot \text{grad} V - V \cdot \text{grad} U) \cdot \vec{n} dA =$$

$$= \oint_A \left(U \frac{\partial V}{\partial n} - V \frac{\partial U}{\partial n} \right) dA = \int_V U \Delta V dv - \int_V V \Delta U dv$$

$$\Delta V = -\rho/\epsilon + \omega^2 \mu \epsilon V = -\rho/\epsilon - k^2 V$$



Radi bi izračunali V v točki T_1
 ki se nahaja izhodišču
 bznajo se pojaviti singularnosti
 zato jo izločimo
 s ploskvico A_2

$$A_1 \rightarrow \infty$$

$$A_2 \rightarrow 0$$

$$r \rightarrow \infty$$

$$r \rightarrow 0$$

$$\omega = 0$$

Elektrostatika: $k = 0$

$$\Delta V = -\rho/\epsilon \quad ; \quad V(\infty) = 0$$

ugibam $U = \frac{1}{r}$ \rightarrow rešuje $\Delta U = 0$

$$\Delta U = \text{div}(\text{grad } U)$$

$$(r, \theta, \phi): \text{grad } U = \vec{r} \cdot \frac{1}{r^2} + \vec{\theta} \cdot \frac{1}{r} \cdot 0 + \vec{\phi} \frac{1}{\sin \theta} \cdot 0 = -\vec{r} \cdot \frac{1}{r^2} \quad \checkmark$$

$$\Delta U = \text{div}(-\vec{r} \cdot \frac{1}{r^2}) = \frac{1}{r^2 \sin \theta} \frac{\partial}{\partial r} (r^2 \sin \theta \cdot \frac{1}{r^2}) = 0 \quad //$$

$$\text{Green: } \oint_{A_1+A_2} (U \frac{\partial v}{\partial n} - v \frac{\partial U}{\partial n}) dA = \int_V U \Delta v dv - \int_V v \Delta U dv$$

$\Delta U = 0$

$$A_1 \rightarrow \infty$$

$$v(\infty) \rightarrow 0(r^{-1}); \frac{\partial v}{\partial n} \rightarrow 0(r^{-2})$$

$$\oint_{A_2} (U \frac{\partial v}{\partial n} - v \frac{\partial U}{\partial n}) dA = \int_V U (-\frac{\rho}{\epsilon}) dv$$

$$\oint_{A_2} (\frac{1}{r} \frac{\partial v}{\partial n} - v \frac{1}{r^2}) r^2 \sin \theta d\theta d\phi =$$

$$= - \oint_{A_2} v \sin \theta d\theta d\phi = 4\pi v$$

$$-4\pi v = \int_V \frac{1}{r} (-\frac{\rho}{\epsilon}) dv \Rightarrow v(r=0) = \frac{1}{4\pi\epsilon} \int_V \frac{\rho}{r} dv = \frac{1}{4\pi\epsilon} \sum_i \frac{Q_i}{r_i}$$

$k = \omega \sqrt{\mu \epsilon}$.. valomc šteno

elektrodinamika: $\omega \neq 0$

$$\Rightarrow U = \frac{1}{r} e^{jkr}$$

$$(r, \theta, \phi)$$

$$\text{grad } U = \vec{r} \frac{\partial U}{\partial r} + \vec{\theta} \frac{1}{r} \frac{\partial U}{\partial \theta} + \vec{\phi} \frac{1}{r \sin \theta} \frac{\partial U}{\partial \phi} =$$

$$= \vec{r} \left(-\frac{1}{r^2} e^{jkr} + \frac{j k}{r} e^{jkr} \right) = -\vec{r} \left(\frac{1}{r^2} + \frac{j k}{r} \right) e^{jkr}$$

$$\Delta U = \text{div} \left(-\frac{1}{r} \left(\frac{1}{r^2} + \frac{j k}{r} \right) e^{jkr} \right) = \frac{1}{r^2 \sin \theta} \frac{\partial}{\partial r} \left(r^2 \sin \theta \left(\frac{1}{r^2} + \frac{j k}{r} \right) e^{jkr} \right) =$$

$$= -\frac{1}{r^2} \frac{\partial}{\partial r} \left((1 + jkr) e^{jkr} \right) = -\frac{1}{r^2} \left(jk e^{jkr} + (1 + jkr) (jk) e^{jkr} \right) =$$

U mora reševati takšno enačbo

$$= -\frac{k^2}{r} e^{jkr} = -k^2 U \Rightarrow \Delta U + k^2 U = 0$$

$$\oint_{A_1 \rightarrow \infty} \left(u \frac{\partial v}{\partial n} - v \frac{\partial u}{\partial n} \right) dA_1 + \oint_{A_2 \rightarrow 0} \left(u \frac{\partial v}{\partial n} - v \frac{\partial u}{\partial n} \right) dA_2 =$$

$$= \int_V u \Delta v dv - \int_V v \Delta u dv = \int_V \left(u \left(-\frac{\rho}{\epsilon} - k^2 v \right) - v \left(-k^2 u \right) \right) dv =$$

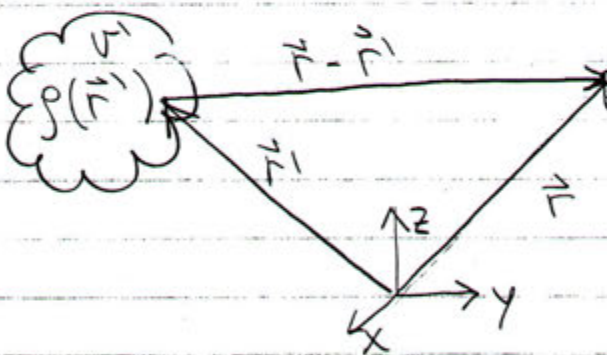
$\Delta v = -\rho/\epsilon - k^2 v$
 $\Delta u = -k^2 u$

$$= \int_V u \left(-\frac{\rho}{\epsilon} \right) dv = -\frac{1}{\epsilon} \int_V \frac{\rho}{r} e^{jkr} dv \quad \leftarrow \text{normala}$$

$$\oint_{A_2} \left(u \frac{\partial v}{\partial n} - v \left(-\vec{n}_r \left(\frac{1}{r^2} + \frac{j k}{r} \right) e^{jkr} \right) \right) (-\vec{n}_r) dA_2 = \underline{4\pi V}$$

$\uparrow k = \omega \sqrt{\mu_0 \epsilon_0}$

$$\Rightarrow \left[V(r=0) = -\frac{1}{4\pi\epsilon} \int_V \frac{\rho(r)}{r} e^{jkr} dv \right] \text{ enačba za zakasnjeni skalarni potencial}$$



$$V(\vec{r}) = \frac{1}{4\pi\epsilon} \int_V \rho(\vec{r}') \cdot \frac{e^{-jk|\vec{r}-\vec{r}'|}}{|\vec{r}-\vec{r}'|} dv'$$

enačba za poljubno porazdelitev elektrinida potencial v poljubni točki

vektorska enačba (x, y, z): \Rightarrow ENAČBA ZA ZAKASNJEN POTENCIAL

$$\Delta \vec{A} = \vec{i}_x \Delta A_x + \vec{i}_y \Delta A_y + \vec{i}_z \Delta A_z$$

$$\Delta \vec{A} + k^2 \vec{A} = -\mu \vec{J} \quad (\text{samo za kartezični ks})$$

$$\Delta A_x + k^2 A_x = -\mu J_x \Rightarrow A_x(\vec{r}) = \frac{\mu}{4\pi} \int_V J_x(\vec{r}') \cdot \frac{e^{jk|\vec{r}-\vec{r}'|}}{|\vec{r}-\vec{r}'|} dv'$$

$$\Delta A_y + k^2 A_y = -\mu J_y \Rightarrow A_y(\vec{r}) = \frac{\mu}{4\pi} \int_V J_y(\vec{r}') \cdot \frac{e^{jk|\vec{r}-\vec{r}'|}}{|\vec{r}-\vec{r}'|} dv'$$

$$\Delta A_z + k^2 A_z = -\mu J_z \Rightarrow A_z(\vec{r}) = \int_V J_z(\vec{r}') \frac{e^{-jk|\vec{r}-\vec{r}'|}}{|\vec{r}-\vec{r}'|} dV'$$

$$\Rightarrow \boxed{\vec{A}(\vec{r}) = \frac{\mu}{4\pi} \int_V \vec{J}(\vec{r}') \frac{e^{-jk|\vec{r}-\vec{r}'|}}{|\vec{r}-\vec{r}'|} dV'} \quad \left. \begin{array}{l} \text{ena\u010dba za zakasnjeni} \\ \text{vektorski potencial} \end{array} \right\}$$

↳ dokazi, velja le za karteziane koordinate

ponovitev:

Maxwellove enačbe v diferencialni obliki

$$\textcircled{1} \text{ rot } \vec{H} = \vec{J} + j\omega \epsilon \vec{E}$$

$$\textcircled{2} \text{ rot } \vec{E} = -j\omega \mu \vec{H}$$

$$\textcircled{3} \text{ div}(\epsilon \vec{E}) = \rho$$

izvor: $\rho, \vec{J} \Rightarrow$ polja \vec{E}, \vec{H}

Neposredna pot?

računamo preko potencialov V, \vec{A}

$$\vec{B} = \text{rot } \vec{A} \Rightarrow \vec{H} = \frac{1}{\mu} \text{rot } \vec{A}$$

$$\vec{E} = -j\omega \vec{A} - \text{grad } V$$

Lorentzova izbira = $\text{div } \vec{A}$

$$\Delta V + \omega^2 \mu \epsilon V = -\rho / \epsilon$$

$$\Delta \vec{A} + \omega^2 \mu \epsilon \vec{A} = -\mu \vec{J}$$

} analitske rešitve
koordinata izvora

$$V(\vec{r}) = \frac{1}{4\pi\epsilon} \int_{V'} \rho(\vec{r}') \frac{e^{-jk|\vec{r}-\vec{r}'|}}{|\vec{r}-\vec{r}'|} dV'$$

skalarni
potencial

↳ koordinate veličine,

↳ razdalja od izvora

ki jo računamo

do točke, kjer gledamo

\vec{r}' ... koordinate izvora

\vec{r} ... koordinate potenciala

$$k^2 = \omega^2 \mu \epsilon$$

$$k = \frac{\omega}{c} = \frac{2\pi}{\lambda}$$

$$\vec{A} = \frac{\mu}{4\pi} \int_{V'} \vec{J}(\vec{r}') \frac{e^{-jk|\vec{r}-\vec{r}'|}}{|\vec{r}-\vec{r}'|} dV'$$

vektorski
potencial

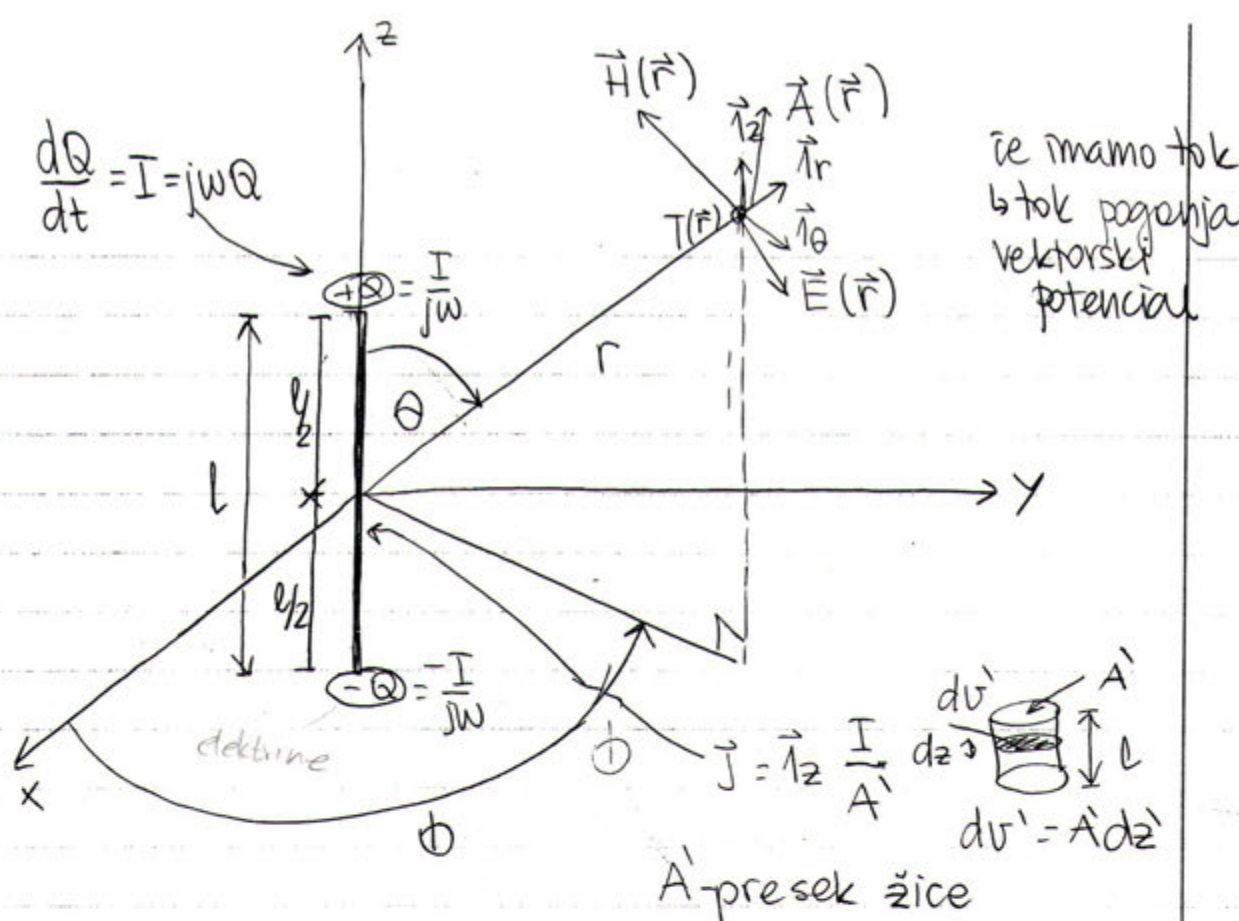
- Zgled: (r, θ, ϕ)

$$h_r = 1$$

$$h_\theta = r$$

$$h_\phi = r \sin \theta$$

$$\vec{A}(\vec{r}) = \frac{\mu}{4\pi} \int_{V'} \vec{J} \frac{1}{r^2} \frac{e^{-jk|\vec{r}-\vec{r}'|}}{|\vec{r}-\vec{r}'|} A' dz'$$



poenostavitve:

1. $r \gg l \Rightarrow \frac{1}{|\vec{r} - \vec{r}'|} \approx \frac{1}{r}$

2. $k^2 = \omega^2 \mu \epsilon$; $k = \omega \sqrt{\mu \epsilon} = \frac{\omega}{c} = \frac{2\pi}{\lambda}$... valovno število
 $\frac{1}{k} \gg l \Rightarrow e^{jk|\vec{r} - \vec{r}'|} \approx e^{-jkr}$ (majhna fazna napaka)

$\frac{\lambda}{2\pi} \gg l$

$\vec{A}(\vec{r}) = \frac{\mu}{2\pi} I \int_{-l/2}^{l/2} \vec{i}_z \cdot \frac{e^{-jkr}}{r} dz' = \vec{i}_z \frac{\mu I l}{4\pi} \frac{e^{-jkr}}{r}$

$\vec{i}_z \cdot \vec{i}_r = \cos \theta$
 $\vec{i}_z \cdot \vec{i}_\theta = -\sin \theta$
 $\vec{i}_z \cdot \vec{i}_\phi = 0$
 $\Rightarrow \vec{i}_z = \vec{i}_r \cos \theta - \vec{i}_\theta \sin \theta$
 smernik \vec{i}_z ni smernik krogelnega coord. sistema

$\vec{A}(\vec{r}) = (\vec{i}_r \cos \theta - \vec{i}_\theta \sin \theta) \frac{\mu I l}{4\pi} \frac{e^{-jkr}}{r}$ vektorski TOKOVE DALJICE
 potencial žice
 v krogelnem k.s.

| | | | |
|---|---------------------------------|---------------------------------|---------------------------------|
| $\text{rot } \vec{A} = \frac{1}{h_1 h_2 h_3}$ | $\vec{i}_{g_1} h_1$ | $\vec{i}_{g_2} h_2$ | $\vec{i}_{g_3} h_3$ |
| | $\frac{\partial}{\partial a_1}$ | $\frac{\partial}{\partial a_2}$ | $\frac{\partial}{\partial a_3}$ |
| | $h_1 A_1$ | $h_2 A_2$ | $h_3 A_3$ |

$$\vec{H} = \frac{1}{\mu} \text{rot } \vec{A} = \frac{-1}{\mu} \frac{1}{r^2 \sin \theta} \begin{vmatrix} \vec{r} & r\vec{\theta} & r\sin\theta\vec{\phi} \\ \partial/\partial r & \partial/\partial \theta & \partial/\partial \phi \\ \frac{\mu I l}{4\pi} \frac{e^{jkr}}{r} \cos \theta & \frac{\mu I l}{4\pi} \frac{e^{jkr}}{r} (-\sin \theta) & r \sin \theta \frac{e^{jkr}}{r} \end{vmatrix}$$

$$= \frac{1}{\mu} \frac{1}{r^2 \sin \theta} \frac{\mu I l}{4\pi} \left[\vec{r} \cdot 0 + r \cdot \vec{\theta} \cdot 0 + \vec{\theta} \cdot r \sin \theta (\sin \theta \cdot jk e^{-jkr} + \sin \theta \frac{e^{jkr}}{r}) \right]$$

sevanje ∇

$$\vec{H} = \vec{\theta} \frac{I l}{4\pi} e^{jkr} \left(\frac{jk}{r} + \frac{1}{r^2} \right) \sin \theta$$

Mag. polje tokove daljice

→ Biot-Savartov zakon

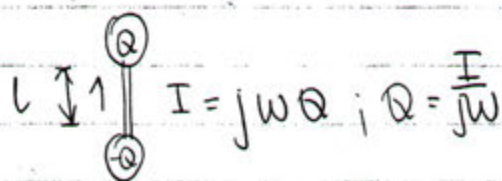
(DET2: $\omega = 0$: Biot-Savart)
 → $e^{jkr} = 1$

$$\vec{E} = -j\omega \vec{A} - \text{grad } V \stackrel{ME \textcircled{1}}{=} \frac{1}{j\omega \epsilon} (\text{rot } \vec{H} - \vec{J}) \quad \leftarrow \vec{J} = 0$$

↳ V "poganja" točkasti dipol Ql .

$$\vec{E} = \frac{1}{j\omega \epsilon} \frac{1}{r^2 \sin \theta} \begin{vmatrix} \vec{r} & r\vec{\theta} & r\sin\theta\vec{\phi} \\ \partial/\partial r & \partial/\partial \theta & \partial/\partial \phi \\ 0 & r \cdot 0 & r \sin \theta \cdot \frac{I l}{4\pi} e^{jkr} \left(\frac{jk}{r} + \frac{1}{r^2} \right) \sin \theta \end{vmatrix}$$

$$= \frac{1}{j\omega \epsilon} \frac{1}{r^2 \sin \theta} \frac{I l}{4\pi} \left[\vec{r} e^{jkr} \left(jk + \frac{1}{r} \right) 2 \sin \theta \cos \theta + \vec{\theta} \cdot r \left(jk e^{jkr} \left(jk + \frac{1}{r} \right) \right) + e^{jkr} \cdot \frac{1}{r^2} \sin^2 \theta \right]$$



$$\vec{E} = \frac{Ql}{4\pi \epsilon \cdot j\omega} e^{jkr} \left[\vec{r} \left(\frac{jk}{r^2} + \frac{1}{r^3} \right) 2 \cos \theta + \vec{\theta} \left(-\frac{k^2}{r} + \frac{jk}{r^2} + \frac{1}{r^3} \right) \sin \theta \right]$$

sevanje na velikih razdaljah prevlada,
ne izgine, le počasni upada

$$\vec{E} = \frac{Ql}{4\pi\epsilon_0 r^2} e^{jkr} \left[\vec{r} \left(\frac{2jk}{r^2} + \frac{2}{r^3} \right) \cos\theta + \vec{\theta} \left(-\frac{k^2}{r} + \frac{jk}{r^2} + \frac{1}{r^3} \right) \sin\theta \right]$$

zakasnitev

točkasti
elektrostatični
dipol

SEVANJE

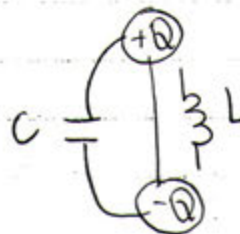
| | energetika f = 50 Hz | GSM telefon f = 900 MHz | vidna svetloba f = 600 THz ($\lambda = 0,5 \mu\text{m}$) |
|--|--|--|---|
| $k = \frac{\omega}{c} = \frac{2\pi f}{c}$ $k = \frac{k}{r} @ r = 1\text{m}$ | $1,05 \cdot 10^{-6} \frac{\text{rad}}{\text{m}}$ | $18,9 \frac{\text{rad}}{\text{m}}$ | $12,5 \cdot 10^6 \frac{\text{rad}}{\text{m}}$ |
| $\left \frac{k^2}{r} \right @ r = 1\text{m}$ | $1,1 \cdot 10^{-12} \frac{\text{rad}^2}{\text{m}^3}$ | $360 \frac{\text{rad}^2}{\text{m}^3}$ | $157 \cdot 10^{12} \frac{\text{rad}^2}{\text{m}^3}$ |
| r = 1m | samo statični členi: 10^6 sevanje | sevanje = = 360 x statika | sevanje = = 10^{14} x statika |
| r = ? enako veliki členi k = 1/r | samo statika 950 km | 5,3 m $\begin{matrix} \uparrow \text{statika} \\ \downarrow \text{dipol} \\ \downarrow \text{dinamika} \end{matrix}$ | 80 nm => samo sevanje |

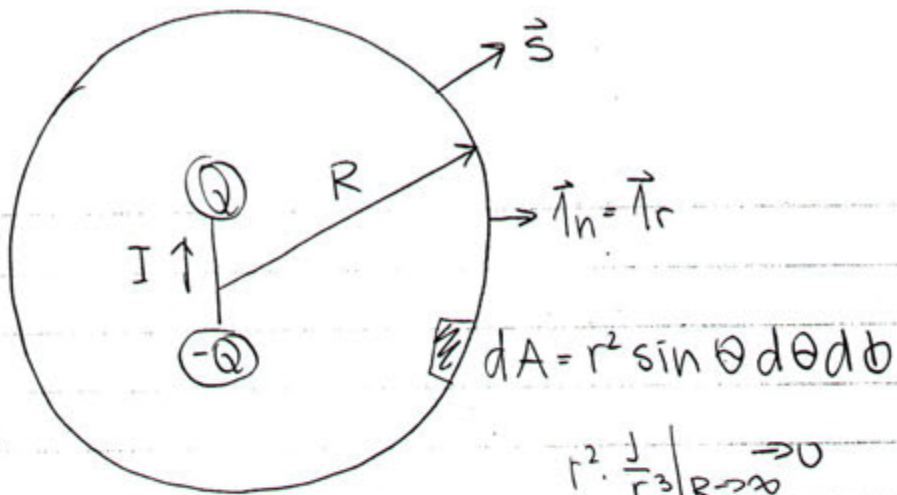
Poyntingov vektor:

$$\vec{S} = \frac{1}{2} \vec{E} \times \vec{H}^* = \frac{1}{2} \frac{I l}{4\pi j \omega \epsilon_0} e^{jkr} \left[\vec{r} \left(\frac{2jk}{r^2} + \frac{2}{r^3} \right) \cos\theta + \vec{\theta} \left(-\frac{k^2}{r} + \frac{jk}{r^2} + \frac{1}{r^3} \right) \sin\theta \right] \times \vec{\theta} \frac{I l}{4\pi} e^{+jkr} \left(-\frac{jk}{r} + \frac{1}{r^2} \right) \sin\theta$$

$$\vec{S} = \frac{I^2 l^2}{32\pi^2 \omega \epsilon_0} \left[\vec{r} \left(\frac{k^3}{r^2} - \frac{j}{r^5} \right) \sin^2\theta + \vec{\theta} \left(\frac{2jk^2}{r^3} + \frac{2j}{r^5} \right) \cos\theta \sin\theta \right]$$

delovna moč jalovo jalovo





Koliko je delovne moči?

$$r^2 \cdot \frac{j}{r^3} \Big|_{R \rightarrow \infty} \rightarrow 0$$

$$P = \int_{4\pi, R \rightarrow \infty} \vec{s} \cdot \vec{n} \cdot dA = \int_0^\pi \int_0^{2\pi} \frac{|I|^2 l^2}{32\pi^2 \omega \epsilon} \left(\frac{k^3}{r^2} - \frac{j}{rs} \right) \sin^2 \theta r^2 \sin \theta d\theta d\phi$$

$$P = \frac{|I|^2 l^2}{32\pi^2 \omega \epsilon} 2\pi k^3 \int_0^\pi \sin^2 \theta d\theta$$

nova sprem. $u = \cos \theta$
 $du = -\sin \theta d\theta$
 $1 - u^2 = \sin^2 \theta$

$$= \frac{|I|^2 l^2}{16\pi \omega \epsilon} k^3 \int_{-1}^1 (1 - u^2) du$$

$$2 - \frac{2}{3} = \frac{4}{3}$$

$$P = \frac{|I|^2 l^2}{12\pi \omega \epsilon} k^3 = \frac{2 |I|^2 l^2}{12\pi} k^2 = \frac{1}{2} |I|^2 R_s \Rightarrow R_s = \frac{2 l^2}{6\pi} k^2 = \frac{2\pi z}{3} \left(\frac{l}{\lambda^2} \right)$$

$$Z_0 = \sqrt{\frac{\mu_0}{\epsilon_0}} = 377 \Omega = 120\pi \Omega$$

sevalna upornost

predpostavka: $l \ll \lambda$

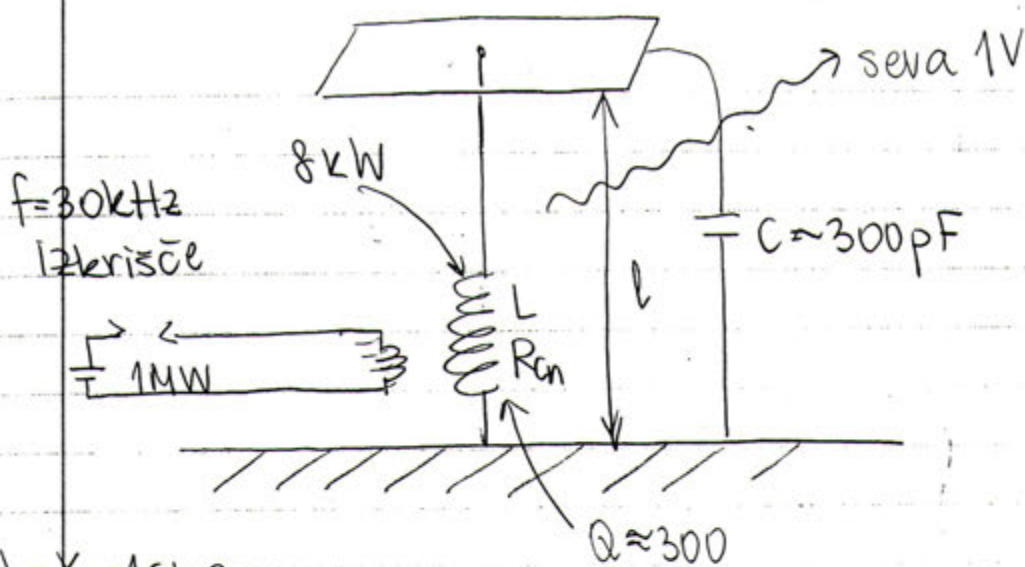
$$\omega \epsilon = \omega \sqrt{\mu \epsilon} \sqrt{\frac{\epsilon}{\mu}} = \frac{k}{z}$$

$\sqrt{\frac{\mu}{\epsilon}}$.. valovna impedanca
 $k = \frac{2\pi}{\lambda}$ $k = \frac{\omega \epsilon}{z}$

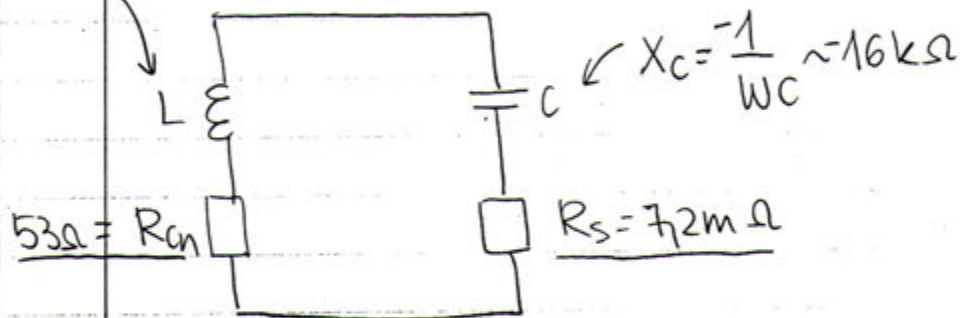
• pravilno nadomestno vezje:



$R_s \leftarrow$ sevalna upornost



$$WL = X_L = 16 \text{ k}\Omega$$



$$X_C = -\frac{1}{\omega C} = -\frac{1}{3 \cdot 10^4 \cdot 2\pi \frac{\text{rad}}{\text{s}} \cdot 3 \cdot 10^{-10} \text{ As}} = -16 \text{ k}\Omega$$

$$Q = \frac{WL}{R_{cn}} \Rightarrow R_{cn} = \frac{WL}{Q} = \frac{X_L}{Q} = \frac{16 \text{ k}\Omega}{300} = 53 \Omega$$

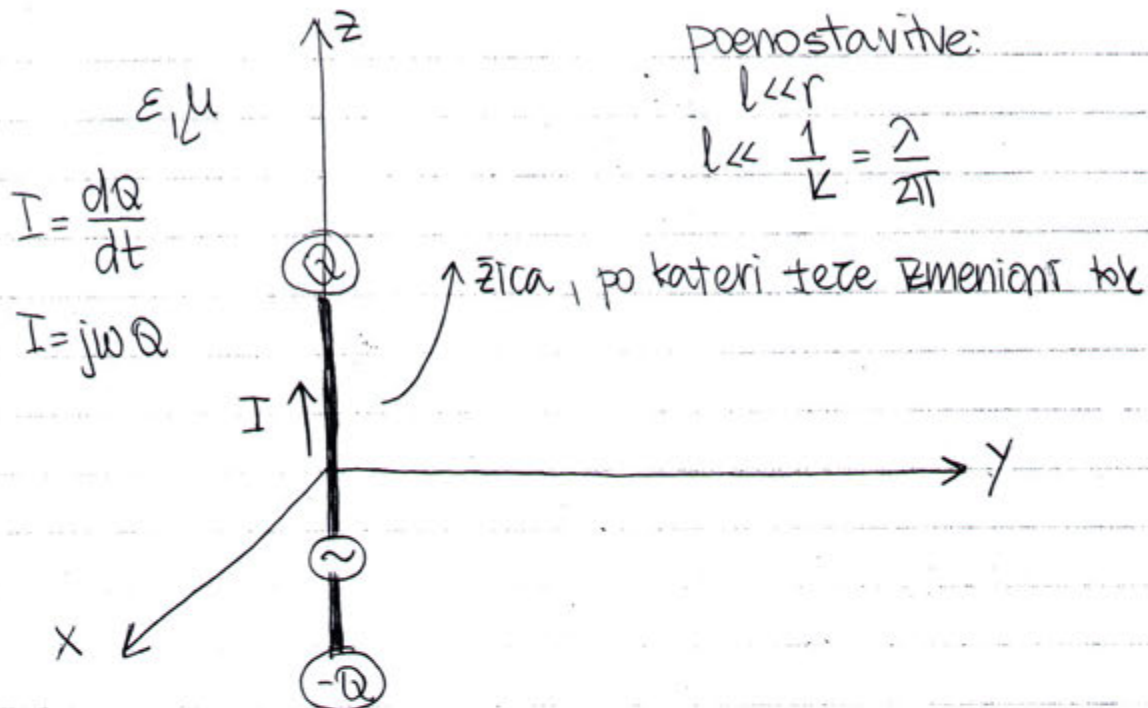
$$\lambda = \frac{c_0}{f} = \frac{3 \cdot 10^8 \text{ m/s}}{3 \cdot 10^4 \text{ Hz}} = \underline{10 \text{ km}} \gg l = 30 \text{ m}$$

$$R_s = \frac{2\pi Z_0}{3} \left(\frac{l}{\lambda}\right)^2 = \frac{2\pi \cdot 120 \pi \Omega}{3} \left(\frac{30}{10^4}\right)^2 = 800 \Omega \frac{900}{10^8} = 7,2 \text{ m}\Omega$$

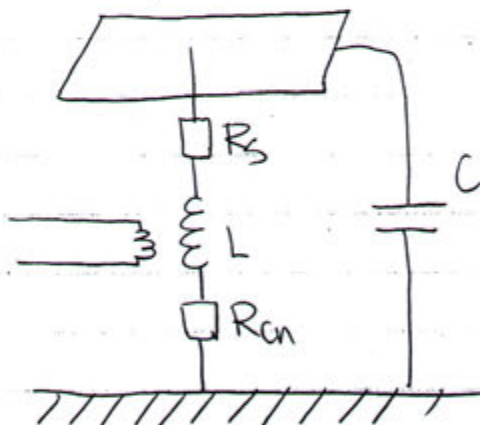
izkoristek sevanja:

$$\eta = \frac{R_s}{R_{cn} + R_s} = \frac{7,2 \cdot 10^{-3} \Omega}{53 \Omega} = 1,3 \cdot 10^{-4} = \underline{\underline{0,013\%}}$$

$$\eta = \frac{R_s}{R_s + R_{cn}}$$



Teslov transformator: Primer žice

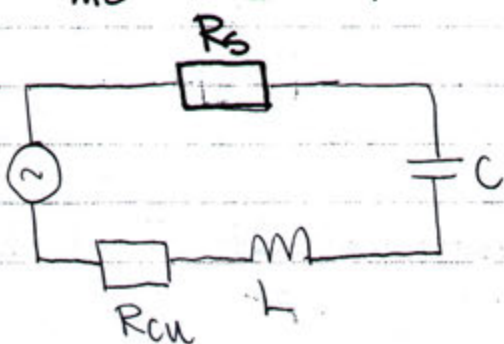


R_s .. sevalna upornost
 (ni upoštevano sevanje)

(r, θ, ϕ)

$\vec{H} = \vec{\hat{\theta}} \frac{I l}{4\pi r} e^{jkr} \left(\frac{jk}{r} + \frac{1}{r^2} \right) \sin \theta$

$\vec{E} = \frac{Q l}{4\pi \epsilon_0 r^2} e^{jkr} \left[\vec{\hat{r}} \left(\frac{2jk}{r^2} + \frac{2}{r} \right) \cos \theta + \vec{\hat{\theta}} \left(-\frac{k^2}{r} + \frac{jk}{r^2} + \frac{1}{r^3} \right) \sin \theta \right]$



$R_s = \frac{2\pi Z}{3} \left(\frac{l}{\lambda} \right)^2$ majhna

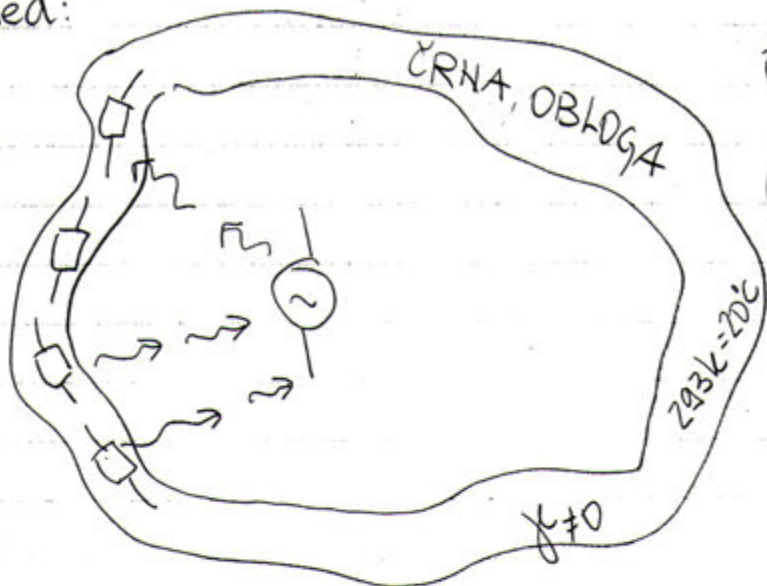
$Z = \sqrt{\frac{\mu}{\epsilon}}$

pretok moči, ki potuje
 v neskončnost od
 naše naprave

sevanje

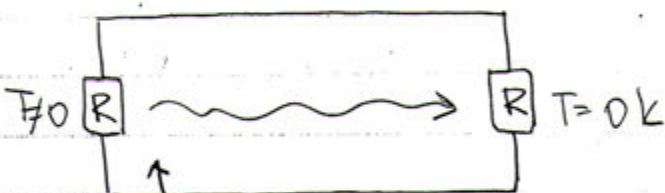
sevanje

- Zgled:



Črna obloga
vpije sevanje
(da imamo pretvorbo
el. energije v toploto
↳ upori, ki so preko
sevalnih denov
sklopljeni na napravo)

prazen prostor: ϵ_0, μ_0 } $T = 2,7 K$
 $\gamma = 0$



$P = Af k_B T$ toplotno gibanje elektronov →
↳ izmenična napetost

$r \ll \frac{1}{k} \Rightarrow$ statika (OET)
 $r \sim \frac{1}{k} \Rightarrow$ komplicirane enačbe
 $r \gg \frac{1}{k} \Rightarrow$ sevanje



velikost ni odvisna
↑ od razdalje

Velike razdalje
(r, θ, ϕ)

$$\frac{\partial}{\partial r} (e^{jkr}) = -jk e^{jkr}$$

odvod faze ∇ vsi drugi
je velik 0 majhni
Vsi ostali odvodi so odvisni od razdalje

$$\frac{\partial}{\partial r} \Rightarrow -jk$$

$$\frac{1}{r} \frac{\partial}{\partial \theta} \Rightarrow 0$$

$$\frac{1}{r \sin \theta} \frac{\partial}{\partial \phi} \Rightarrow 0$$

$$\text{rot } \vec{A} = \frac{1}{h_1 h_2 h_3} \begin{vmatrix} \vec{e}_1 h_1 & \vec{e}_2 h_2 & \vec{e}_3 h_3 \\ \frac{\partial}{\partial q_1} & \frac{\partial}{\partial q_2} & \frac{\partial}{\partial q_3} \\ h_1 A_1 & h_2 A_2 & h_3 A_3 \end{vmatrix} \quad r \gg \frac{1}{k} \downarrow \approx$$

$$= \frac{1}{r^2 \sin \theta} \begin{vmatrix} \vec{r} & \vec{e}_\theta \cdot r & r \sin \theta \vec{e}_\phi \\ jk & 0 & 0 \\ A_r & r A_\theta & r \sin \theta A_\phi \end{vmatrix}$$

0, ker ne bo nikjer različen od 0

$$\vec{A} = (\vec{r} \cos \theta - \vec{e}_\theta \sin \theta) \frac{\mu I l}{4\pi r} \cdot \frac{1}{c} \quad \text{približek nam da}$$

$$\vec{H} = \frac{1}{\mu} \text{rot } \vec{A} = \vec{e}_\phi jk \frac{I l}{4\pi} \frac{\sin \theta}{r}$$

samo sevano polje
magnetno sevano polje
↳ samo sevanje

$$\vec{E} = -j\omega \vec{A} - \text{grad } V = -j\omega \vec{A} - \vec{r} \frac{\partial V}{\partial r} \approx -j\omega (\vec{A} - \vec{r} (\vec{r} \cdot \vec{A})) \text{ sevanje}$$

$$\text{če } r \gg \frac{1}{k} : \rho = 0 = \text{div } \epsilon \vec{E} = \frac{1}{r^2 \sin \theta} \left[\frac{\partial}{\partial r} (r^2 \sin \theta \epsilon E_r) \right] \downarrow = 0$$

$$\vec{E} = \vec{e}_\theta j\omega \frac{\mu I l}{4\pi} \frac{\sin \theta}{r} \quad \text{električno sevano polje}$$

pri sevanem el. in mag. polju
nimamo radialnih komponent

$$j\omega \mu = j\omega \sqrt{\mu \epsilon} \frac{\omega \mu \epsilon}{\omega \epsilon} = j \frac{k^2}{\omega \epsilon}$$

$$I = j\omega Q \rightsquigarrow \text{pride } - \frac{k^2}{r} \text{ sevanje}$$

sevanje: $\begin{matrix} \vec{E} \perp \vec{r} \\ \vec{H} \perp \vec{r} \\ \vec{E} \perp \vec{H} \end{matrix} \left. \vphantom{\begin{matrix} \vec{E} \\ \vec{H} \\ \vec{E} \end{matrix}} \right\} \text{Prečno valovanje} \quad \text{transferzalno} \\ \text{elektromagnetno} \\ \text{valovanje} \quad \underline{\text{TEM}} \quad \nabla \circ$

Maxwellove enačbe:

$$\begin{aligned} \textcircled{2} \text{ rot } \vec{E} &= -j\omega\mu \vec{H} \\ \Rightarrow \vec{H} &= \frac{-j}{\omega\mu} \text{rot } \vec{E} = \frac{-j}{\omega\mu} (-jk) \hat{r} \times \vec{E} = \frac{k}{\omega\mu} \hat{r} \times \vec{E} = \\ &= \frac{\omega\sqrt{\mu\epsilon}}{\omega\mu} \hat{r} \times \vec{E} = \sqrt{\frac{\epsilon}{\mu}} \hat{r} \times \vec{E} = \frac{1}{Z} \hat{r} \times \vec{E} \end{aligned}$$

$$\begin{aligned} \textcircled{1} \text{ rot } \vec{H} &= \vec{j} = j\omega\epsilon \vec{E} \\ \Rightarrow \vec{E} &= \frac{1}{j\omega\epsilon} \text{rot } \vec{H} \approx \frac{1}{j\omega\epsilon} (-jk) \hat{r} \times \vec{H} = -\sqrt{\frac{\mu}{\epsilon}} \hat{r} \times \vec{H} = \\ &= -Z \hat{r} \times \vec{H} \end{aligned}$$

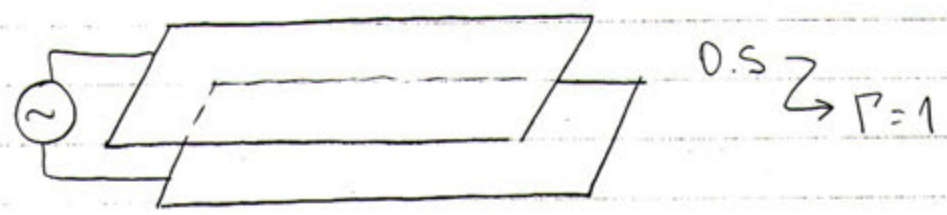
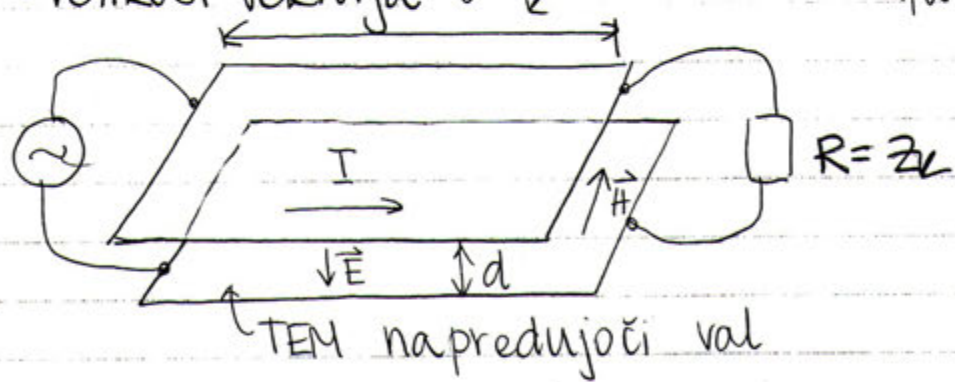
sofazna
(ni faznega zamika)

$$\text{rot } \vec{A} = \frac{1}{r^2 \sin\theta} \begin{vmatrix} \hat{r} & r\hat{\theta} & r\sin\theta\hat{\phi} \\ -jk & 0 & 0 \\ A_r & r \cdot A_\theta & r\sin\theta A_\phi \end{vmatrix} \approx \hat{r} (-jk) \times \vec{A}$$

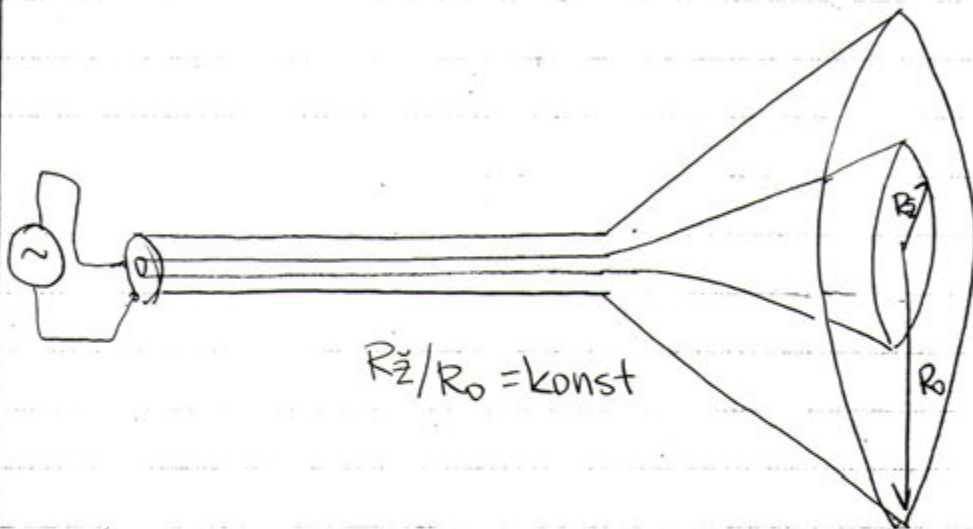
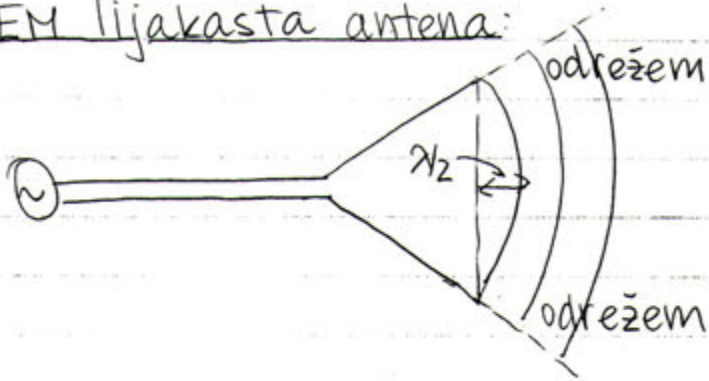
$\hat{r} (-jk)$

SEVANJE $\nabla \cdot \vec{A}$

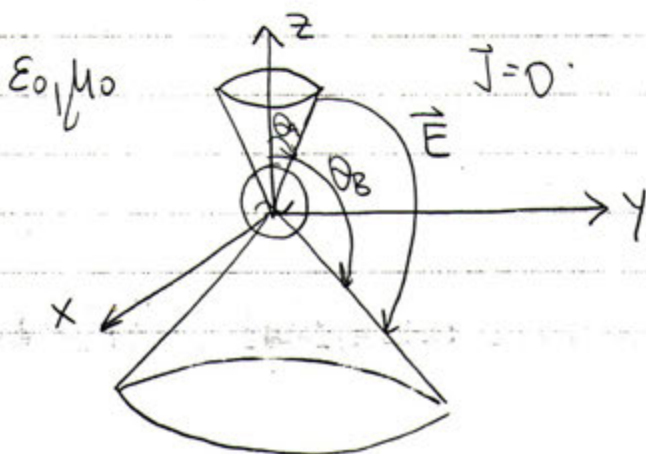
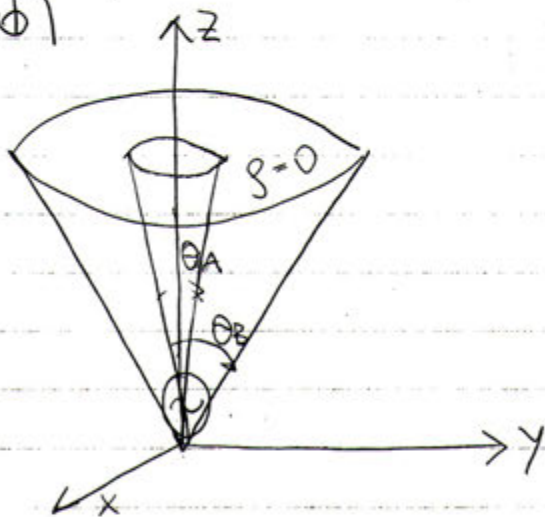
$\frac{|\vec{E}|}{|\vec{H}|} = Z = \sqrt{\frac{\mu}{\epsilon}}$ \vec{E} in \vec{H} sta sofazna! Ko ima en max, ima tudi drugi max. Ni faznega zamika
 \hookrightarrow velikost vektorja $l \approx \frac{1}{k}$ $d, \omega \ll \frac{1}{k}$



TEM lijakasta antena:



(r, θ, ϕ)



rešitev Maxwellovih enačb
 ugibam: $\vec{E} = \vec{1}_\theta \frac{c}{r \sin \theta} e^{jkr}$

① $\text{div } \epsilon \vec{E} = \rho = 0?$

$\text{div } \epsilon \vec{E} = \frac{1}{r^2 \sin \theta} \left[\frac{\partial}{\partial \theta} \left(r \sin \theta \epsilon \frac{c}{r \sin \theta} e^{jkr} \right) \right] = 0 \rightarrow \rho = 0$

elektrine ni!

② $\vec{H} = \frac{j}{\omega \mu} \text{rot } \vec{E} = \frac{j}{\omega \mu} \frac{1}{r^2 \sin \theta} \begin{vmatrix} \vec{1}_r & r \vec{1}_\theta & r \sin \theta \vec{1}_\phi \\ \frac{\partial}{\partial r} & \frac{\partial}{\partial \theta} & \frac{\partial}{\partial \phi} \\ 0 & \frac{c}{\sin \theta} e^{jkr} & r \sin \theta \cdot 0 \end{vmatrix} =$

$= - \vec{1}_\phi \frac{k}{\omega \mu} \frac{c \cdot e^{jkr}}{r \sin \theta}$

$\vec{H} = \vec{1}_\phi \frac{c}{z_0} \frac{e^{jkr}}{r \sin \theta}$

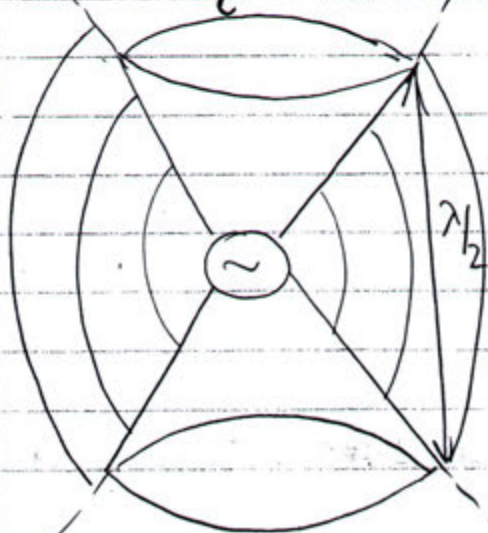
\vec{E} in \vec{H} sta v razmerju
 valovne impedance v

preverimo:

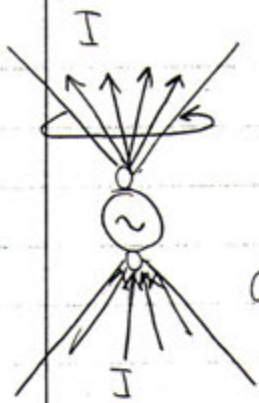
① $\text{rot } \vec{H} = \vec{J} + j\omega \epsilon \vec{E} = \frac{1}{r^2 \sin \theta} \begin{vmatrix} \vec{1}_r & r \vec{1}_\theta & r \sin \theta \vec{1}_\phi \\ \frac{\partial}{\partial r} & \frac{\partial}{\partial \theta} & \frac{\partial}{\partial \phi} \\ 0 & r \cdot 0 & r \sin \theta \frac{e^{jkr}}{r \sin \theta} \frac{c}{z_0} \end{vmatrix} = j\omega \epsilon \vec{E}$

$= \vec{1}_\theta \cdot jk \frac{c}{z_0} \frac{e^{jkr}}{r \sin \theta} - j\omega \epsilon \vec{1}_\theta c \frac{e^{jkr}}{r \sin \theta} = 0 \checkmark \Rightarrow \vec{J} = 0$

$j k / z_0 = \frac{j \omega \sqrt{\mu \epsilon}}{\sqrt{\mu / \epsilon}} = j \omega \epsilon$



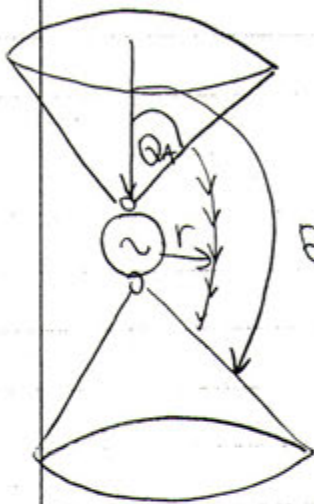
kakšno impedanco
 vidi generator?



$$I = \oint \vec{H} \cdot d\vec{s} = \int_0^{2\pi} \vec{I}_\theta \frac{c}{z_0} \frac{e^{jkr}}{r \sin \theta} \vec{I}_\theta r \sin \theta d\phi =$$

$$= \frac{2\pi c}{z_0} e^{jkr}$$

$d\vec{s} = \vec{I}_\theta r \sin \theta d\phi$ gornji stožec



$$U = \int_{\theta_A}^{\theta_B} \vec{I}_\theta \frac{c e^{jkr}}{r \sin \theta} \vec{I}_\theta r d\theta =$$

$$= c e^{jkr} \int_{\theta_A}^{\theta_B} \frac{d\theta}{\sin \theta} = c e^{jkr} \ln \left(\tan \frac{\theta}{2} \right) \Big|_{\theta_A}^{\theta_B}$$

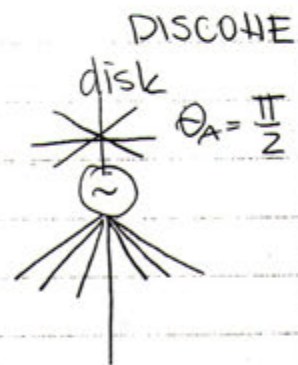
$$ds = \vec{I}_\theta \cdot r d\theta$$

$$\int \frac{d\theta}{\sin \theta} = \ln \left(\tan \frac{\theta}{2} \right) + c$$

vir pri $r=0$: $Z_s = \frac{U}{I} = \frac{c e^{jkr} \ln \left(\tan \frac{\theta}{2} \right) \Big|_{\theta_A}^{\theta_B}}{\frac{2\pi c}{z_0} e^{jkr}}$

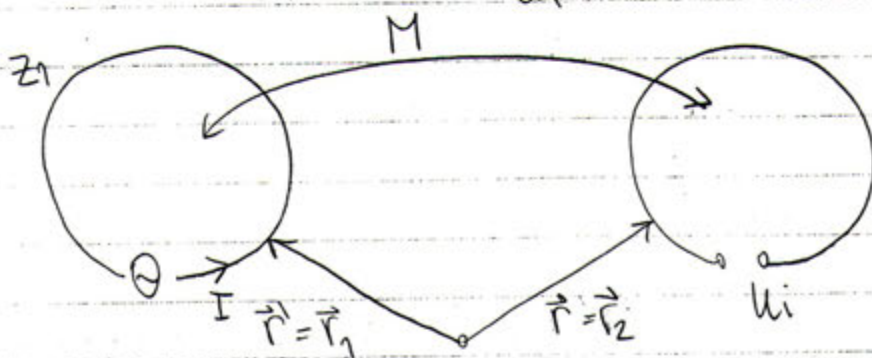
sevalna impedanca:

$$Z_s = R_s = \frac{z_0}{2\pi} \ln \left(\frac{\tan \theta_B/2}{\tan \theta_A/2} \right)$$



Primer:

$$R_s = 60 \Omega \ln \frac{\tan(\theta_B/2)}{\tan(\pi/4)} \rightarrow \theta_A = \pi/2$$



$$M = z_0$$

$$\vec{A} = \frac{\mu}{4\pi} \oint_{z_1} I \frac{e^{-jk|\vec{r}-\vec{r}'|}}{|\vec{r}-\vec{r}'|} d\vec{s}_1 \quad ; \quad \phi = \int_{A_2} \vec{B} \cdot \vec{n} dA$$

$$\vec{B} = \text{rot } \vec{A} \quad M = \frac{\phi}{I}$$

stokes

$$\phi = \int_{A_2} \text{rot } \vec{A} \cdot \vec{n} dA \stackrel{\text{stokes}}{=} \oint_{z_2} \vec{A} \cdot d\vec{s}_2$$

$$M = \frac{\mu}{4\pi} \oint_{z_1} \oint_{z_2} \frac{e^{-jk|\vec{r}_2-\vec{r}_1|}}{|\vec{r}_2-\vec{r}_1|} d\vec{s}_1 \cdot d\vec{s}_2$$

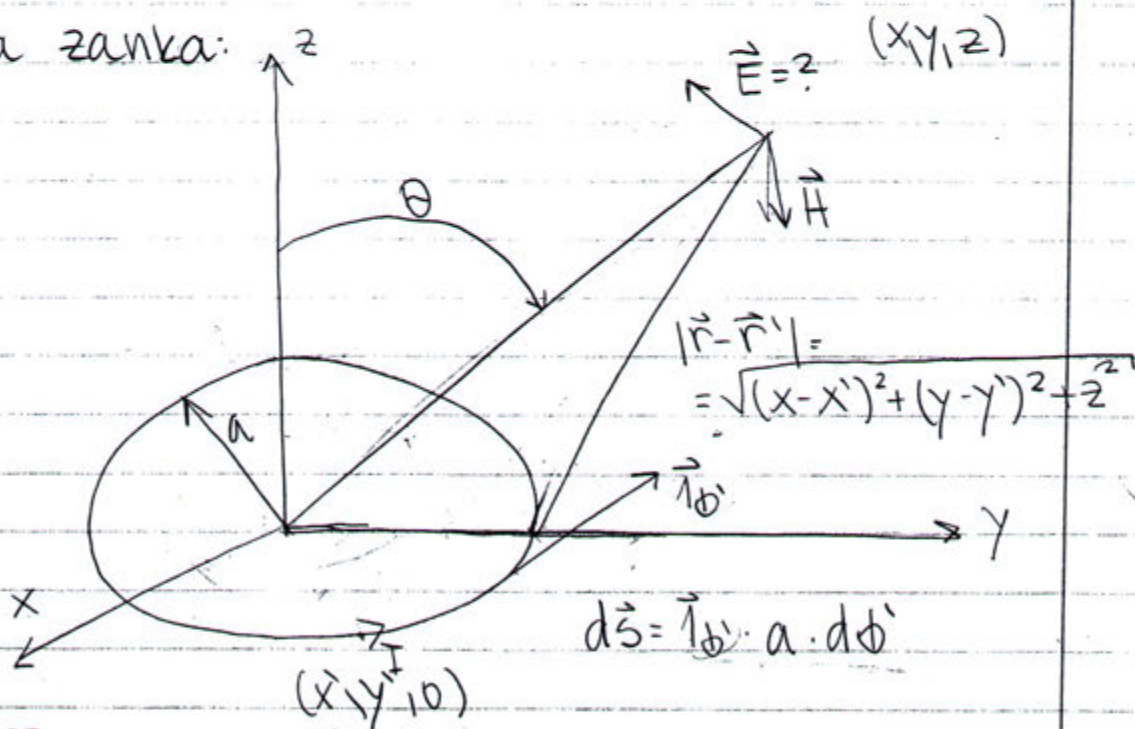
ni vektorskih produktov
↳ ni važno ali je levi
ali desni koordinatni sistem

M definiran $w=0$ $ijk=0$ v stacionarnem

$$M = \frac{\mu}{4\pi} \oint_{z_1} \oint_{z_2} \frac{d\vec{s}_1 \cdot d\vec{s}_2}{|\vec{r}_2-\vec{r}_1|}$$

majhna zanka:

- ① $a \ll r$
- ② $a \ll \frac{1}{k}$



$$\vec{A} = \frac{\mu}{4\pi} \int_0^{2\pi} \vec{r}_{\phi'} \cdot I \cdot \frac{e^{-jk|\vec{r}-\vec{r}'|}}{|\vec{r}-\vec{r}'|} \cdot a \cdot d\phi'$$

$$A = \frac{\mu I a}{4\pi} \int_0^{2\pi} \vec{r}_{\phi'} \cdot \frac{e^{-jk|\vec{r}-\vec{r}'|}}{|\vec{r}-\vec{r}'|} d\phi'$$

$$\vec{r}_{\phi'} = -\vec{r}_x \sin\phi' + \vec{r}_y \cos\phi'$$



$$r_{\phi} = r_x \sin\phi$$

$$\begin{aligned}
 |\vec{r} - \vec{r}'| &= \sqrt{(x-x')^2 + (y-y')^2 + z^2} = \\
 &= \sqrt{(r \sin \theta \cos \phi - a \cos \phi')^2 + (r \sin \theta \sin \phi - a \sin \phi')^2 + (r \cos \theta)^2} = \\
 &= \sqrt{r^2 + a^2 - 2ra \sin \theta (\cos \phi \cos \phi' - \sin \phi \sin \phi')} = \\
 &= \sqrt{r^2 + a^2 - 2ra \sin \theta \cos(\phi - \phi')} \approx \\
 &\quad \text{majhen, zanem.}
 \end{aligned}$$

$$\begin{aligned}
 \sqrt{1+x} &\approx 1 + \frac{x}{2} \quad \textcircled{1} \\
 \sqrt{r^2 - 2ra \sin \theta \cos(\phi - \phi')} &\approx \\
 &\approx r \left(1 - \frac{a}{r} \sin \theta \cos(\phi - \phi')\right) \\
 \frac{1}{|\vec{r} - \vec{r}'|} &\approx \frac{1}{r} \left(1 + \frac{a}{r} \sin \theta \cos(\phi - \phi')\right)
 \end{aligned}$$

$$\begin{aligned}
 1 + \frac{1}{x} &\approx 1 + x \\
 e^{-jk|\vec{r} - \vec{r}'|} &\approx e^{-jkr} e^{jka \sin \theta \cos(\phi - \phi')} \quad \textcircled{2} \\
 &\approx e^{-jkr} \left(1 + jka \sin \theta \cos(\phi - \phi')\right)
 \end{aligned}$$

$e^{ix} \approx 1 + ix$ (for $x \ll 1$)
 $e^{ix} = 1 + ix$ (for $\cos x \approx 1$)

$$\vec{A} = \frac{\mu I a}{4\pi} \int_0^{2\pi} (-\vec{r}_x \sin \phi' + \vec{r}_y \cos \phi') e^{-jkr} \left(1 + jka \sin \theta \cos(\phi - \phi')\right) \cdot \frac{1}{r} \left(1 + \frac{a}{r} \sin \theta \cos(\phi - \phi')\right) d\phi'$$

$$\vec{A} = \frac{\mu I a}{4\pi} \frac{e^{-jkr}}{r} \int_0^{2\pi} (-\vec{r}_x \sin \phi' + \vec{r}_y \cos \phi') \left(jka + \frac{a}{r}\right) \sin \theta \cdot \underbrace{(\cos \phi \cos \phi' - \sin \phi \sin \phi')}_{\cos(\phi - \phi')} d\phi'$$

$$\vec{A} = \frac{\mu I a^2}{4\pi} \frac{e^{-jkr}}{r} \left(jk + \frac{1}{a}\right) \sin \theta \left(\vec{r}_y \cdot \pi \cos \phi - \vec{r}_x \cdot \pi \sin \phi\right)$$

A ... površina zanke $\vec{r}_\phi \cdot \pi$

$$\vec{A} = \vec{r}_\phi \frac{\mu I \pi a^2}{4\pi} e^{-jkr} \left(\frac{jk}{r} + \frac{1}{r^2}\right) \sin \theta$$

potencial \swarrow ZANKA mag tokovi dipol \swarrow

$$\vec{E} = -j\omega \vec{A} - \text{grad } V = \vec{r}_\phi \cdot \frac{-j\omega \mu}{4\pi} I \cdot A e^{-jkr} \left(-\frac{jk}{r} + \frac{1}{r^2}\right) \sin \theta$$

\uparrow
 \parallel
 \circ ; ni elektrini!

Prostor brez izvorov: $\vec{J}=0, \rho=0$
 $\Delta \vec{E} + \omega^2 \mu \epsilon \vec{E} = 0$ } valovni enačbi
 $\Delta \vec{H} + \omega^2 \mu \epsilon \vec{H} = 0$ } (vsebujejo ① in ② Max. enačbi)

$$(x, y, z) \quad \omega^2 \mu \epsilon = k^2$$

$$\Delta \vec{E} = \text{grad}(\text{div} \vec{E}) - \text{rot}(\text{rot} \vec{E}) = \vec{1}_x \Delta E_x + \vec{1}_y \Delta E_y + \vec{1}_z \Delta E_z$$

$$\Delta E_x = \frac{\partial^2 E_x}{\partial x^2} + \frac{\partial^2 E_x}{\partial y^2} + \frac{\partial^2 E_x}{\partial z^2} \quad \text{vektorsko enačbo}$$

razstavimo na 3 skalarne

$$\Delta \vec{E} + \omega^2 \mu \epsilon \vec{E} = 0 \implies \begin{cases} \Delta E_x + k^2 E_x = 0 \\ \Delta E_y + k^2 E_y = 0 \\ \Delta E_z + k^2 E_z = 0 \end{cases} \text{skalarnе valovne enačbe}$$

poskusim z nastavkom:

$$E_x(x, y, z) = X(x)Y(y)Z(z)$$

$$YZ \frac{\partial^2 X}{\partial x^2} + XZ \frac{\partial^2 Y}{\partial y^2} + XY \frac{\partial^2 Z}{\partial z^2} + k^2 XYZ = 0 \quad / \cdot \frac{1}{XYZ}$$

$$\underbrace{\frac{1}{X} \frac{\partial^2 X}{\partial x^2}}_{-k_x^2} + \underbrace{\frac{1}{Y} \frac{\partial^2 Y}{\partial y^2}}_{-k_y^2} + \underbrace{\frac{1}{Z} \frac{\partial^2 Z}{\partial z^2}}_{-k_z^2} + k^2 = 0$$

$$k_x^2 + k_y^2 + k_z^2 = k^2$$

$$\frac{1}{X} \frac{\partial^2 X}{\partial x^2} = -k_x^2 \implies \frac{\partial^2 X}{\partial x^2} + k_x^2 X = 0$$

$$\frac{1}{Y} \frac{\partial^2 Y}{\partial y^2} = -k_y^2$$

$$\frac{1}{Z} \frac{\partial^2 Z}{\partial z^2} = -k_z^2$$

Rešitve: $k_x^2 > 0$

$$X = \underbrace{A e^{+jk_x x}}_{\text{odbiti val}} + \underbrace{B e^{-jk_x x}}_{\text{napredujoči val}}$$

potujoča valova

Kam gre moč? Poyntingov vektor:

$$\vec{S} = \frac{1}{2} \vec{E} \times \vec{H}^* = \vec{1}_z \frac{\kappa C C^*}{\omega \mu} e^{jk_z z} \frac{e^{jk_z z}}{*} = \vec{1}_z \frac{|C|^2}{2Z}$$

⇒ TEM (potujoči) val

$$\vec{E} = \vec{1}_E C e^{-jk_x x} e^{jk_y y} e^{jk_z z} = \vec{1}_E C e^{j\vec{k} \cdot \vec{r}}$$

↳ napredujoči val

① M.e.: $0 = \text{div}(\epsilon \vec{E}) = \epsilon \left(\frac{\partial E_x}{\partial x} + \frac{\partial E_y}{\partial y} + \frac{\partial E_z}{\partial z} \right) =$

* $\frac{\partial}{\partial x} = -jk_x$; $\frac{\partial}{\partial y} = -jk_y$; $\frac{\partial}{\partial z} = -jk_z$

$$= \epsilon (\vec{1}_E \cdot \vec{1}_x (-jk_x) C e^{-jk_x x} e^{jk_y y} e^{jk_z z} + \vec{1}_E \cdot \vec{1}_y (-jk_y) C e^{jk_x x} e^{jk_y y} e^{jk_z z} + \vec{1}_E \cdot \vec{1}_z (-jk_z) C e^{jk_x x} e^{jk_y y} e^{jk_z z}) = -j\epsilon \vec{k} \cdot \vec{E} = 0$$

② M.e.: $\vec{H} = \frac{j}{\omega \mu} \text{rot} \vec{E} = \frac{j}{\omega \mu} \begin{vmatrix} \vec{1}_x & \vec{1}_y & \vec{1}_z \\ -jk_x & -jk_y & -jk_z \\ \vec{1}_x \cdot \vec{E} & \vec{1}_y \cdot \vec{E} & \vec{1}_z \cdot \vec{E} \end{vmatrix} = \frac{1}{\omega \mu} \vec{k} \times \vec{E} =$

$$\text{rot} \vec{E} = -j\vec{k} \times \vec{E}$$

$$= \frac{\kappa}{\omega \mu} \vec{1}_k \times \vec{E} = \frac{\vec{1}_k \times \vec{E}}{Z}$$

Definiramo valovni vektor, $\vec{k} = \vec{1}_k \cdot k$

$$\vec{k} = \vec{1}_x k_x + \vec{1}_y k_y + \vec{1}_z k_z$$

$$|\vec{k}| = k = \omega \sqrt{\mu \epsilon}$$

$$\vec{1}_x (-jk_x) + \vec{1}_y (-jk_y) + \vec{1}_z (-jk_z) = -j\vec{k}$$

lastnosti za TEM val: $\vec{k} \perp \vec{E}$
 $\vec{k} \perp \vec{H}$
 $\vec{H} \perp \vec{k}, \vec{H} \perp \vec{E}$

$\vec{S} \perp \vec{E}$ & $\vec{S} \perp \vec{H} \Rightarrow$ TEM val

(ni vzdolžnih komponent)

0 M.e: $\vec{J} = 0 = \text{rot } \vec{H} - j\omega \epsilon \vec{E} = -j\vec{k} \times \left(\frac{1}{\omega \mu} \vec{k} \times \vec{E} \right) - j\omega \epsilon \vec{E} = \underline{0} \checkmark$

Poyntingov vektor:

$$\vec{S} = \frac{1}{2} \vec{E} \times \vec{H}^* = \frac{1}{2} \vec{E} c e^{j\vec{k} \cdot \vec{r}} \times \left(\frac{\vec{k} \times \vec{E} c^* e^{+j\vec{k} \cdot \vec{r}}}{Z} \right) = \vec{k} \frac{c c^*}{2Z} = \vec{k} \frac{|c|^2}{2Z}$$

smer valovnega vektorja ∇
kam bo šla moč

Zgled: ϵ_0, μ_0
 $\vec{k} = (\vec{1}_x + \vec{1}_y + \vec{1}_z) \cdot 2 \frac{\text{rad}}{\text{m}}$

$$k = |\vec{k}| = \sqrt{4 \frac{\text{rad}^2}{\text{m}^2} + 4 \frac{\text{rad}^2}{\text{m}^2} + 4 \frac{\text{rad}^2}{\text{m}^2}} = 2\sqrt{3}$$

$f = ?$
 $k = \frac{\omega}{c_0} = \frac{2\pi f}{c_0} \Rightarrow f = \frac{k c_0}{2\pi} = \frac{3,5 \frac{\text{rad}}{\text{m}} \cdot 3 \cdot 10^8 \text{ m/s}}{2\pi \text{ rad}} = \underline{\underline{166 \text{ MHz}}}$

$|\vec{S}| = 1 \text{ W/m}^2$ kam kaže S?
 $\vec{S} = \vec{k} \cdot |\vec{S}| = \frac{\vec{1}_x + \vec{1}_y + \vec{1}_z}{\sqrt{3}} = 1 \text{ W/m}^2$

$\vec{k} = \frac{\vec{1}_x + \vec{1}_y + \vec{1}_z}{\sqrt{3}}$

$|\vec{S}| = \frac{|\vec{E}|^2}{2z_0} \Rightarrow |\vec{E}| = \sqrt{2z_0 |\vec{S}|} = \sqrt{2 \cdot 377 \Omega \cdot 1 \text{ W/m}^2} = \underline{\underline{27 \text{ V/m}}}$
 smer $\vec{E} \perp \vec{S}$

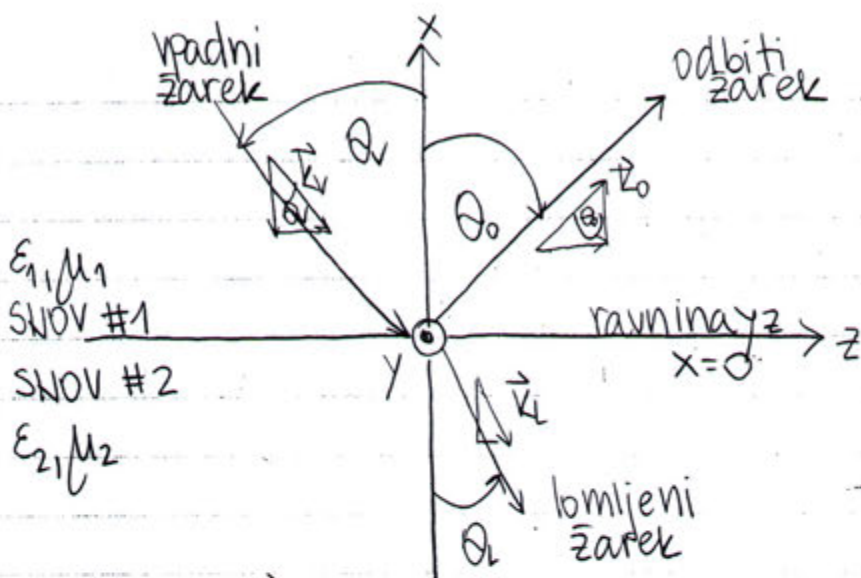
\vec{E} leži v ravnini xy pogoj: $\vec{E} \cdot \vec{k} = 0$ TEM

$\vec{E} = \vec{1}_x \cdot \vec{E}_x + \vec{1}_y \cdot \vec{E}_y$
 $(\vec{1}_x \vec{E}_x + \vec{1}_y \vec{E}_y) \cdot (\vec{1}_x + \vec{1}_y + \vec{1}_z) \cdot 2 \frac{\text{rad}}{\text{m}} = 0$

$(E_x + E_y + 0) \cdot 2 \frac{\text{rad}}{\text{m}} = 0 \Rightarrow E_x = -E_y$

$|\vec{E}| = \sqrt{E_x^2 + E_y^2} = \sqrt{2E_x^2} \Rightarrow E_x = \pm \sqrt{\frac{|\vec{E}|^2}{2}} = \pm \frac{|\vec{E}|}{\sqrt{2}} = \underline{\underline{\pm 19 \text{ V/m}}}$

poljubna ∇
faza \circ



ϵ_1, μ_1
 SNOV #1
 SNOV #2
 ϵ_2, μ_2

$$\vec{k}_v = \vec{1}_x k_{vx} + \vec{1}_z k_{vz}$$

$$\vec{k}_o = \vec{1}_x k_{ox} + \vec{1}_z k_{oz}$$

$$\vec{k}_l = \vec{1}_x k_{lx} + \vec{1}_z k_{lz}$$

enak pojav na meji

⇒ neodvisen od y, z

faza k_v se enako spreminja

kot k_o , kot k_l

$$\Rightarrow k_{vz} = k_{oz} = k_{lz} = \beta$$

$$\vec{k}_v = \vec{1}_x k_{vx} + \vec{1}_z \beta = \vec{1}_v \omega \sqrt{\mu_1 \epsilon_1}$$

$$\vec{k}_o = \vec{1}_x k_{ox} + \vec{1}_z \beta = \vec{1}_o \omega \sqrt{\mu_1 \epsilon_1}$$

$$\vec{k}_l = \vec{1}_x k_{lx} + \vec{1}_z \beta = \vec{1}_l \omega \sqrt{\mu_2 \epsilon_2}$$

$$\left. \begin{aligned} k_{vx}^2 + \beta^2 &= k_1^2 \\ k_{ox}^2 + \beta^2 &= k_1^2 \\ k_{lx}^2 + \beta^2 &= k_2^2 \end{aligned} \right\} \begin{aligned} k_{ox} &= -k_{vx} \Rightarrow \theta_o = \theta_v \\ &\text{odbojni zakon} \end{aligned}$$

$$\sin \theta_v = \frac{\beta}{k_v} = \frac{\beta}{\omega \sqrt{\mu_1 \epsilon_1}}$$

$$\sin \theta_l = \frac{\beta}{k_l} = \frac{\beta}{\omega \sqrt{\mu_2 \epsilon_2}}$$

lomni zakon (Snell)

$$\frac{\sin \theta_l}{\sin \theta_v} = \frac{\sqrt{\mu_1 \epsilon_1}}{\sqrt{\mu_2 \epsilon_2}} = \frac{\sqrt{\mu_{r1} \mu_0 \epsilon_{r1} \epsilon_0}}{\sqrt{\mu_{r2} \mu_0 \epsilon_{r2} \epsilon_0}} = \frac{\sqrt{\mu_{r1} \epsilon_{r1}}}{\sqrt{\mu_{r2} \epsilon_{r2}}} = \frac{n_1}{n_2}$$

lomni količnik: $n = \sqrt{\mu_r \epsilon_r}$ kolikokrat se hitrost svetlobe zmanjša v snovi

$$v = \frac{c_0}{n}$$

$$k = nk_0 = n \omega \sqrt{\mu_0 \epsilon_0}$$

$$\lambda = \frac{c_0}{f} = \frac{c_0}{nf_0} = \frac{\lambda_0}{n}$$

← valovna dolžina v praznem prostoru

$$\left\{ \begin{matrix} \mu \\ \epsilon \end{matrix} \right\} \Rightarrow \left\{ \begin{matrix} n \\ z \end{matrix} \right\}$$

impedanca: $z = \sqrt{\frac{\mu}{\epsilon}}$
impedanca praznega prostora: $z_0 = \sqrt{\frac{\mu_0}{\epsilon_0}}$

$$\sin \theta_L = \frac{n_1}{n_2} \sin \theta$$

majhen

$\sin \theta_L > 1$??? POPOLNI ODBOJ!

↓ majhen ← velik

$$k_{Lx}^2 + \beta^2 = k_2^2 \Rightarrow k_{Lx}^2 = k_2^2 - \beta^2 < 0$$

$$k_{Lx} = \pm j \sqrt{\beta^2 - k_2^2}$$

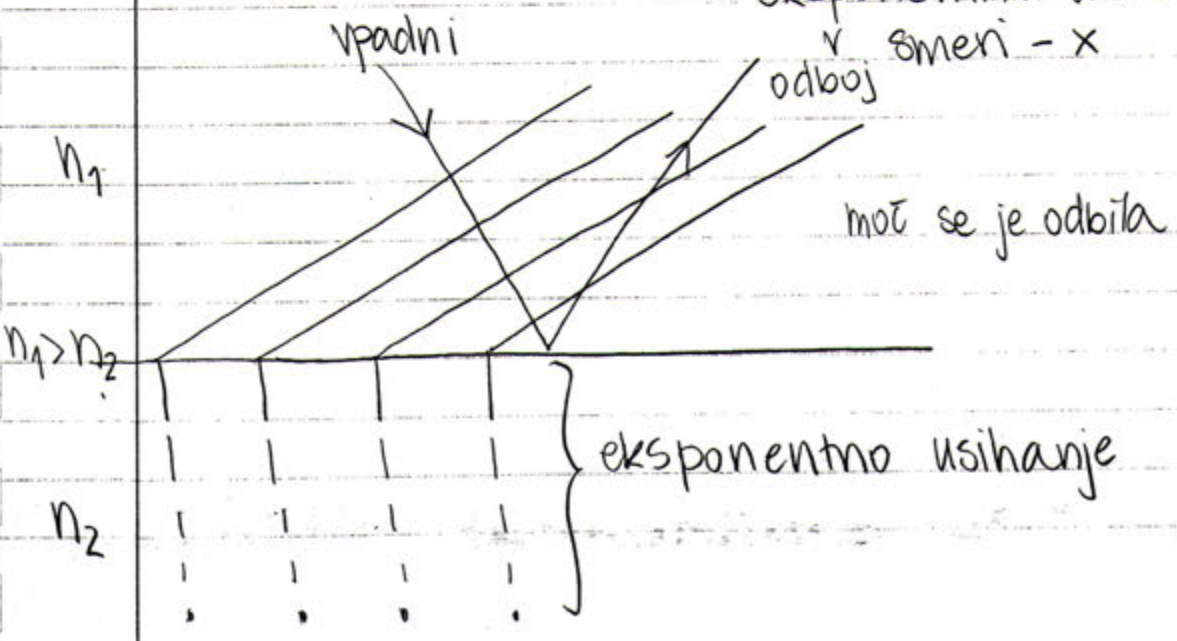
↑ čisto imaginarno

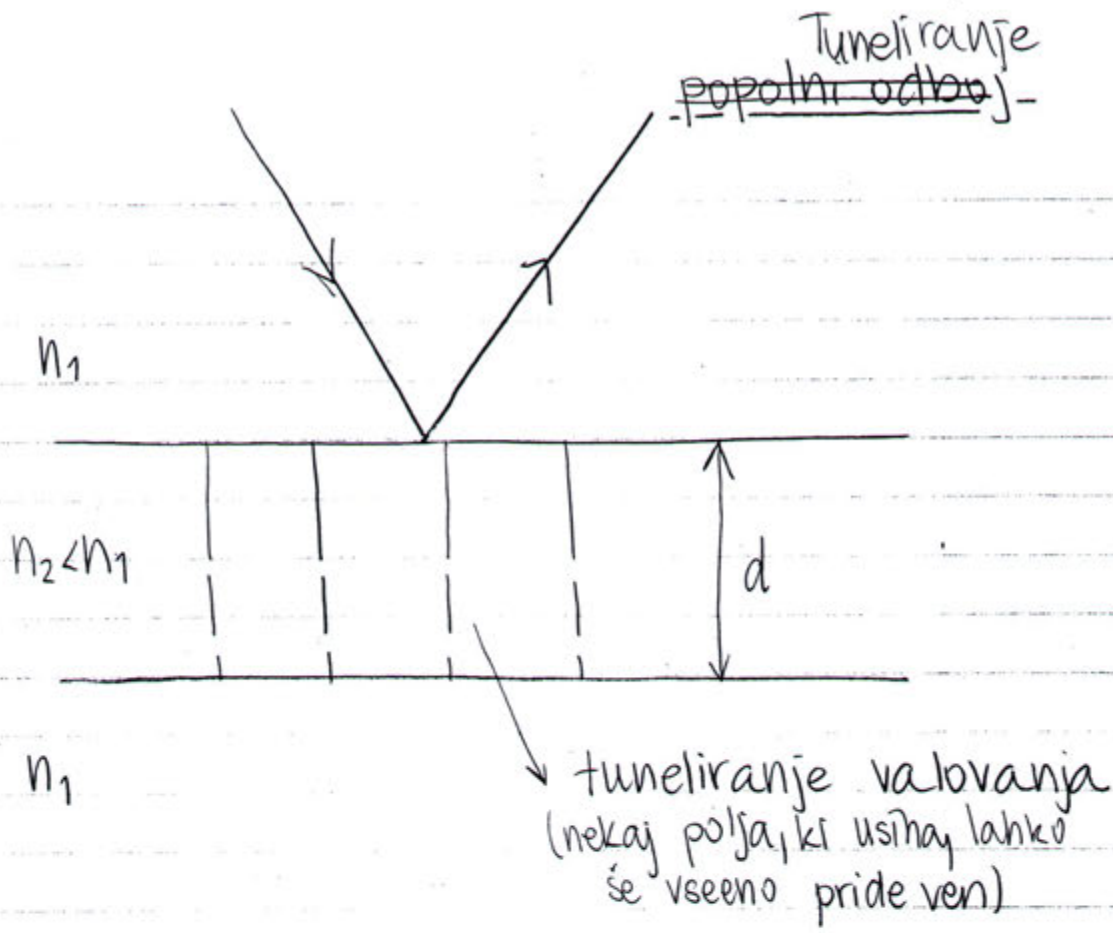
$$k_{Lx} = \pm j |k_{Lx}| \Rightarrow \vec{k}_L = \vec{i}_x \cdot j |k_{Lx}| + \vec{i}_z \cdot \beta$$

$$\Rightarrow \vec{E}_L = \vec{i}_{EL} \cdot C_L \cdot e^{jk_x x} e^{jk_z z} = \vec{i}_{EL} C_L e^{j(j|k_{Lx}|x)} e^{j\beta z} =$$

$$= \vec{i}_{EL} C_L e^{|k_{Lx}|x} e^{j\beta z}$$

↳ eksponentno usihanje v smeri -x





$$e^{ikx} + e^{-ikx} = \cos kx - j \sin kx + \cos kx + j \sin kx = \underline{2 \cos kx}$$

potujoči val

$$\vec{E} = \vec{E}_0 \cdot e^{j\vec{k}\cdot\vec{r}}$$

$$\vec{k} = \vec{k}_x + \vec{k}_y + \vec{k}_z$$

$$k_x^2 + k_y^2 + k_z^2 = k^2 = \omega^2 \mu \epsilon$$

$$\vec{k} \perp \vec{E} \quad \vec{E} \perp \vec{H}$$

$$\vec{k} \parallel \vec{S} \quad \vec{E} \perp \vec{H} \perp \vec{k}$$

$$\vec{\nabla} = -j\vec{k}$$

velja samo za en sam potujoči val

1D Stojni val

$$\vec{E} = \vec{E}_0 \cdot \cos kz = \vec{E}_0 \cdot C (e^{jkz} + e^{-jkz}) \frac{1}{2}$$

? valovni vektor valovni vektor

$$z = \sqrt{\frac{\mu}{\epsilon}}$$

\vec{E}, \vec{H} v kvadraturi

$$\vec{H} = \frac{1}{\omega \mu} \begin{vmatrix} \vec{k}_x & \vec{k}_y & \vec{k}_z \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \end{vmatrix} = \vec{k}_y \frac{jC}{\omega \mu} (-\sin kz) = -j \vec{k}_y \frac{C}{z} \sin kz$$

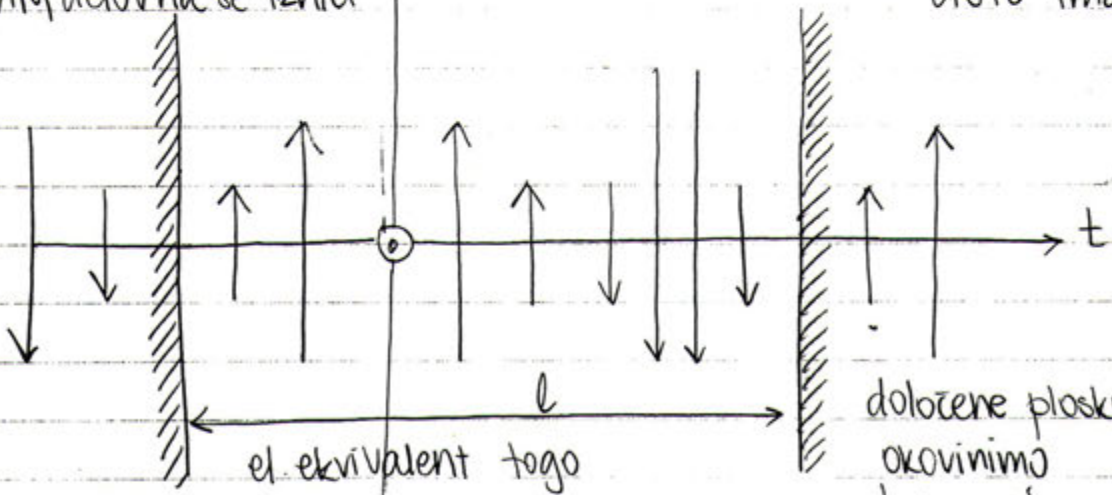
Pri stojnem valu sta si el. in mag. polje v kvadraturi (-j je 90° faznega zasuka). Aja sta bila sofazna.

$$\vec{S} = \frac{1}{2} \vec{E} \times \vec{H}^* = \frac{1}{2} \vec{k}_x C \cos kz \times (+j \vec{k}_y) \frac{C^*}{z} \sin kz = j \vec{k}_z \frac{C \cdot C^*}{2z} \cos kz \sin kz$$

Imamo samo jalovo

čisto imaginaren

komponento, delovna se izniči



el. ekvivalent toga opete strune

določene ploskve lahko okovinjimo

↳ tiste, ki nimajo tangencialne komponente

$$\vec{E}_t = 0 \Rightarrow \text{kovina}$$

$$\vec{E}_t = 0 \Rightarrow \text{kovina tangencialne komponente}$$

Fabry-Perot-ov rezonator

Kovinskih plošč ne moremo postavljati na poljubno razdaljo oz. če imamo plošče na določeni razdalji, bo to dobro samo za določen k oz. frekvenco

$$kl = m\pi; m = 1, 2, 3, 4 \dots \quad m\pi = kl = \frac{\omega}{c_0} l = \frac{2\pi f}{c_0} l \Rightarrow \underline{f = m \frac{c_0}{2l}}$$

Zrcalo #1

Zrcalo #2

Ojačevalna snov
vzbujen HE

μ_0, ϵ_0

l

svetloba niha, želimo da vsaj ena izmed frekvenc svetlobe pade med resonančne frekvence

$$\Delta f = \frac{c_0}{2l} = \frac{3 \cdot 10^8 \text{ m/s}}{2 \cdot 0,33 \text{ m}} = 4,5 \cdot 10^8 \text{ s}^{-1} = \underline{450 \text{ MHz}}$$

$l = 33 \text{ cm}$

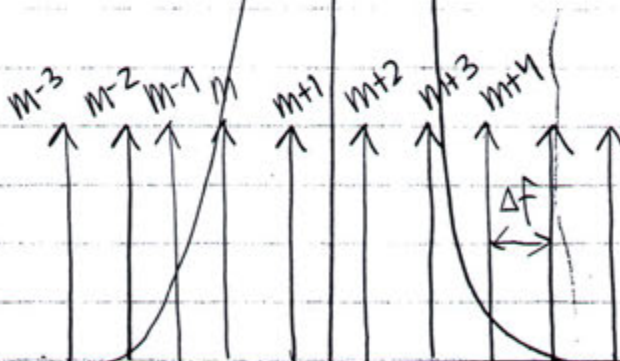
$G(f)$

TEM_{00m}
xy z → št. robov

ojačenje

širina ojačanja niha na

$\sim 1 \text{ GHz} \Rightarrow$ 2 ali 3 robovih $\rightarrow m-1, m, m+1$



SS

474 THz (rdeča svetloba $\lambda \sim 633 \text{ nm}$)

Izgubni kabel:

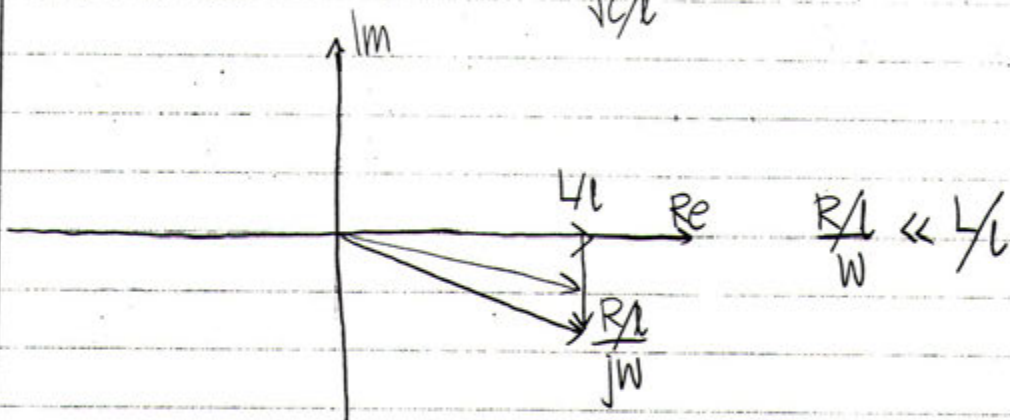
$$Z_k = \frac{\sqrt{L/l + \frac{R/l}{j\omega}}}{\sqrt{C/l}} \approx \sqrt{\frac{L/l}{C/l}}$$

$$K = \omega \sqrt{\left(L/l + \frac{R/l}{j\omega}\right) \cdot C/l} = \beta + j\alpha$$

$\beta \approx \omega \sqrt{L/l + C/l}$
 $\alpha \neq 0$

$$\alpha = \beta \cdot \frac{R/l}{2\omega L/l} = \omega \sqrt{L/l \cdot C/l} \frac{R/l}{2\omega L/l}$$

$$= \frac{R/l}{2\sqrt{L/l}} = \frac{R/l}{2Z_k}$$



$$\sqrt{1+x} \approx 1 + \frac{x}{2}$$

$x \ll 1$

$$K = \omega \sqrt{\left(L/l + \frac{R/l}{j\omega}\right) (C/l)} = \omega \sqrt{\left(L/l\right) (C/l) \left(1 - j \frac{R/l}{\omega L/l}\right)}$$

$$\approx \omega \sqrt{\left(L/l\right) (C/l)} \left(1 - j \frac{R/l}{2\omega L/l}\right)$$

$$\alpha = \frac{R/l}{2Z_k} \quad ; \quad U(l) = U(0) e^{j\omega l} e^{-\alpha l}$$

$$a_{\frac{dB}{m}} = 20 \log_{10} \left| \frac{U(0)}{U(l)} \right| = 20 \log_{10} e^{\alpha l} \text{ [dB]}$$

$$a = \frac{Z_0}{\ln 10} \quad \alpha l = \frac{Z_0}{\ln 10} \frac{R/L}{2Z_c} l$$

$$a/l = \frac{10}{\ln 10} \frac{R/L}{Z_c} \quad \left[\frac{\text{dB}}{\text{m}} \right]$$

$$Z_c = \frac{Z_0}{2\pi\sqrt{\epsilon_r}} \ln \frac{R_0}{R_z}$$

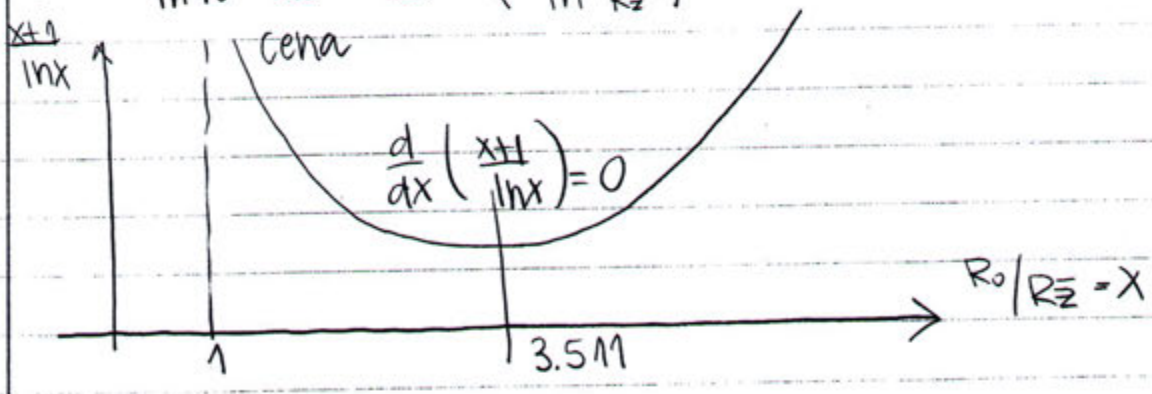
$$R/L = R_z/l + R_0/l = \frac{1}{2\pi R_z \delta \gamma_{cu}} + \frac{1}{2\pi R_0 \delta \gamma_{cu}}$$

$$R/l = \frac{1}{2\pi} \frac{\sqrt{WM}}{\sqrt{2\gamma_{cu}}} \left(\frac{1}{R_z} + \frac{1}{R_0} \right)$$

$$a/l = \frac{10}{\ln 10} \frac{\frac{1}{2\pi} \frac{\sqrt{WM}}{\sqrt{2\gamma_{cu}}} \left(\frac{1}{R_z} + \frac{1}{R_0} \right)}{\frac{Z_0}{2\pi\sqrt{\epsilon_r}} \ln \frac{R_0}{R_z}} = \frac{10}{\ln 10} \sqrt{\epsilon_r} \frac{\sqrt{WM}}{Z_0} \frac{\left(\frac{1}{R_z} + \frac{1}{R_0} \right)}{\ln \frac{R_0}{R_z}} \quad \left[\frac{\text{dB}}{\text{m}} \right]$$

$\epsilon_r \gg 1$; votel dielektrik (penast dielektrik)
 cena $\sim R_0^2$

$$a/l = \frac{10}{\ln 10} \frac{\sqrt{\epsilon_r}}{R_0} \frac{\sqrt{WM}}{Z_0} \left(\frac{\frac{R_0}{R_z} + 1}{\ln \frac{R_0}{R_z}} \right) \quad \left[\frac{\text{dB}}{\text{m}} \right]$$



$f = 100 \text{ MHz}$ $\delta = 6.8 \cdot 10^{-6} \text{ m}$ $R_z = 0.5 \text{ mm}$ $\epsilon_r = 2$ polietilen
 $\gamma_{cu} = 56 \cdot 10^6 \text{ s/m}$ $R_0 = 1.75 \text{ mm}$ $Z_c = 50 \Omega$ @ $\frac{R_0}{R_z} = 3.5$

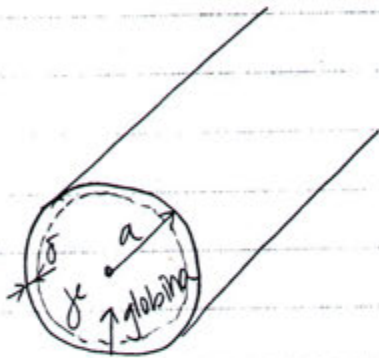
$$R_p = \sqrt{\frac{W}{2\gamma}} = \frac{1}{\delta\gamma} = \frac{1}{380} = \underline{\underline{2.6 \text{ m}\Omega}}$$

$$R/l = \frac{1}{2\pi} \cdot \overbrace{2.6 \text{ m}\Omega}^{R_p} \left(\frac{1}{R_z} + \frac{1}{R_0} \right) = \frac{1}{2\pi} \cdot 2.6 \cdot 10^3 \Omega \left(\frac{10^3}{0.5 \text{ m}} + \frac{10^3}{1.75 \text{ m}} \right) \approx \underline{\underline{1 \Omega/\text{m}}}$$

$$a/l = \frac{10}{\ln 10} \cdot \frac{R/l}{Z_c} = \frac{10}{2.305} \frac{1 \Omega/\text{m}}{50 \Omega} \Rightarrow a/l = 0.08 \frac{\text{dB}}{\text{m}} = \underline{\underline{8 \text{ dB}/100 \text{ m}}}$$

dober prevodnik: $\gamma \gg \omega \epsilon$

$$\delta = \sqrt{\frac{2}{\omega \mu \gamma}}$$



Cu
 $f = 100 \text{ MHz}$
 $\delta = 6.8 \mu\text{m}$

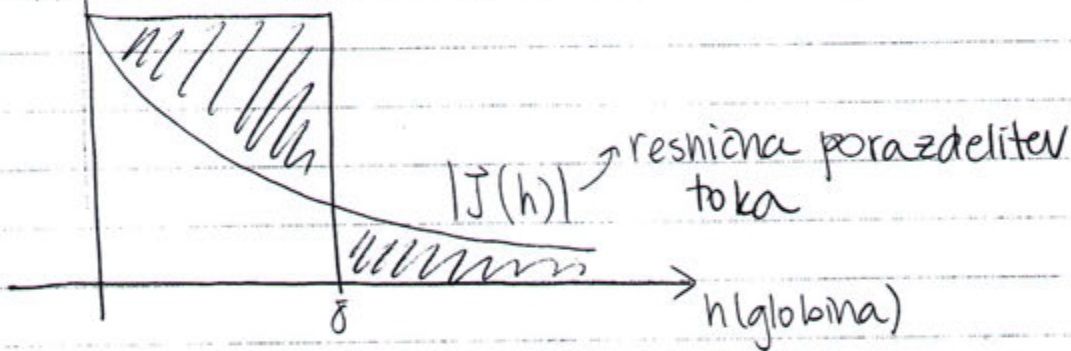
upornost žice
 z enosmerno

$$R = \frac{l}{\pi a^2} \cdot \frac{1}{\gamma}$$

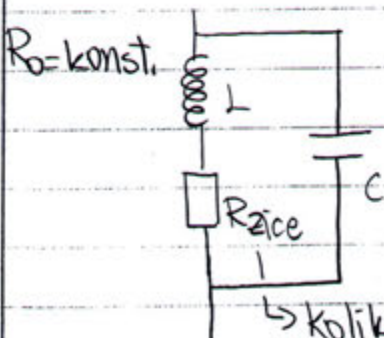
upornost žice
 z izmenično

$$R_w = \frac{l}{2\pi a \delta} \cdot \frac{1}{\gamma} > R; R_w = R_0 \sqrt{\omega}$$

$|J(h)|$



RESNIČNA TULJAVA

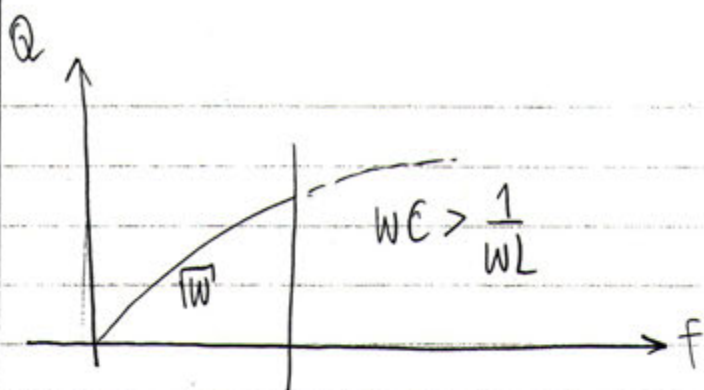


$$Q = \frac{\omega L}{R_{\text{zice}}} = \frac{\omega L}{R_0 \sqrt{\omega}} = \frac{L}{R_0} \sqrt{\omega}$$

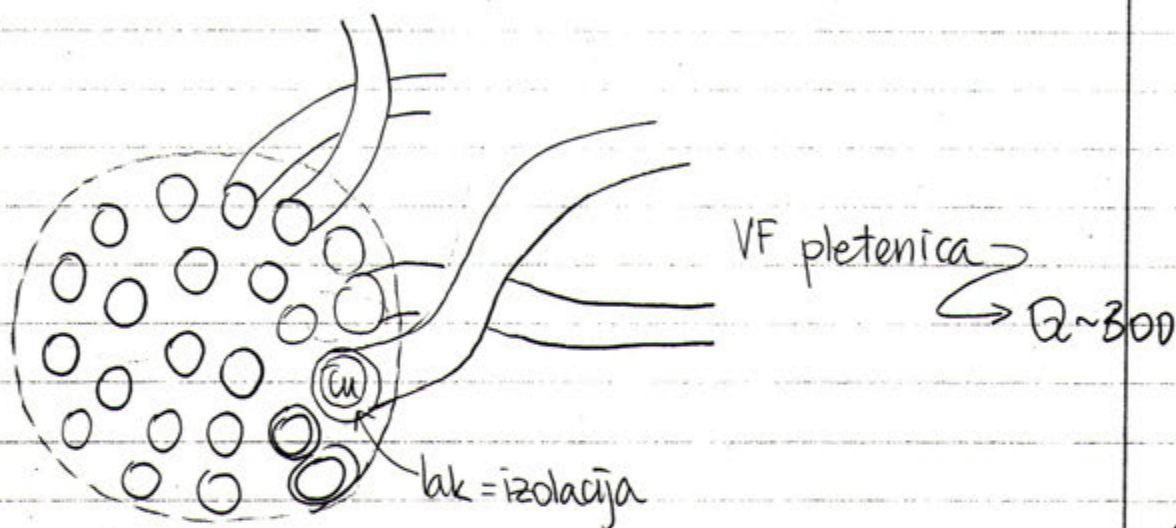
tuljava Cu žica

Mjedra = μ : $Q \sim 100$

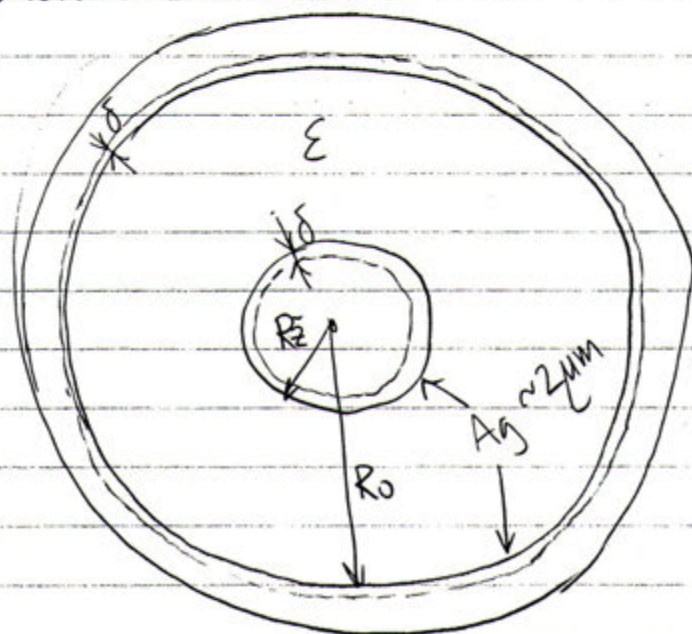
↳ koliko je kvaliteta tuljave (omejuje kvaliteto)



Kako povečamo kvaliteto tuljave?
 ↳ naredimo žico iz več vodnikov



koaksialen kabel.



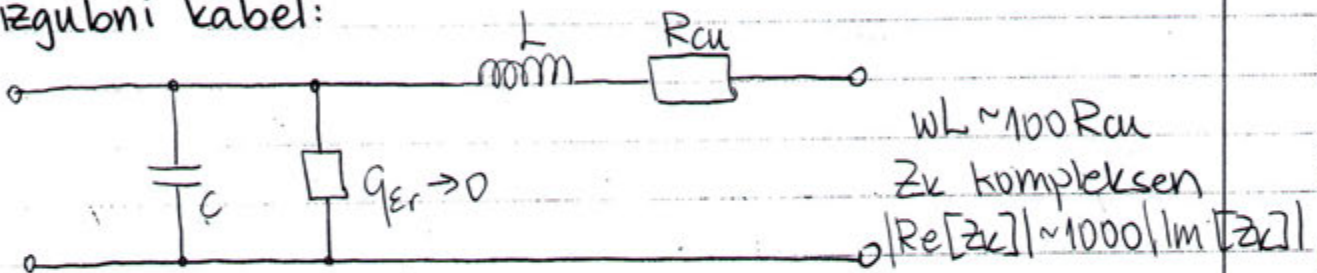
karakteristična impedanca:

$$Z_c \approx \frac{Z_0}{2\pi\sqrt{\epsilon_r}} \ln \frac{R_o}{R_z} \quad (\text{brezizgubni kabel})$$

$$Z_0 = \sqrt{\frac{\mu_0}{\epsilon_0}} = 120\pi \Omega$$

$$\Rightarrow Z_c \approx \frac{60\Omega}{\sqrt{\epsilon_r}} \ln \frac{R_o}{R_z}$$

izgubni kabel:

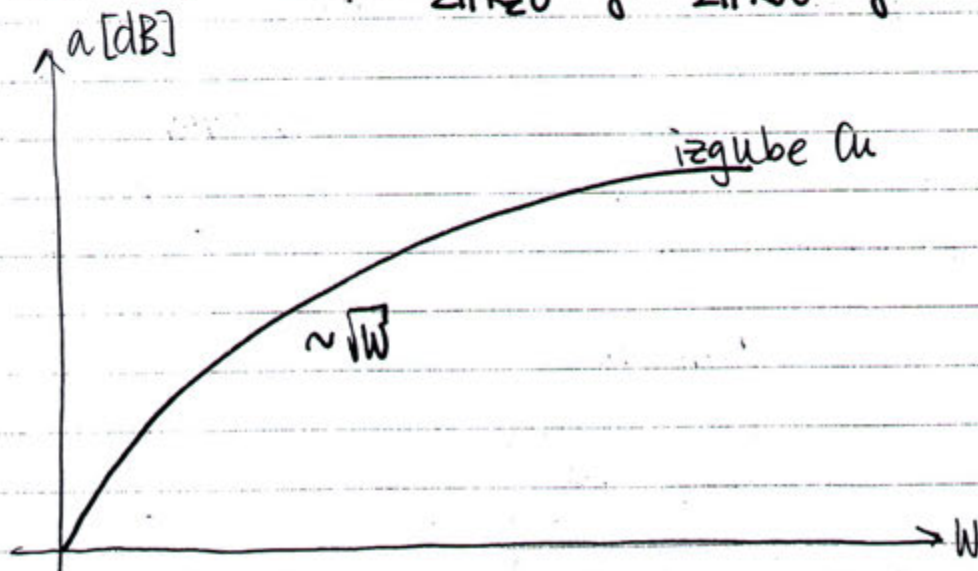


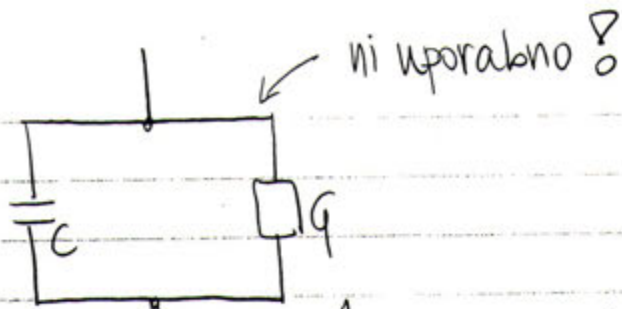
slabljenje kabla: ^{konst.}

$$a[\text{dB}] = \frac{10}{\ln 10} \frac{R/l}{Z_c} \cdot l = C_a \sqrt{\epsilon_r} \sqrt{W} \frac{1}{R_o} \left(\frac{R_o/R_z + 1}{\ln(R_o/R_z)} \right)$$

minimum
 $R_o/R_z = 3.5M$

$$R_{cu} = R_{zile} + R_{oklopa} = \frac{l}{2\pi R_z \delta} \cdot \frac{1}{\gamma} + \frac{l}{2\pi R_o \delta} \cdot \frac{1}{\gamma}$$



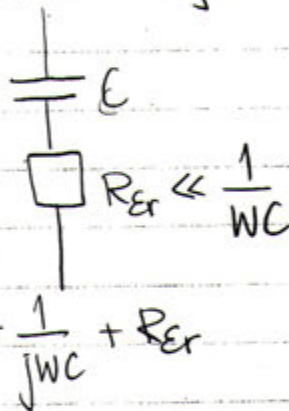
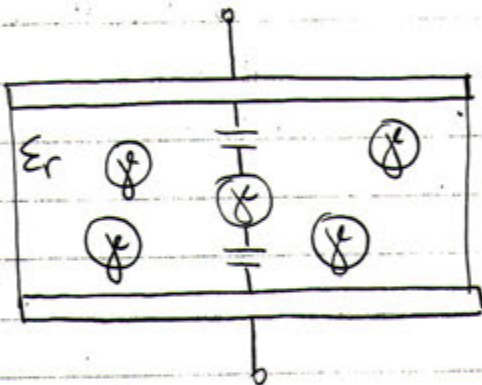


$$Y = \frac{1}{Z} = \frac{1}{\frac{1}{j\omega C} + R_{er}} = \frac{j\omega C}{1 + j\omega C R_{er}} \approx j\omega C + R_{er} \omega^2 C^2$$

$\underbrace{\hspace{10em}}_{\text{zanemarimo}}$

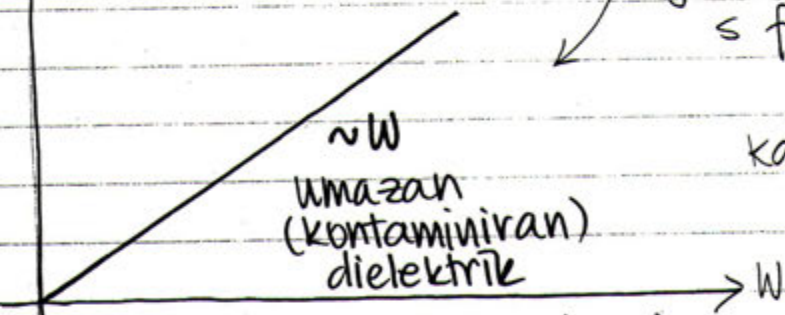
$$Y = j\omega C (1 - j R_{er} \omega C)$$

slab dielektrik
resnično vezje:



$$Z = \frac{1}{j\omega C} + R_{er}$$

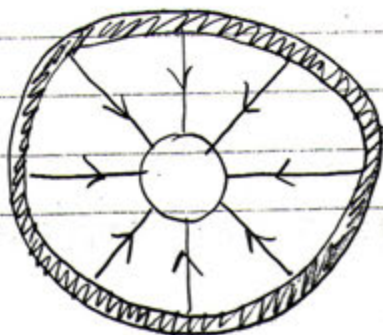
$a[\text{dB}]$



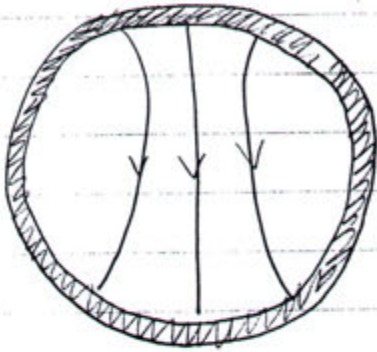
izgube premo sorazmerne
s frekvenco

kako ugotovimo ali
je kabel dober? ▽
- izmerimo potek ○

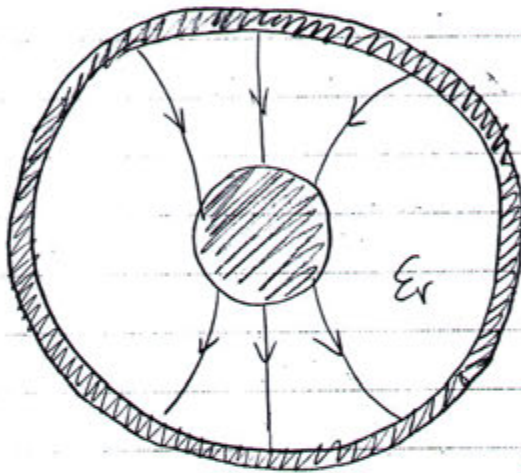
kabel z majhnimi izgubami
min a ⇒ max Roklopa?



TE1 mod: način razširjanja

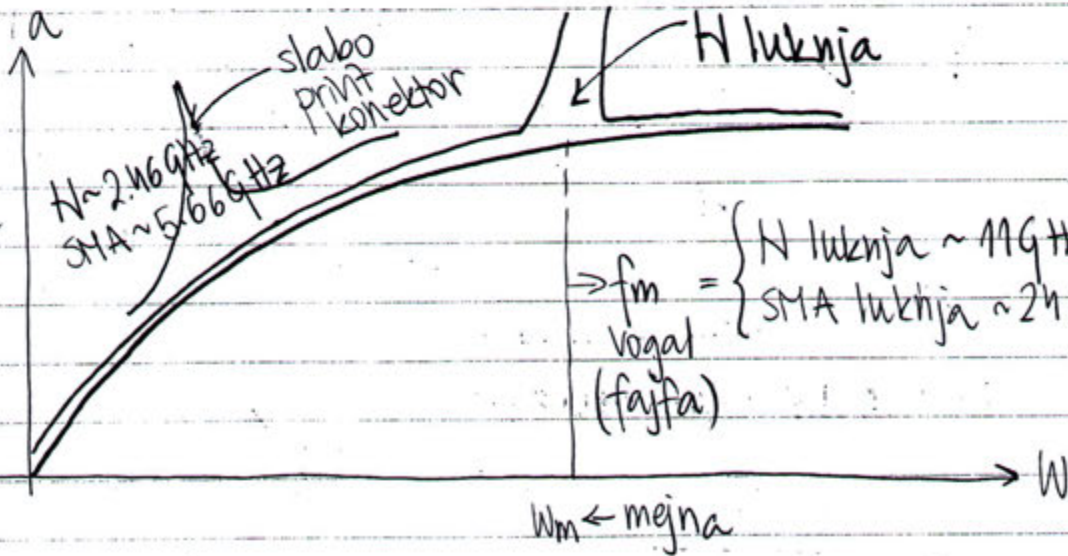


rod TE₁₁ (f, ρ, z)
 ustreza TE₁₀ v $\underbrace{\quad}_?$ snovi
 $f_m > 0$



ustreza rodu TE₁₁ v koaksu
 $R_{\text{zile}} = 0.5 \text{ mm}$
 $R_{\text{oklopa}} = 1.75 \text{ mm}$
 $\epsilon_r = 2$

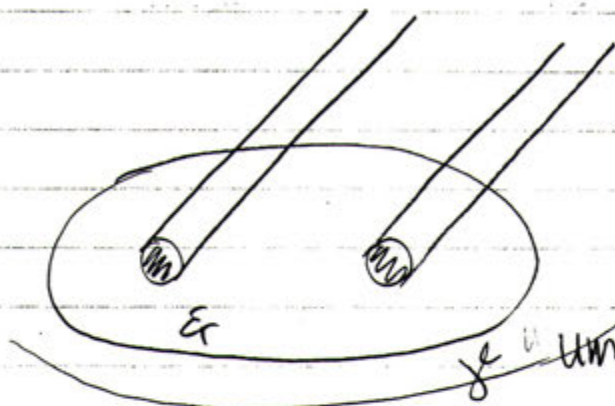
$$f_m = \frac{c/\sqrt{\epsilon_r}}{\pi(R_{\text{zile}} + R_{\text{oklopa}})} = \frac{3 \cdot 10^8 \text{ m/s}}{\sqrt{2}} \cdot \frac{1}{\pi(0.5 \cdot 10^{-3} \text{ m} + 1.75 \cdot 10^{-3} \text{ m})} = \frac{3 \cdot 10^8 \text{ Hz} \cdot 10^3}{\sqrt{2} \cdot \pi \cdot 2.25} \approx \underline{\underline{30 \text{ GHz}}}$$



navadni dvovod:

TEM (osnovni mod) + višji modi !

palica
Ethernet

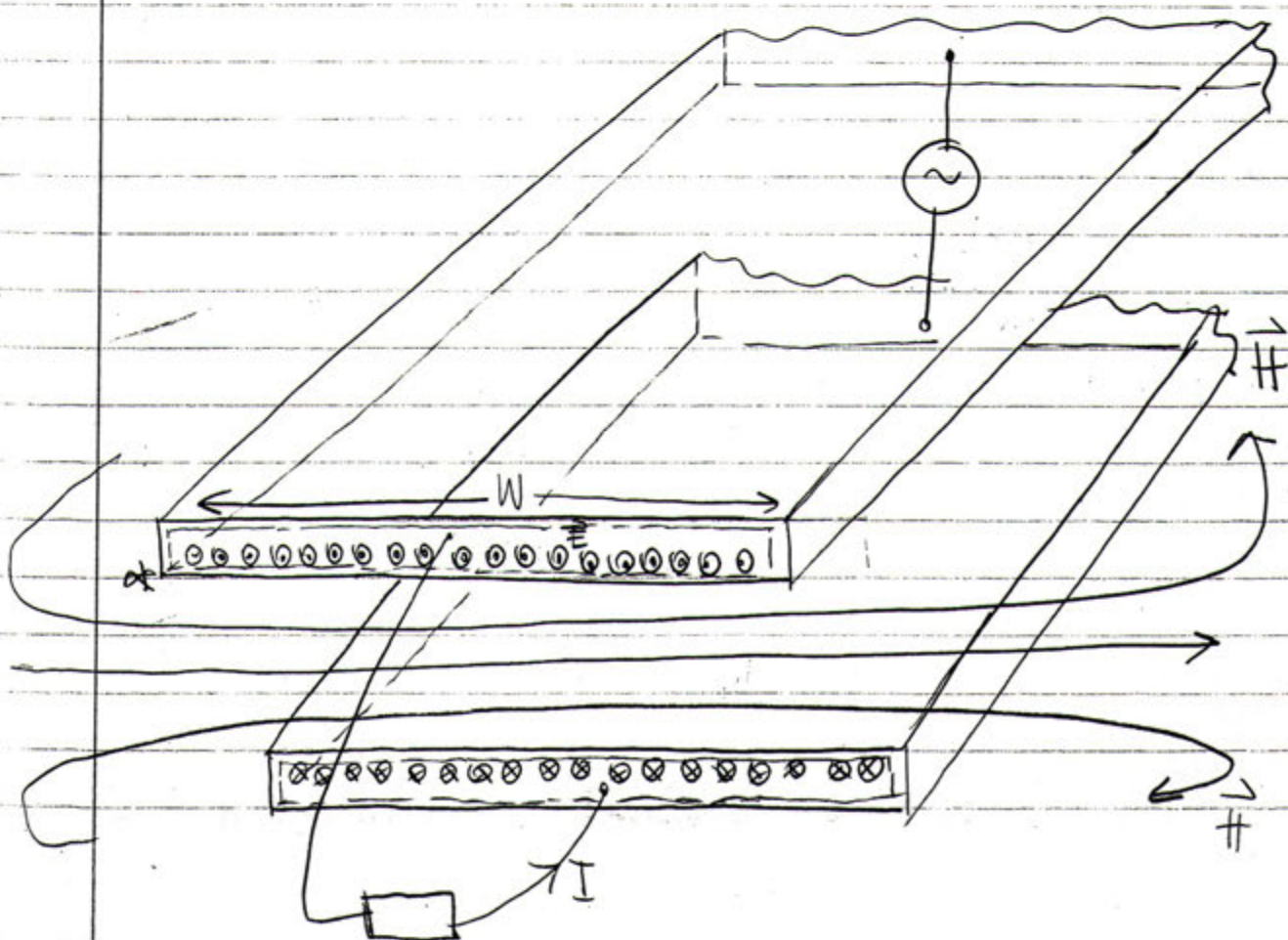
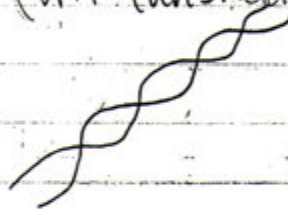


$R_{\text{dovoda}} \sim 2 \cdot R_{\text{kabla}}$

$Z_{\text{dovoda}} \sim 1/2 Z_{\text{kabla}}$

$\alpha_{\text{dovoda}} \sim \frac{1}{2} \alpha_{\text{kabla}}$

brez olopa
(UTP (unshielded twisted pair))



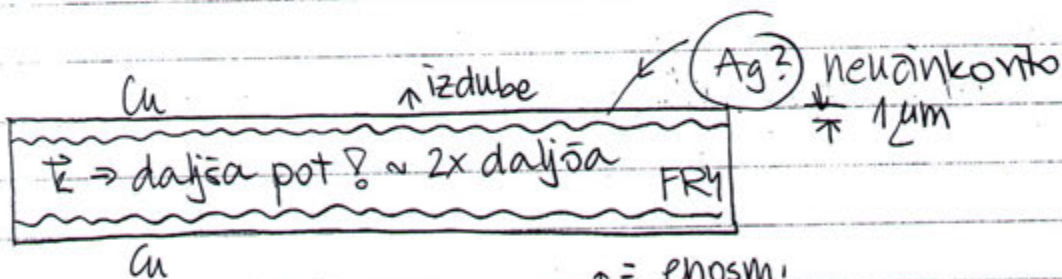
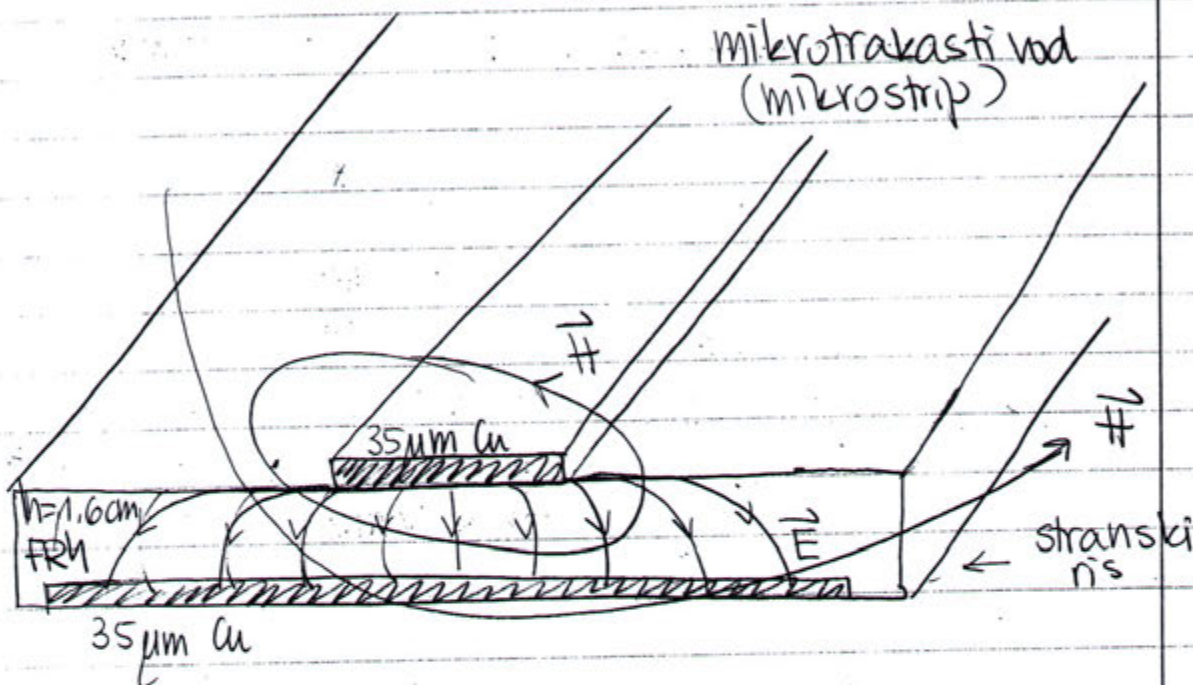
R posameznega vodnika

$$* R_g = \frac{l}{W\delta} \cdot \frac{1}{\gamma}$$

$$R_s = \frac{l}{W\delta} \cdot \frac{1}{\gamma}$$

$$Z_k = \frac{h}{W} \sqrt{\frac{\mu}{\epsilon}} = \frac{h}{W} \frac{Z_0}{\sqrt{\epsilon_r}}$$

↳ brez stresanja $w \gg h$



navadno tiskano vezje

$$\epsilon_r: FR4 = \begin{cases} < 1 \text{ MHz } \epsilon_r \sim 5 \\ 100 \text{ GHz } \epsilon_r \sim 4 \end{cases}$$

$$FR4 \epsilon_r = 4.6$$

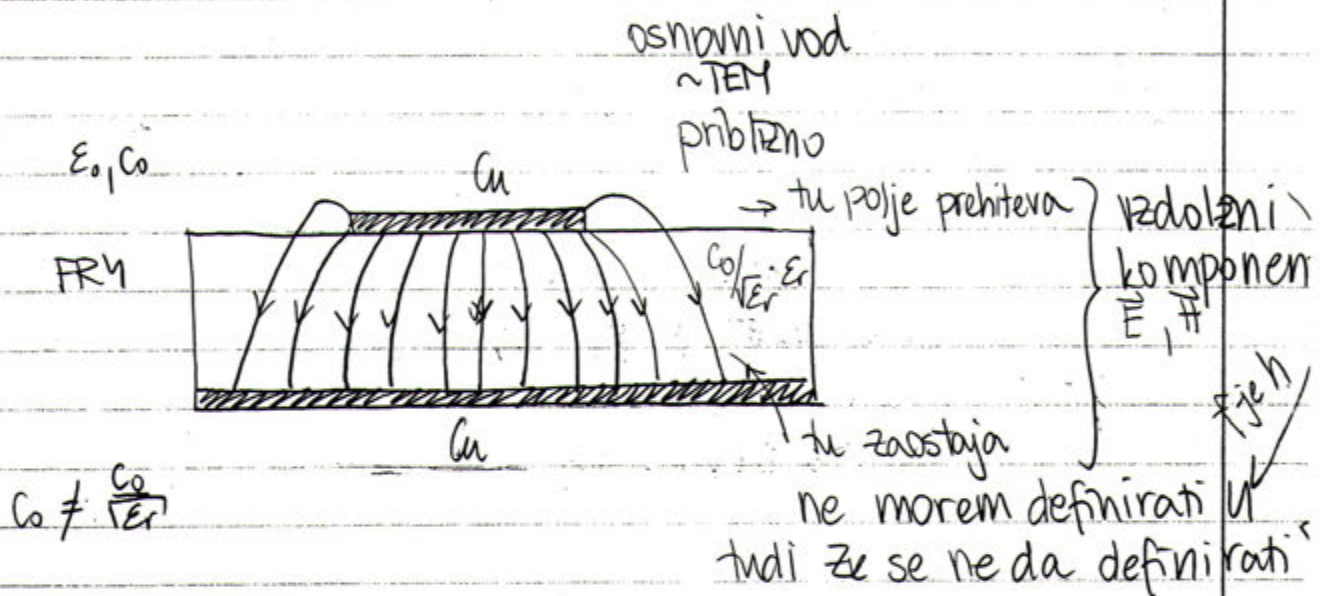
$Z_k = 50 \Omega \Rightarrow$ MORANO UPOŠTEVATI STRESANJE ∇

$$W = \frac{h}{Z_k} \cdot \frac{Z_0}{\sqrt{\epsilon_r}} = \frac{1.6 \text{ cm}}{50} \cdot \frac{120 \pi \Omega}{\sqrt{4.6}} = 1.6 \cdot 3.5 \text{ cm} = \underline{5.5 \text{ cm}} \quad ? \text{ NAROBE } \nabla$$

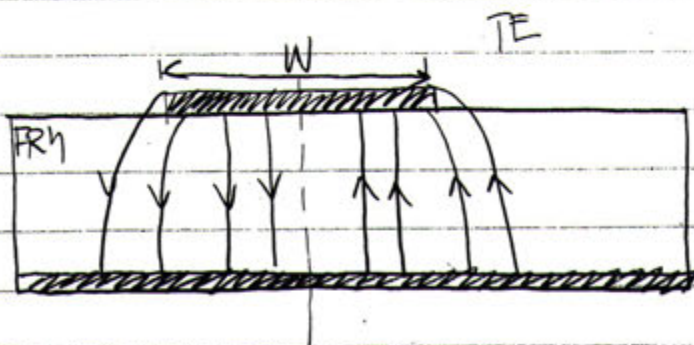
razmerje premajhno $\frac{W}{h} = 3.5$

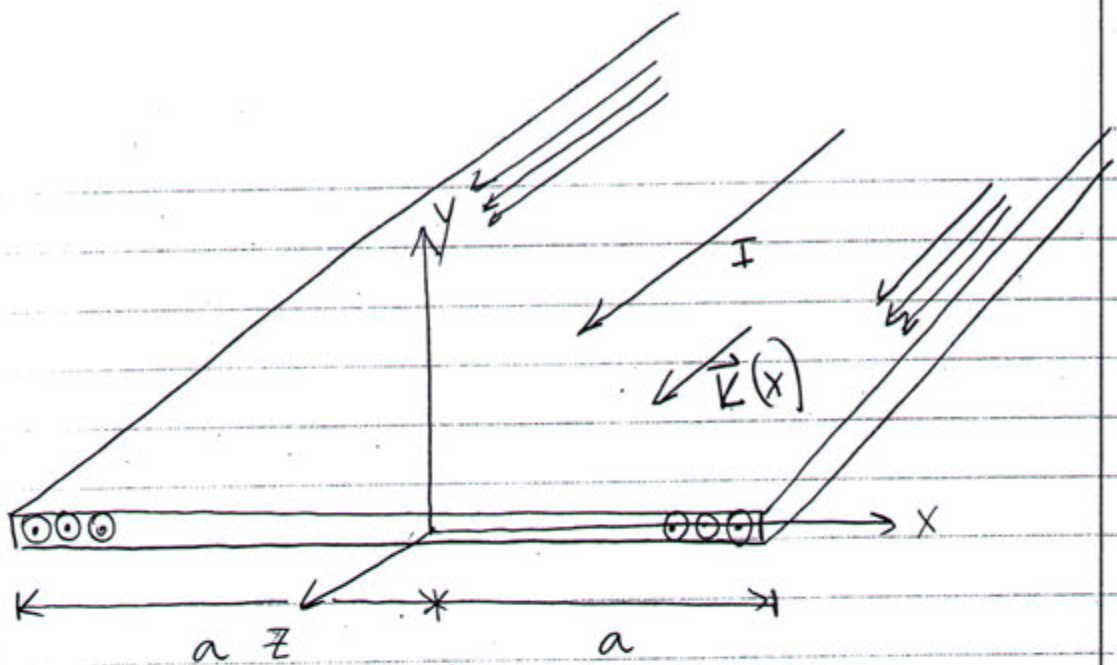
stresanje $\left. \begin{matrix} c/l \uparrow \\ l/l \downarrow \end{matrix} \right\} Z_c = \sqrt{\frac{l/c}{c/l}} \downarrow$ ZARADI STRESANJA

Wheelerjevi približki $Z_c = 50 \Omega$ $\frac{W}{h} \approx 2$
 FR4: $\epsilon_r \approx 4.5$
 teflonski laminat $\epsilon_r \approx 2.5$ $\frac{W}{h} \approx 3$



Naslednji višji red \rightarrow fja W



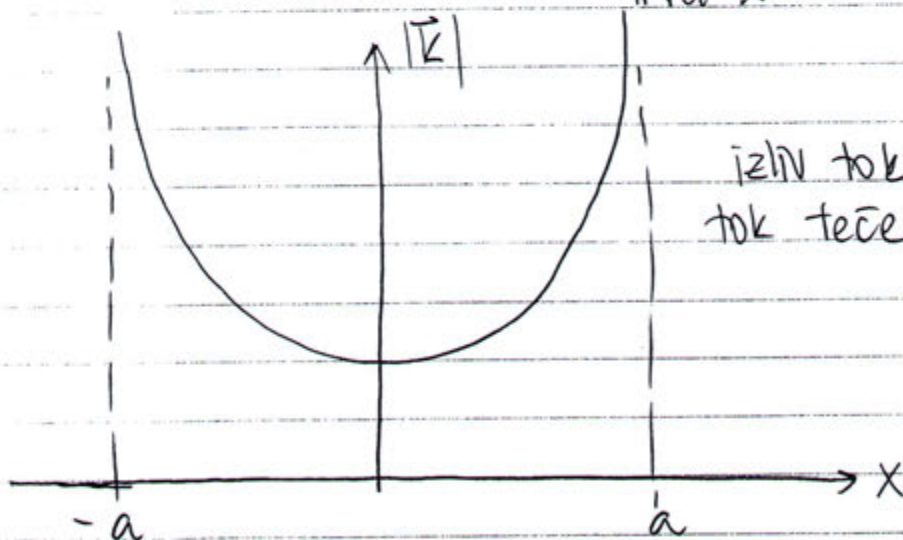


vektorski potencial: $\vec{A} = \vec{1}_z A_z$
 na vodniku $\frac{\partial A_z}{\partial x} = 0$

vajni eliptični koordinatni sistem

$$\left. \begin{aligned} x &= a \cdot \cosh u \cdot \cos v \\ y &= a \cdot \sinh u \cdot \sin v \end{aligned} \right\} \frac{\partial}{\partial v} = 0$$

$$\Rightarrow \vec{E}(x) = \vec{1}_z \frac{I}{\pi \sqrt{a^2 - x^2}}$$



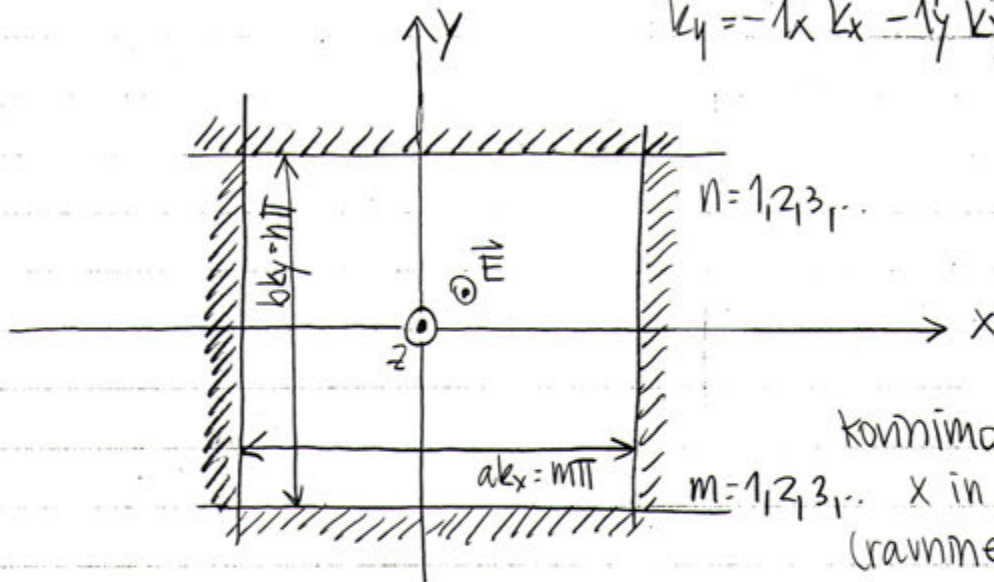
| Vrsta voda | slabljenje |
|-------------------|-------------------------|
| koaks | $\sim 0.1 \text{ dB/m}$ |
| @ 1GHz | |
| mikrotrakasti vod | $\sim 1 \text{ dB/m}$ |

2D stojni val

$$\vec{E} = \vec{1}_z C \cos k_x x \cdot C \cdot \cos k_y y = \vec{1}_z C \cdot \frac{1}{2} (e^{jk_x x} + e^{-jk_x x}) \cdot \frac{1}{2} (e^{jk_y y} + e^{-jk_y y})$$

$$k_x^2 + k_y^2 = k^2 = \omega^2 \mu \epsilon$$

$$\begin{aligned} \vec{k}_1 &= \vec{1}_x k_x + \vec{1}_y k_y && \text{iz štirih} \\ \vec{k}_2 &= -\vec{1}_x k_x + \vec{1}_y k_y && \text{valov lahko} \\ \vec{k}_3 &= \vec{1}_x k_x + \vec{1}_y k_y && \text{sestavimo 2D} \\ \vec{k}_4 &= -\vec{1}_x k_x - \vec{1}_y k_y && \text{stojni val} \end{aligned}$$



$$k_x = \frac{m\pi}{a}$$

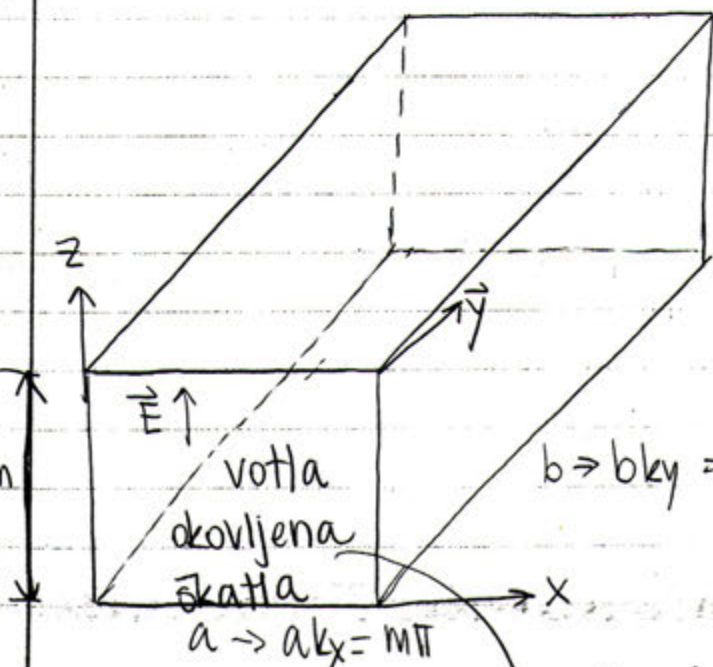
$$k_y = \frac{n\pi}{b}$$

konmimo lahko po
x in y osi
(ravnote \perp na x in
ravnote \perp na y)

$$k^2 = \left(\frac{m\pi}{a}\right)^2 + \left(\frac{n\pi}{b}\right)^2 = \frac{\omega^2}{c_0^2} = \left(\frac{2\pi f}{c_0}\right)^2$$

$$f = \frac{c_0}{2} \sqrt{\left(\frac{m}{a}\right)^2 + \left(\frac{n}{b}\right)^2}$$

najmanjša f m=1, n=1



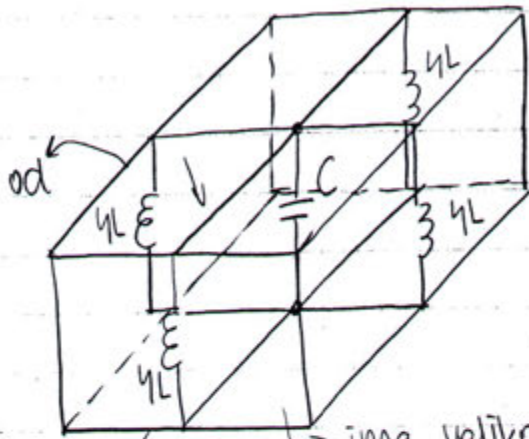
votlinski rezonator

3D Stojni val TM_{011}

$$\left. \begin{matrix} \vec{E} \parallel \vec{z} \\ \vec{H} \perp \vec{z} \end{matrix} \right\} TM_{0nm} \begin{matrix} zyx \\ zyx \end{matrix}$$

RESONANCE
ZA WOLNISKI
REZONATOR

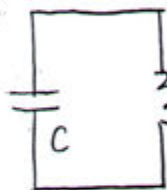
val se odbija od sten in krozi



$$f = \frac{c_0}{2} \sqrt{\left(\frac{m}{a}\right)^2 + \left(\frac{n}{b}\right)^2 + \left(\frac{l}{c}\right)^2}$$

($\sqrt{\epsilon_r}$)

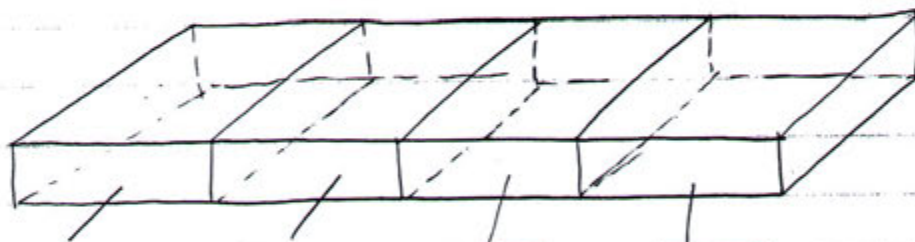
ima veliko resonančnih frekvenc za različne n m l



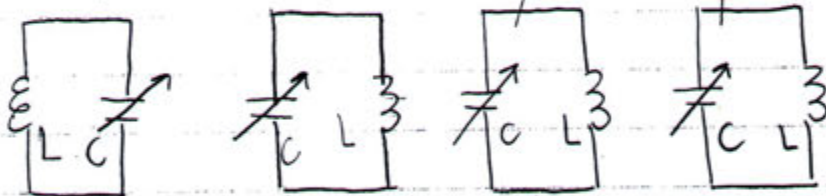
nihajni krog

3D rezonator \rightarrow 8 valov

4 rezonatorji



TM_{011}
 $a = 3,5 \text{ cm}$
 $b = 2,4 \text{ cm}$
 $c = 1,6 \text{ cm}$



a in b dasta najmanjšo resonančno frekvenco

pasivno sito f_0

\rightarrow vijaki nastavljajo kapacitivnost
 \rightarrow vijaki za nastavljanje induktivnosti

$Im(\vec{z})$ $y \rightarrow$ stojni val k_y
 $Re(\vec{z})$ $z \rightarrow$ potujoči val ($\beta = k_z$)

$$\vec{E}_1 = -\vec{y} k_y + \vec{z} \beta \quad \vec{E}_2 = \vec{y} k_y + \vec{z} \beta$$

$$\vec{E} = \vec{z} \cdot C \cos k_y y e^{-j\beta z} = \vec{z} \cdot C \frac{1}{2} (e^{jk_y y} + e^{-jk_y y}) e^{-j\beta z}$$

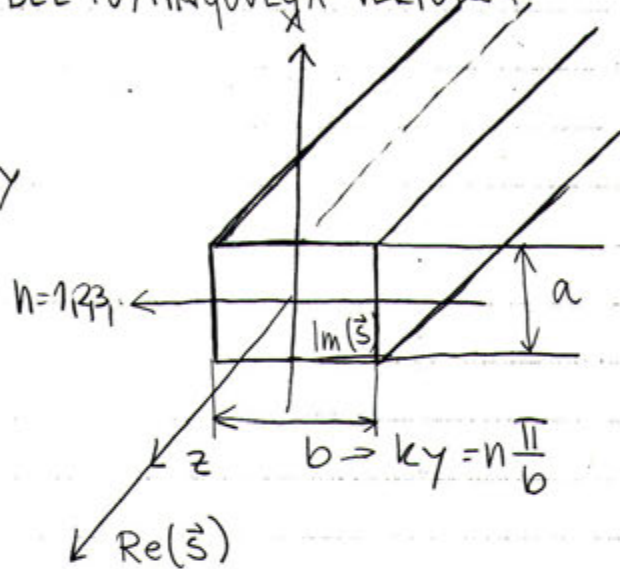
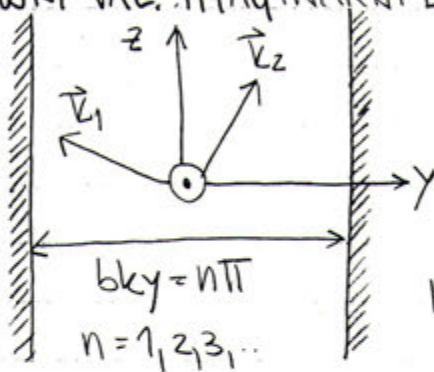
$$\vec{H} = \frac{j}{\omega \mu} \begin{vmatrix} \vec{z} & \vec{y} & \vec{z} \\ \partial/\partial x & \partial/\partial y & \partial/\partial z \\ \cos k_y y e^{-j\beta z} & 0 & 0 \end{vmatrix} =$$

komponenti sta med sabo v kvadraturi

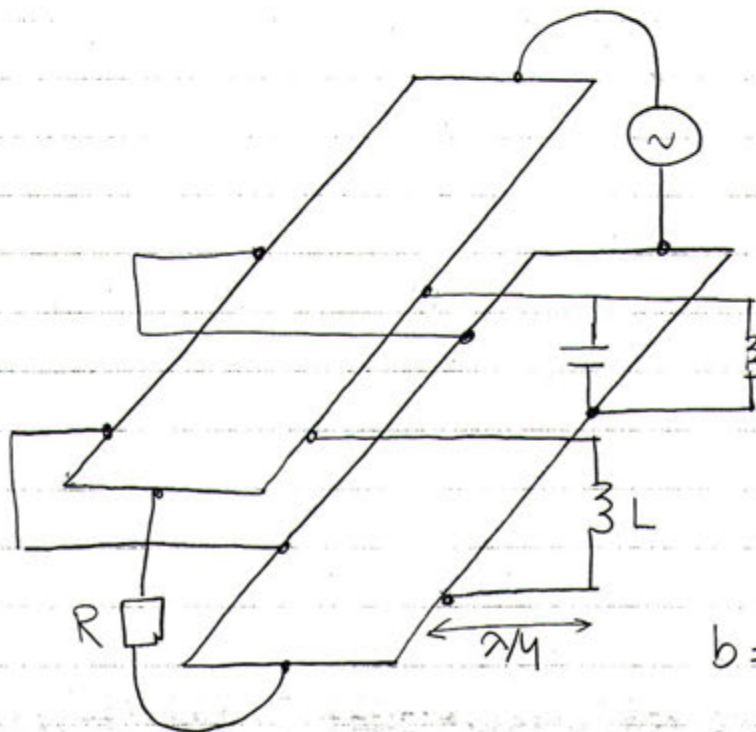
$$= \vec{1}_y \frac{-\beta}{\omega \mu} \cos ky y e^{j\beta z} + \vec{1}_z \frac{jky}{\omega \mu} \sin ky y e^{j\beta z}$$

$$\vec{S} = \frac{1}{2} \vec{E} \times \vec{H}^* = \vec{1}_z \frac{\beta}{\omega \mu} \cos^2 ky y + \vec{1}_y \frac{jky}{\omega \mu} \cos ky y \sin ky y$$

POTOJOČI VAL. REALNI DEL POYTINGOVEGA VEKTORJA
 STUJNI VAL. IMAGINARNI DEL POYTINGOVEGA VEKTORJA



b. omejen
 a. ni omejen



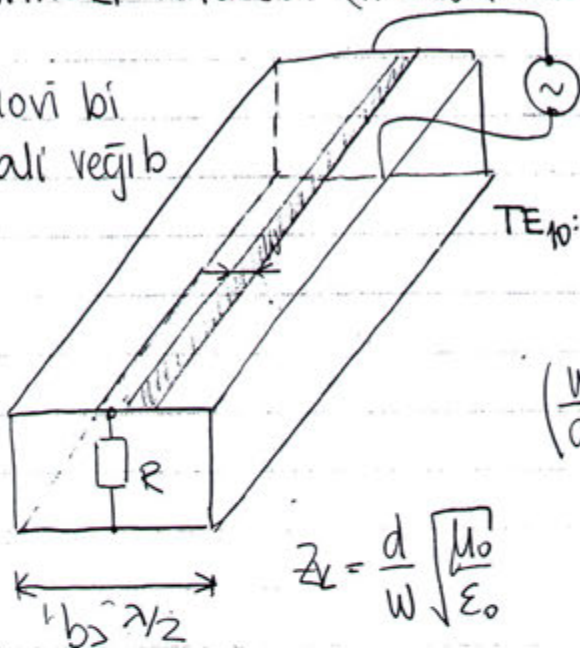
DRSTIČNIKI... njihov vpliv
 Izračunamo, ko LMC
 spravimo v resonanco

L_C resonanca

$$b = \frac{\lambda}{4} + w + \frac{\lambda}{4}$$

če imamo dovolj drstičnikov dobimo pravokotno cev
kovinski valovod (metal waveguide):

višji rodovi bi
potrebovali večji b



$$\beta = \sqrt{k^2 - k_p^2} = \sqrt{\left(\frac{\omega}{c}\right)^2 - \left(\frac{n\pi}{b}\right)^2}$$

prva rešitev $n=1$

$$TE_{10}: \beta = \sqrt{\left(\frac{\omega}{c_0}\right)^2 - \left(\frac{\pi}{b}\right)^2}$$

$$\left(\frac{\omega}{c_0}\right)^2 - \left(\frac{\pi}{b}\right)^2 \geq 0 : \left(\frac{\omega}{c_0}\right)^2 \geq \left(\frac{\pi}{b}\right)^2$$

$$Z_L = \frac{d}{W} \sqrt{\frac{\mu_0}{\epsilon_0}}$$

$$\frac{2\pi}{\lambda} = \frac{2\pi R}{c_0} \geq \frac{\pi}{b} \Rightarrow b \geq \frac{\lambda}{2}$$

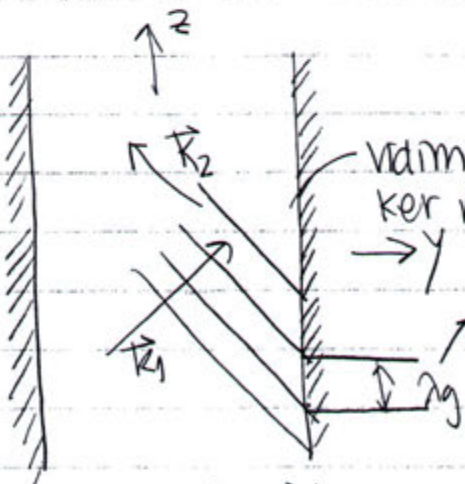
$$Z_L \sim 500 \Omega$$

fazna hitrosti... kako hitro se spreminja faza

$$v_f = \frac{\omega}{\beta} = \frac{\omega}{\sqrt{\left(\frac{\omega}{c_0}\right)^2 - \left(\frac{n\pi}{b}\right)^2}} = c_0 \frac{k}{\beta}$$

$$c_0 = \frac{\omega}{k} \Rightarrow \omega = c_0 k$$

$$\beta \leq k \Rightarrow \boxed{v_f \geq c_0} \quad \omega \geq \frac{c_0 \pi}{b}$$



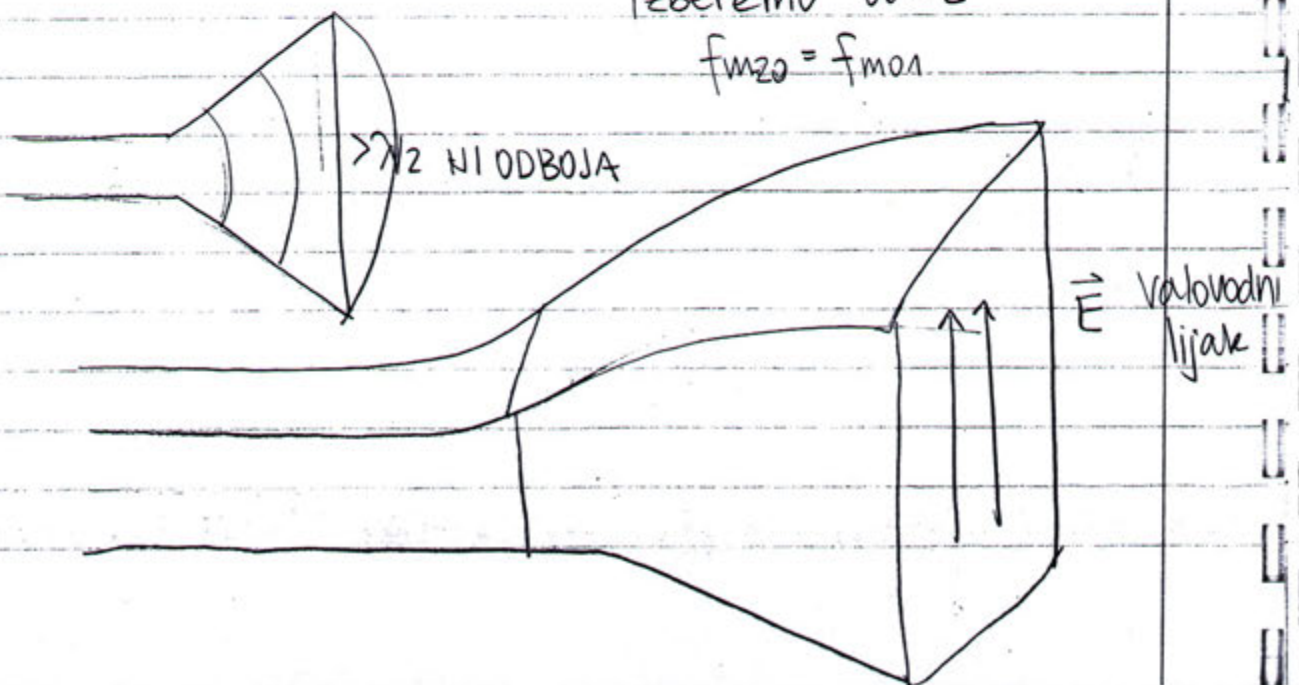
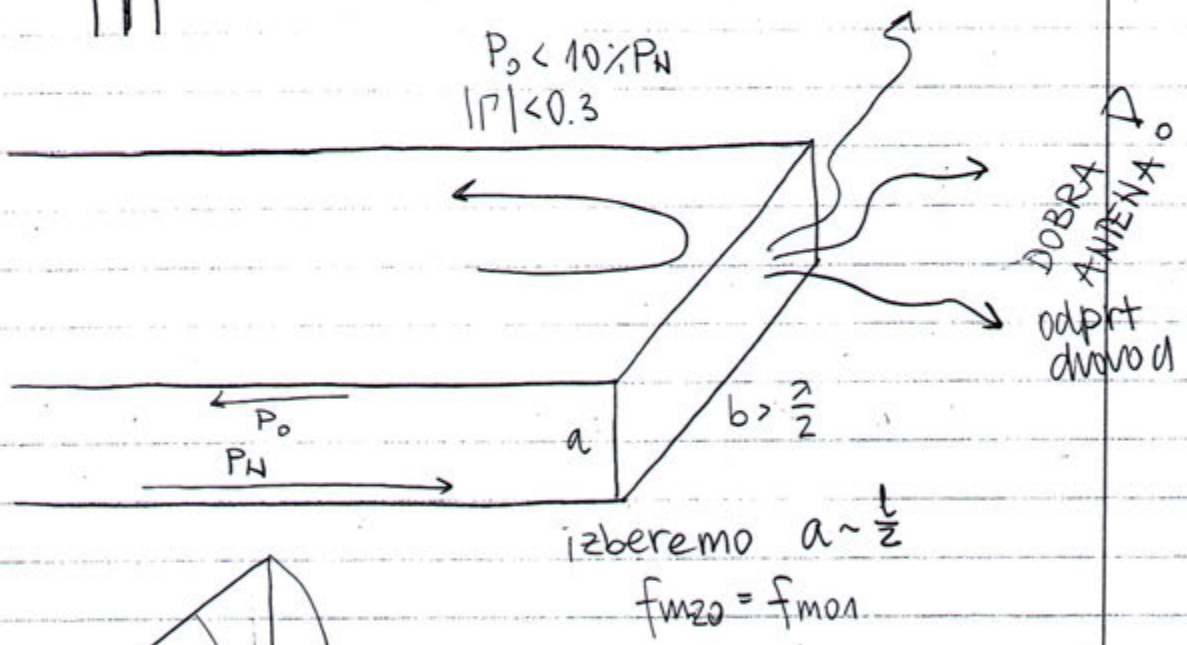
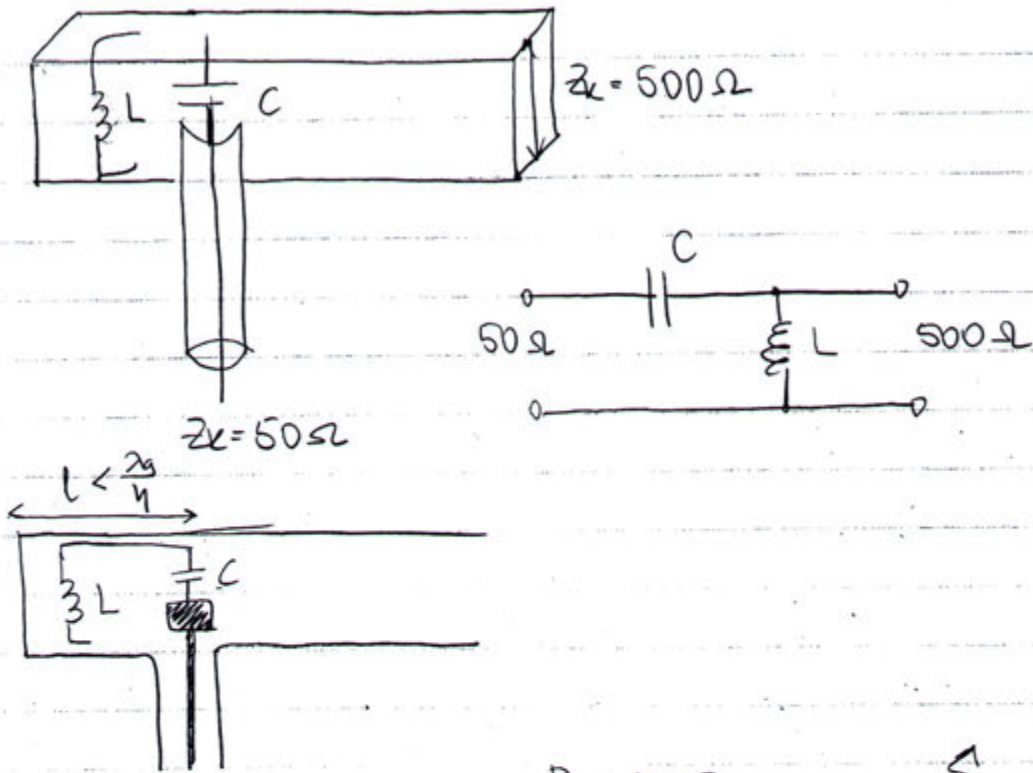
$$\lambda_g = \frac{2\pi}{\beta} \geq \lambda = \frac{2\pi}{k}$$

vidimo večo valovno dolžino kot v rešnici,
ker ne opazujemo v smeri valovanja

GUIDED

$\lambda_g \geq \lambda \Rightarrow$ zato smo dobili, da je $v_g \geq c_0$

navidez veča valovna dolžina



impedanca:

$$Z = \frac{U}{I} = \frac{E \cdot l}{k \cdot 2\pi a \gamma} = \frac{l}{2\pi a \gamma} (\alpha + j\beta) = \underbrace{R}_{\text{izgube}} + jX$$

↑ upornost

dolžina upora

$$R = \frac{l}{2\pi a} \frac{\alpha}{\gamma} = \frac{l}{W} R_p = \frac{l}{2\pi a} \sqrt{\frac{W \mu}{2\gamma}}$$

širina upora

$$\alpha = \sqrt{\frac{W \mu \gamma}{2}}$$

plastna upornost:

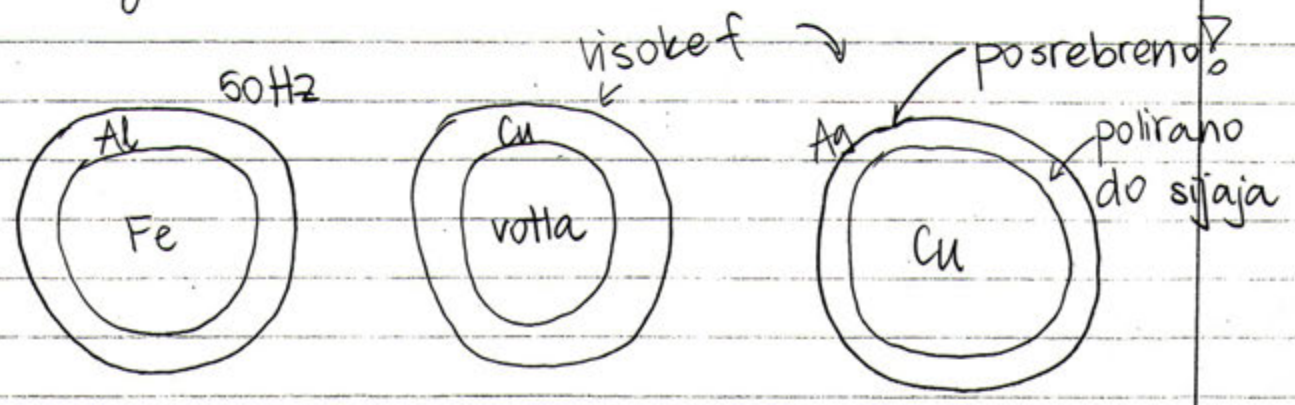
$$R_p = R_D = \sqrt{\frac{W \mu}{2\gamma}}$$

enosmerna: $W=0$: (tok po celem preseku vodnika)

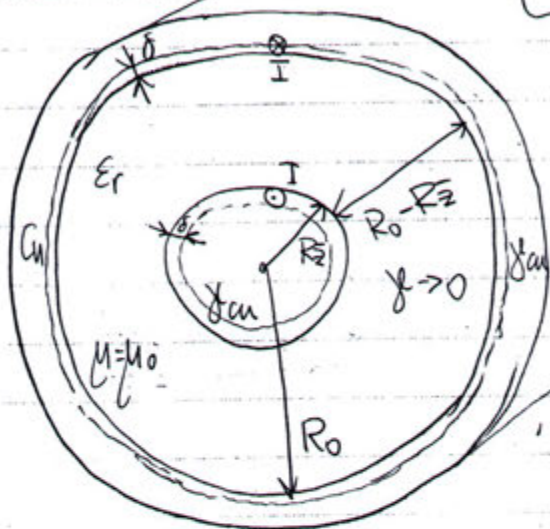
$$R = \frac{l}{\pi a^2} \cdot \frac{1}{\gamma} \ll R = \frac{l}{2\pi a} \sqrt{\frac{W \mu}{2\gamma}} = \frac{l}{2\pi a \delta} \cdot \frac{1}{\gamma}$$

tok samo po koži debeline δ za visoke frekvence $W \sim 100 \text{ MHz} \Rightarrow$ več izgub

$$\delta = \sqrt{\frac{2}{W \mu \gamma}}$$

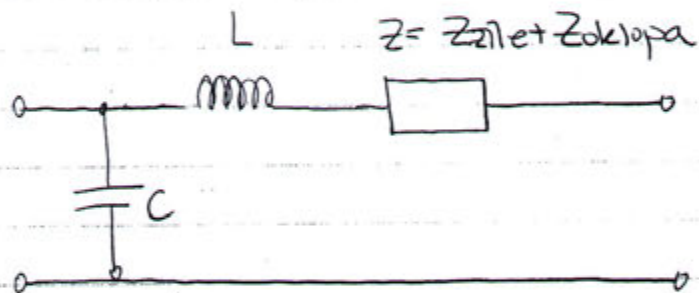


koaksialni kabl:



$R_0 - R_2 \gg \delta$
 $\omega L \gg X_{zile}, X_{klopa}$
 zanemarimo

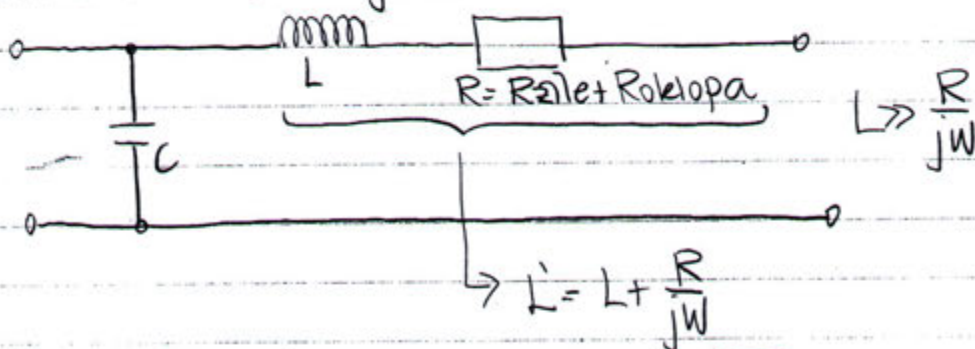
nadomestna vezava:



$$C/l = 2\pi\epsilon \ln \frac{R_0}{R_2} \quad ; \quad L/l = \frac{\mu}{2\pi} \ln \frac{R_0}{R_2}$$

$$Z_{zile}/l = R_{zile} + jX_{zile} \quad ; \quad Z_{klopa}/l = R_{klopa} + jX_{klopa}$$

⇒ nadomestno vezje bo:



brezizgubni kabl

karakteristična impedanca: $Z_k = \sqrt{\frac{L/l}{C/l}}$

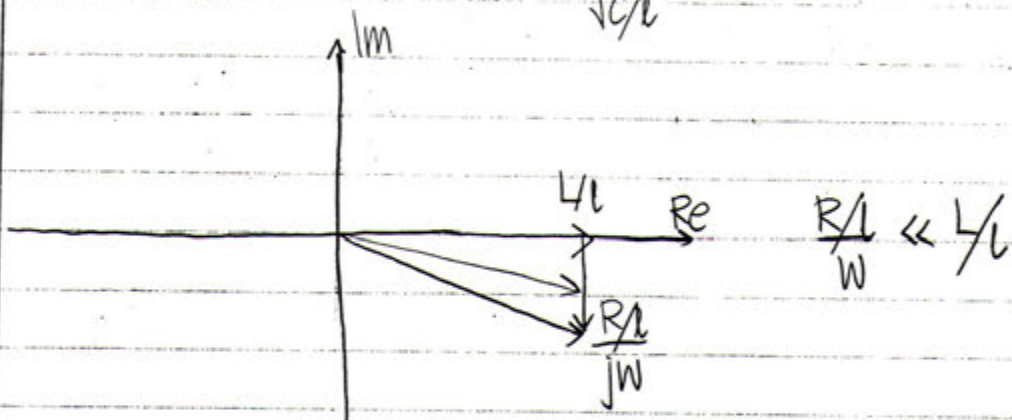
fazna konstanta: $\beta = \omega \sqrt{L/l \cdot C/l} = k$

Izgubni kabel:

$$Z_k = \sqrt{\frac{L/l + \frac{R/l}{j\omega}}{C/l}} \approx \sqrt{\frac{L/l}{C/l}}$$

$$K = \omega \sqrt{\left(L/l + \frac{R/l}{j\omega}\right) \cdot C/l} = \beta \cdot (j\alpha) \quad \begin{matrix} \text{izgube!} \\ \beta \approx \omega \sqrt{L/l + C/l} \\ \alpha \neq 0 \end{matrix}$$

$$\begin{aligned} \alpha &= \beta \cdot \frac{R/l}{2\omega L/l} = \omega \sqrt{L/l \cdot C/l} \frac{R/l}{2\omega L/l} = \\ &= \frac{R/l}{2\sqrt{L/l}} = \frac{R/l}{2Z_k} \end{aligned}$$



$$\sqrt{1+x} \approx 1 + \frac{x}{2} \quad x \ll 1$$

$$K = \omega \sqrt{\left(L/l + \frac{R/l}{j\omega}\right) (C/l)} = \omega \sqrt{\left(L/l\right) (C/l) \left(1 - j \frac{R/l}{\omega L/l}\right)} \approx$$

$$\approx \omega \sqrt{\left(L/l\right) (C/l)} \left(1 - j \frac{R/l}{2\omega L/l}\right)$$

$$\alpha = \frac{R/l}{2Z_k} \quad ; \quad U(l) = (U(0) e^{j\beta l}) e^{-\alpha l}$$

$$a = 20 \log_{10} \left| \frac{U(0)}{U(l)} \right| = 20 \log_{10} e^{\alpha l} \quad [\text{dB}]$$

$$a = \frac{Z_0}{\ln 10} \quad \alpha l = \frac{Z_0}{\ln 10} \frac{R/L}{2Z_c} l$$

$$a/l = \frac{10}{\ln 10} \frac{R/L}{Z_c} \quad \left[\frac{\text{dB}}{\text{m}} \right]$$

$$Z_c = \frac{Z_0}{2\pi\sqrt{\epsilon_r}} \ln \frac{R_0}{R_z}$$

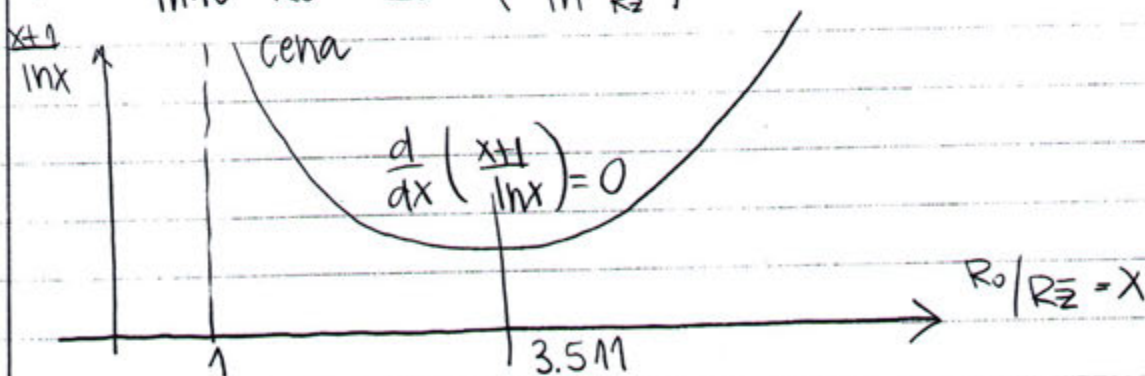
$$R/L = R_z/l + R_0/l = \frac{1}{2\pi R_z \delta \gamma_{cu}} + \frac{1}{2\pi R_0 \delta \gamma_{cu}}$$

$$R/l = \frac{1}{2\pi} \sqrt{\frac{\omega \mu}{2 \gamma_{cu}}} \left(\frac{1}{R_z} + \frac{1}{R_0} \right)$$

$$a/l = \frac{10}{\ln 10} \frac{\frac{1}{2\pi} \sqrt{\frac{\omega \mu}{2 \gamma_{cu}}} \left(\frac{1}{R_z} + \frac{1}{R_0} \right)}{\frac{Z_0}{2\pi\sqrt{\epsilon_r}} \ln \frac{R_0}{R_z}} = \frac{10}{\ln 10} \sqrt{\epsilon_r} \frac{\sqrt{\frac{\omega \mu}{2 \gamma_{cu}}}}{Z_0} \frac{\left(\frac{1}{R_z} + \frac{1}{R_0} \right)}{\ln \frac{R_0}{R_z}} \quad \left[\frac{\text{dB}}{\text{m}} \right]$$

$\epsilon_r \gg 1$; votel dielektrik (penast dielektrik)
 cena $\sim R_0^2$

$$a/l = \frac{10}{\ln 10} \frac{\sqrt{\epsilon_r}}{R_0} \frac{\sqrt{\frac{\omega \mu}{2 \gamma_{cu}}}}{Z_0} \left(\frac{\frac{R_0}{R_z} + 1}{\ln \frac{R_0}{R_z}} \right) \quad \left[\frac{\text{dB}}{\text{m}} \right]$$



$f = 100 \text{ MHz}$ $\delta = 6.8 \cdot 10^{-6} \text{ m}$ $R_z = 0.5 \text{ mm}$ $\epsilon_r = 2$ polietilen
 $\gamma_{cu} = 56 \cdot 10^6 \text{ s/m}$ $R_0 = 1.75 \text{ mm}$ $Z_c = 50 \Omega$ @ $\frac{R_0}{R_z} = 3.5$

rešitev valovne enačbe brez izvorov.

BREZIZGUBNA SNOV

$$\Delta \vec{E} + \omega^2 \mu \epsilon \vec{E} = 0$$

$$\rho = 0, \vec{J} = 0$$

SNOV Z IZGUBAMI $\vec{J} \neq 0, \vec{J} = \gamma \vec{E}$

$$\textcircled{1} \text{ M.E. } \text{rot } \vec{H} = \vec{J} + j\omega \epsilon \vec{E}$$

$$\text{rot } \vec{H} = \gamma \vec{E} + j\omega \epsilon \vec{E}$$

$$\epsilon = \epsilon_0 \epsilon_r$$

$$\text{rot } \vec{H} = j\omega \epsilon_0 \underbrace{\left(\frac{\gamma}{j\omega \epsilon} + \epsilon_r \right)}_{\epsilon_r'} \vec{E} = j\omega \epsilon_0 \epsilon_r' \vec{E} = j\omega \epsilon' \vec{E}$$

$$\epsilon_r' = \epsilon_r - \frac{j\gamma}{\omega \epsilon_0}$$

enako velika?

$$\epsilon_r = \frac{\gamma}{\omega_m \epsilon} \Rightarrow \underline{\omega_m} = \frac{\gamma}{\epsilon_0 \epsilon_r} = \underline{\frac{\gamma}{\epsilon}}$$

$$|\epsilon_0| \sim \frac{1}{4\pi \cdot 9 \cdot 10^9} \frac{\text{As}}{\text{Vm}}$$

$$\Delta \vec{E} + \omega^2 \mu \epsilon' \vec{E} = 0 \quad \beta > \alpha$$

$$\Delta \vec{E} + \omega^2 \mu \epsilon \vec{E} - j\omega \mu \gamma \vec{E} = 0$$

pri visokih frekv. dielektrik

prevlada pri nizkih frekvencah prevodnik

PRIMERJAVA: velikostni razred

| | SNOV | ϵ_r | γ | $f_m = \frac{\omega_m}{2\pi}$ |
|------------|--|--------------|-----------------------------|---|
| prevodnik | kovina Cu | 1 | $56 \cdot 10^6 \text{ S/m}$ | $10^{18} \text{ Hz} = 10^6 \text{ THz}$ področje rentgenskih žarkov |
| | morska voda $\mu \sim 10$ | 80 | 5 S/m | $1.2 \cdot 10^9 \text{ Hz} = 1.2 \text{ GHz}$ |
| dielektrik | čisti SiO_2 ^{čisto kremenovo steklo} | | | $\frac{1}{100} \text{ let} \approx 10^{-8} \text{ Hz}$ |

dober prevodnik $\Rightarrow \beta = \alpha$

$$\epsilon_r \ll \frac{\omega}{\omega_{e0}}$$

$$\omega \epsilon \ll \gamma$$

približek za valovno enačbo:

$$\Delta \vec{E} - \underbrace{j\omega\mu\gamma}_{k^2} \vec{E} = 0$$

$$\Delta \vec{E} + k^2 \vec{E} = 0$$

fazna konstanta

amplitudna konstanta

$$k^2 = -j\omega\mu\gamma \Rightarrow k = \sqrt{\omega\mu\gamma} \cdot \sqrt{-j} = \pm \left(\sqrt{\frac{\omega\mu\gamma}{2}} - j \sqrt{\frac{\omega\mu\gamma}{2}} \right) = \pm (\beta - j\alpha)$$

$$\vec{E} = \vec{1}_x C e^{\pm jkz} = \vec{1}_x C e^{\mp j \left(\sqrt{\frac{\omega\mu\gamma}{2}} - j \sqrt{\frac{\omega\mu\gamma}{2}} \right) z}$$

$$\vec{E} = \vec{1}_x C \underbrace{e^{\mp j \sqrt{\frac{\omega\mu\gamma}{2}} z}}_{\text{faza}} \underbrace{e^{\mp \sqrt{\frac{\omega\mu\gamma}{2}} z}}_{\text{eksponentno usihanje}}$$

čisto
magnarno

ali eksponentno naraščanje

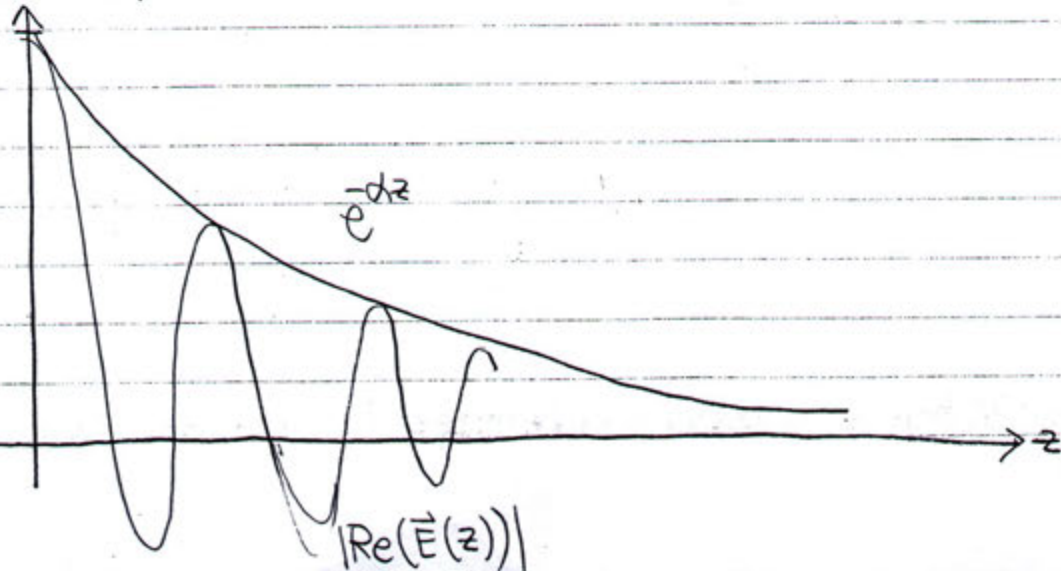
$$\vec{E} = \vec{1}_x C e^{\mp j\beta z} e^{\mp \alpha z}$$

(-) napredujoči val v smeri +z
(+) odbiti val v smeri -z

faza amplituda

enaka predznaka: slabljenje

$|\text{Re}(\vec{E}(z))|$

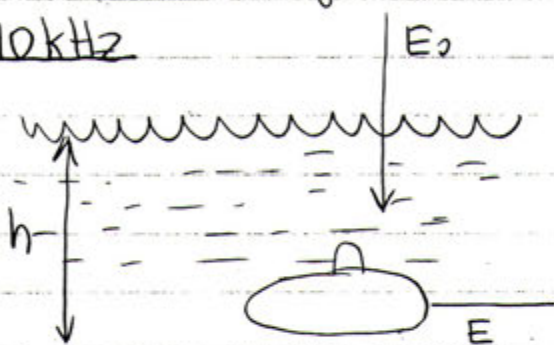


Vdorna globina δ ($\alpha \neq 0$)
 $|\vec{E}(\delta)| = \frac{|E(0)|}{e} = \frac{1}{e} |E(0)|$

$\alpha\delta = 1$
 $\delta = \frac{1}{\alpha} = \sqrt{\frac{2}{\omega\mu\sigma}} \quad (\mu \gg \mu_0 \epsilon)$

| | |
|---|---|
| Zgled | α, β |
| dober prevodnik $\mu \gg \omega\epsilon$ vmesni primer $\mu \sim \omega\epsilon$ dober dielektrik $\mu \ll \omega\epsilon$ | $\alpha = \beta = \sqrt{\frac{\omega\mu\sigma}{2}}$ $\alpha < \beta$ $\beta = \omega\sqrt{\mu\epsilon}, \alpha \rightarrow 0$ |

$f = 10 \text{ kHz}$



$E = E_0 e^{-\alpha h} = E_0 e^{-h/\delta}$

$\delta = \sqrt{\frac{2}{2 \cdot \pi \cdot 10^4 \text{ s}^{-1} \cdot 4\pi \cdot 10^{-7} \frac{\text{Vs}}{\text{Am}} \cdot 5 \frac{\text{A}}{\text{Vm}}}} = \sqrt{5 \text{ m}^2} = \underline{2.2 \text{ m}}$

Slabljenje

$\alpha = 20 \log_{10} \frac{E_0}{E} = 20 \log_{10} e^{h/\delta} = 20 \frac{\ln e}{\ln 10} \frac{h}{\delta} =$
 $= \frac{20}{2.305} \cdot \frac{30 \text{ m}}{2.2 \text{ m}} = \underline{110 \text{ dB}}$

Vdorna globina v kovine

Cu: $\mu = \mu_0$ ($\mu_r = 1$)

$\sigma_{Cu} = 56 \cdot 10^6 \text{ S/m}$

Fe: $\mu_r \sim 1000$

$\sigma_{Fe} \sim 1/10 \cdot \sigma_{Cu}$

| | frekvéncia | δ_{Cu} | δ_{Fe} | frekvéncia | δ_{Cu} | δ_{Fe} |
|-------------|------------|--------------------|--------------------|------------|------------------|---------------|
| ENERGETIKA | 1 Hz | 6.8 cm | 6.8 mm | 1 THz | 68 nm | 6.8 nm |
| | 100 Hz | 6.8 mm | 0.68 mm | 100 THz | ? 6.8 nm | 0.68 nm |
| | 10 kHz | 0.68 mm | 68 μm | svetloba | dimenzije atomov | |
| ELEKTRONIKA | 1 MHz | 68 μm | 6.8 μm | 50 Hz | 10 mm | 1 mm |
| | 100 MHz | 6.8 μm | 0.68 μm | | | |
| | 10 GHz | 0.68 μm | 68 nm | | | |

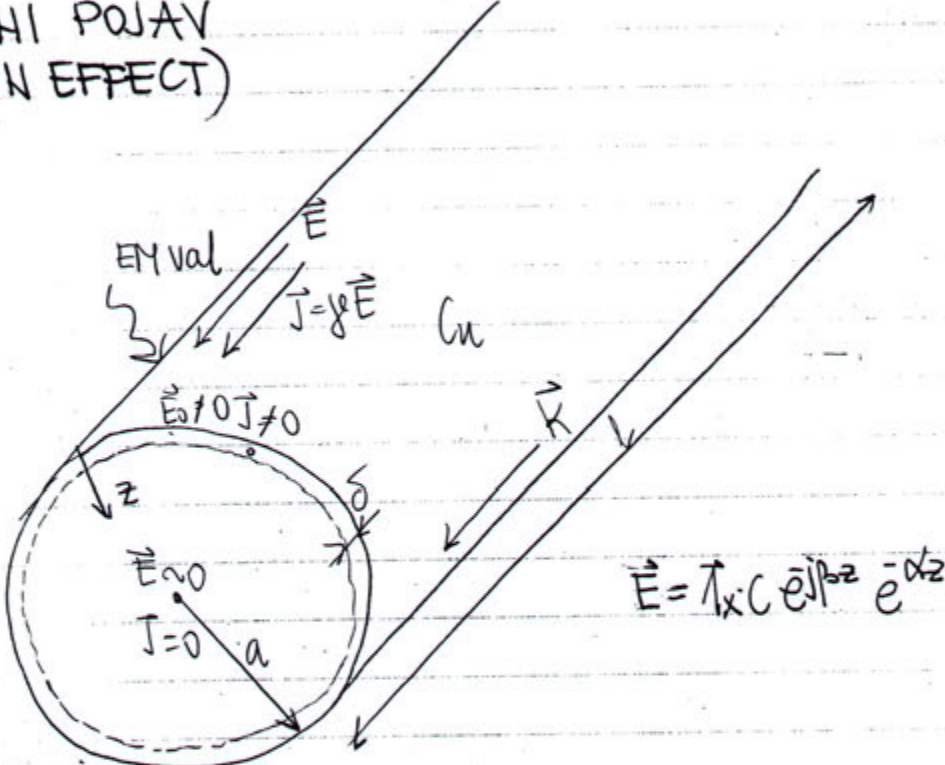
$$f = 1 \text{ Hz}$$

$$\delta_{Cu} = \sqrt{\frac{2}{2\pi \cdot 5 \cdot 10^{-7} \cdot 56 \cdot 10^6}} = \sqrt{\frac{2 \text{ m}^2}{448}} = \sqrt{22 \text{ m}}$$

$$\delta_{Cu} = 6.8 \text{ cm @ 1 Hz}$$

$$\delta_{Fe} = 1/10 \delta_{Cu}$$

KOŽNI POJAV
(SKIN EFFECT)



ploskovni tok:

$$\vec{K} = \int_0^{\infty} \vec{J} dz = \int_0^{\infty} \gamma \vec{E} dz = \int_0^{\infty} \vec{i}_x \gamma C e^{-j\beta z} e^{-\alpha z} dz$$

$$\vec{K} = \vec{i}_x C \gamma \int_0^{\infty} e^{-(\alpha + j\beta)z} dz$$

$$\vec{K} = \vec{i}_x C \frac{-1}{\alpha + j\beta} e^{-(\alpha + j\beta)z} \Big|_0^{\infty} = \vec{E}(0) \frac{\gamma}{\alpha + j\beta}$$

ploskovni tok:

$$\vec{K} = \frac{\gamma}{\alpha + j\beta} \vec{E}$$

$$\frac{E}{K} = \alpha + j\beta$$